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WAVE DRAG REDUCTION FOR AIRCRAFT FUSELAGE - WING CONFIGURATIONS

VOLUME II: Manual for Computer Programs

C.W. Chu, J. Der, Jr., H. Ziegler

Northrop Corporation Aircraft Division

FINAL REPORT

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) An optimization procedure has been developed to minimize the wave drag of an aircraft fuselage-wing configuration subject to constraints imposed by design require- ments. The theory, methods, computer programs and results are presented in this report in two volumes. Volume I describes analyses, results and the optimization procedure. The procedure makes use of the Latin Square sampling technique and the Three-Dimensional Method of Characteristics. The former is used to efficiently sample the family of configurations, and the latter is used to accurately calculate the		

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wave drags of the sampled configurations. The calculated wave drag coefficients are then used to derive a functional dependence of the wave drag on the geometric variables that define the family of configurations. The minimum wave drag configuration can be obtained by minimizing the wave drag function subject to a given set of constraints. The wave drag reduction procedure is demonstrated using an F-4 type configuration as the baseline. The results are presented and discussed.

nsf This Volume H is the user's manual for the computer programs. The input/output information is described in detail. Listings of the programs are given, and samples of built-in program diagnostic messages are explained. Also included are the logical structures of the programs and the descriptions of the subroutines, which in combination with the program listings can be used for possible future modification, improvement, or extension of these computer programs.

FOREWORD

This work was performed by the Aerodynamics Research Organization of the Aircraft Division of the Northrop Corporation in Hawthorne, California for the Naval Air Development Center in Warminster, Pennsylvania (Contract No. N62269-75-C-0537) under the auspices of the Naval Air Systems Command. The contract monitor was Mr. Carmen Mazza of NADC, whose cooperation and assistance are gratefully acknowledged. The authors are indebted to Messrs. William Becker, David Bailey and K. T. Yen of NADC for their valuable assistance during the course of this work. Special thanks go to Messrs. Ray Siewert and Louis Schmidt of NASC for their encouragement and interest in the present work.

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PREFACE

The wave drag reduction procedure presented in Volume I of this report makes use of three major computer programs: the Initial Value Surface (IVS) program, the Three-Dimensional Method of Characteristics (3DMoC) program, and the Surface Fit and Minimum Search program, which are described in the present volume in three parts. The procedure can be used to improve an existing aircraft or to aid in the design of a new one. In the case of improvement, the existing aircraft naturally serves as the baseline. In the case of new design, the preliminary configuration, which is usually obtained through considerations other than the wave drag, can serve as the baseline for wave drag reduction.

The wave drag reduction procedure consists of three major steps:

1. The first step is to select either the 5 x 5 Latin Square for the forward fuselage or the 3 x 3 Latin Square for the blended wing configuration and to describe the baseline and variation configurations using the body description method presented in Appendix C of Volume I. The sections on the description and variation of configuration in Appendix A or the main text of Volume I should be consulted in producing the body description. This step is time-consuming but must be done carefully to assure success in wave drag calculations by the method of characteristics.
2. For the next step of calculating the wave drag coefficients of the configurations sampled by each cell of the Latin Square, the IVS and 3DMoC programs are used. These two programs can run together with the IVS program providing the initial data needed by the 3DMoC program. Input cards can be prepared according to the instructions given in Parts 1 and 2 of the present volume and fed to the IVS and the 3DMoC programs for wave drag calculations. Care needs to be taken in the preparation of these cards, for if the calculation fails to proceed further the first item to check is the correctness of the input cards.
3. After the wave drag coefficients have been calculated by the 3DMoC program, the Surface Fit and Minimum Search Program can be used to define the minimum wave drag configuration for a given set of constraints as explained in Part 3 of the present volume. The program can be used to calculate various minimum wave drag configurations for different sets of constraints as long

as the same baseline configuration is considered and the variables stay within the ranges.

In the following parts, detailed information for setting up and using the three computer program are presented. Samples of deck set-up are compiled in the Appendix for illustration and reference.

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PART 1: THE INITIAL VALUE SURFACE PROGRAM

SECTION I

INTRODUCTION

The Initial Value Surface Program is used to generate starting data for the Three-Dimensional Method of Characteristics Program. In combination, these two programs determine the supersonic flow past smooth blunted bodies for an angle of attack at which the initial value surface remains on the blunted nose. Since the sonic point on a sphere lies between 40 and 50 degrees from the stagnation point, the sphere-body junction should occur at an angle greater than approximately $(50 - \alpha)$ degrees on the sphere, measured in the body axis system.

The lowest usable Mach number is around 2.5, with lower values attainable by careful attention to the initial value surface solution. There is no computational upper limit on the Mach number. However, above $M_\infty = 7.0$ (approximately) the ideal gas model becomes somewhat inaccurate.

The Initial Value Surface Program consists of four separate programs, all connected through an OVERLAY sequence. These programs are:

- (1) Blunt Body Program
- (2) Initial Value Line Interpolation Program
- (3) Rotationally Symmetric Method of Characteristics Program
- (4) Initial Value Surface Interpolation Program

The Blunt Body Program determines the subsonic through slightly supersonic flow over the blunted nose. The Initial Value Line Interpolation Program interpolates in the Blunt Body Program data to develop a start line for the Rotationally Symmetric Method of Characteristics Program. This latter program calculates the required remaining supersonic flow field over the nose. The Initial Value Surface Interpolation Program interpolates in the RSMoC-generated data to determine properties on a plane normal to the body axis, given the number of data rings and the number of meridian planes.

The final output is provided in printed form and is written on a scratch tape for use

by the Three-Dimensional Method of Characteristics Program.

The Initial Value Surface Program consists of approximately 3000 cards. It is written entirely in FORTRAN EXTENDED and has been run under $OPT = 2$ on the CDC FTN Compiler.

SECTION II

INPUT/OUTPUT DESCRIPTION

1. INPUT DESCRIPTION*

The input data cards required by the Initial Value Surface Program are shown in Figure 1. They are described in detail below. The limits indicated refer to storage limitations of the program in its present form.

Card No.	Variable	Format	Description
①	TITLE	7A10	Problem identification
②	ACHM	E12.4	Freestream Mach number
	GAMA	E12.4	Ratio of specific heats
	ALFA	E12.4	Angle of attack, in degrees
	ELAM	E12.4	Slope of the sphere at the sphere-body juncture, in degrees. For bodies with non-conical shapes, this slope should be the largest value of the slopes around the sphere-body juncture.
	RINGS	E12.4	Number of data rings on the initial value surface. A minimum of 3 is recommended. Limit: RINGS < 20
	ONE05	E12.4	M_{body} , Mach number on the body at the point through which the IVL is passed. For $M_{\infty} \geq 2.5$, a value of 1.05 is recommended for M_{body} . For lower Mach numbers, M_{body} should be increased to 1.10. The upper limit is the highest Mach number calculated by the Blunt Body portion of the program on the surface of the sphere. When M_{body} is specified to be greater than this highest value, the program automatically reduces M_{body} to .01 below this value.

*The Appendix may be consulted for sample deck setup.

Card No.	Variable	Format	Description
③	BBW	E12.4	Body bluntness, B_{body} . For a sphere, B_{body} is equal to 1.0. For an ellipse, B_{body} is equal to a^2/b^2 , where a and b are the semi-axes of the ellipse.
	BTEST	E12.4	The tolerance, ΔB , accepted in B_{body} . A value of .001 is usually sufficient.
	STEPS	E12.4	Number of steps required to reach the body, not counting the shock wave. For $M_\infty \geq 2.5$, a value of 4 should be sufficient. For lower Mach numbers, larger values should be used. Limit: STEPS < 10
	B	E12.4	Initial guess at the shock wave bluntness, B_{shock} . If $B=0$, the program computes its own value based on an approximating curve. Card 4 is not required for this case.
	POINTS	E12.4	Number of shock points. For $M_\infty > 2.5$, a value of 70 should be sufficient. For lower Mach numbers, this value should be increased. Limit: POINTS < 100
④	EM	E12.4	Number of meridian planes in 90° . This defines the spacing of the meridian planes. Note that, if EM is the number of meridian planes in 90° , $2EM-1$ is the number in 180° . Limit: EM \leq 10
	● If B=0, omit card 4		
	G	E12.4	Step size multiplier, to be obtained from previous calculations or other knowledge.
⑤	DETA	E12.4	Initial step size normal to the shock, $\Delta \eta$
	DY	E12.4	Initial step size along the shock, $\Delta \xi$
⑥	I	I1	Output control for the RSMoC portion of the program. I=2 is recommended. If I $\left\{ \begin{array}{l} = 1, \text{ only body points are printed} \\ = 2, \text{ all points are printed} \\ = 4, \text{ detailed print is generated} \end{array} \right.$
	FJ	F3.0	Initial C-Summary Number for obtaining local checkout print. Should normally be zero.

Card No.	Variable	Format	Description
⑤	FK	F2.0	Final C-Summary Number for obtaining local checkout print. Should normally be zero.
	HOL (3)	E18.6	Step size along the body for the RSMoC portion of the program. A value of 0.1 is recommended. Should difficulties arise in the RSMoC portion of the program, a small change in this value will rearrange the mesh points and often cure the problem.

Figure 2 shows the input data cards required to generate an initial value surface for a blunted 25° cone at 15° angle of attack.

2. OUTPUT DESCRIPTION

The first item of output is a listing of the input data, as read. Figure 3 is an example of such output. Whenever unusual messages or stops occur later in the program, this listing should be examined for correctness. Also note that an interpolation Mach number which is higher than the recommended value (for the freestream Mach number specified) has been used. This was done to exercise the automatic resetting feature of the program, which was discussed in the preceding section.

Each iteration of the Blunt Body portion of the program generates output, such as shown in Figure 4. At the top are given the freestream conditions, followed by the governing quantities for the Blunt Body portion of the program, B, DELTA, DY and G which have all been identified in the preceding section. Following this is a progress report showing the number of points on each shock-like line. Note that the program will drop a minimum of six points in passing from line to line. More points may be dropped due to increasing roughness in the interpolation process. The results of the body fit process are listed, where DELTA is the shock stand-off distance, Δ/R_{shock} , B(BODY) is the body bluntness, and R(BODY) is the ratio of $R_{\text{body}}/R_{\text{shock}}$. The η and ξ coordinates and the local Mach number are given for each subsonic body point. Near convergence, the final body Mach number should be only slightly less than 1.0.

When convergence has occurred, the complete blunt body flow field is printed out, with the coordinates now normalized by R_{body} . Figure 5 shows a typical first page of such an output. At the top are given the freestream conditions, and the geometric

```

***** LEWIS CHECK CASE NO.1F WTIDY DECK CHECK< MAY/10/72 *****
*****
* I * MACH NO. = 8.8000
* N * GAMMA = 1.4000
* P * ANGLE OF ATTACK = 15.000 DEG.
* U * BODY SLOPE = 25.000 DEG.
* T * NO. OF RINGS = 5.0000
* D * INTERPOLATION MACH NO. = 1.1500
* A * BODY BLUNTNESS = 1.0000
* A * BLUNTNESS TOLERANCE = .10000E-02
* T * STEPS = 4.0000
* A * R(SHOCK) = -0.
* I * NO. OF POINTS = 70.000
***** NO. OF MERIDIANS = 4.0000

```

FIGURE 3. LISTING OF INPUT DATA

```

FREE STREAM CONDITIONS
M= .880000E+01
GAMMA= 1.400000
PARAMETERS
H= .451491E+00
DETA= .207438E-01
DY= .200000E-01
G= .100000E+01
ETA STEP NO 1 ETA= 1.000000 NO OF X1 S = 70
ETA STEP NO 2 ETA= .9722562 NO OF X1 S = 62
ETA STEP NO 3 ETA= .9585124 NO OF X1 S = 55
ETA STEP NO 4 ETA= .9377886 NO OF X1 S = 49
ETA STEP NO 5 ETA= .9170248 NO OF X1 S = 43
ETA STEP NO 6 ETA= .8952810 NO OF X1 S = 37
*****
DELTA= .1031314E+00
B(BODY)= .8519421E+00
P(BODY)= .7433888E+00
*****
NO. ETA XI MACH
1 .893619E+00 .100000E-01 .203352E-01
2 .893566E+00 .300000E-01 .483754E-01
3 .893461E+00 .500000E-01 .787246E-01
4 .893302E+00 .700000E-01 .109517E+00
5 .893091E+00 .900000E-01 .140506E+00
6 .892825E+00 .110000E+00 .171634E+00
7 .892504E+00 .130000E+00 .202892E+00
8 .892128E+00 .150000E+00 .234284E+00
9 .891694E+00 .170000E+00 .265825E+00
10 .891203E+00 .190000E+00 .297533E+00
11 .890653E+00 .210000E+00 .329429E+00
12 .890041E+00 .230000E+00 .361538E+00
13 .889365E+00 .250000E+00 .393887E+00
14 .888625E+00 .270000E+00 .426507E+00
15 .887816E+00 .290000E+00 .459435E+00
16 .886936E+00 .310000E+00 .492709E+00
17 .885982E+00 .330000E+00 .526374E+00
18 .884950E+00 .350000E+00 .560483E+00
19 .883835E+00 .370000E+00 .595096E+00
20 .882632E+00 .390000E+00 .630282E+00
21 .881337E+00 .410000E+00 .666126E+00
22 .879942E+00 .430000E+00 .702726E+00
23 .878440E+00 .450000E+00 .740200E+00
24 .876821E+00 .470000E+00 .778697E+00

```

FIGURE 4. INTERMEDIATE BLUNT BODY OUTPUT

COMPLETE FLOW FIELD NORMALIZED BY RBODY										
		M=	R.800000							
		GAMA=	1.400000							
		B=	.100000E+01							
		R=	.100000E+01							
		DELTA=	.137283E+00							
X	R	MACH NO	VELOCITY	TOT PRES	PRESSURE	TEMPERATURE	DENSITY	DELTA	THETA	
.633329E-04	.129824E-01	.3904266	.177688E+00	.550484E-02	.901714E+02	.159990E+02	.563407E+01	2.58852	89.44099	
.570052E-03	.389473E-01	.3956237	.179759E+00	.551445E-02	.901026E+02	.159875E+02	.563481E+01	7.69219	88.32308	
.158379E-02	.649122E-01	.4048641	.183826E+00	.553374E-02	.899652E+02	.159646E+02	.563528E+01	12.54567	87.20545	
.310514E-02	.908770E-01	.4183654	.189752E+00	.556279E-02	.897595E+02	.159303E+02	.563450E+01	17.15888	86.08830	
.513501E-02	.116842E+00	.4357583	.197357E+00	.560176E-02	.894860E+02	.158847E+02	.563345E+01	21.33741	84.97181	
.767460E-02	.142807E+00	.4566327	.206441E+00	.565084E-02	.891451E+02	.158279E+02	.563214E+01	25.08290	83.85618	
.107254E-01	.168772E+00	.4805762	.216799E+00	.571030E-02	.887378E+02	.157600E+02	.563056E+01	28.38731	82.74159	
.142893E-01	.194737E+00	.5072014	.228238E+00	.578044E-02	.882648E+02	.156812E+02	.562871E+01	31.26663	81.62821	
.183684E-01	.220701E+00	.5361614	.240579E+00	.586164E-02	.877272E+02	.155916E+02	.562658E+01	33.74258	80.51622	
.229451E-01	.246666E+00	.5671563	.253668E+00	.595432E-02	.871261E+02	.154914E+02	.562417E+01	35.85596	79.40578	
.280823E-01	.272631E+00	.5999329	.267368E+00	.605899E-02	.864629E+02	.153808E+02	.562147E+01	37.64195	78.29706	
.337232E-01	.298596E+00	.6342815	.281565E+00	.617623E-02	.857384E+02	.152601E+02	.561848E+01	39.13708	77.19020	
.394911E-01	.324561E+00	.6700308	.296159E+00	.630667E-02	.849554E+02	.151295E+02	.561520E+01	40.37554	76.08535	
.465899E-01	.350526E+00	.7070426	.311067E+00	.645106E-02	.841142E+02	.149893E+02	.561160E+01	41.38836	74.98265	
.534239E-01	.376491E+00	.7452071	.326218E+00	.661021E-02	.832171E+02	.148398E+02	.560770E+01	42.20319	73.88222	
.615977E-01	.402455E+00	.7844378	.341552E+00	.678505E-02	.822657E+02	.146812E+02	.560347E+01	42.84435	72.78818	
.699163E-01	.428420E+00	.8246683	.357017E+00	.697660E-02	.812619E+02	.145139E+02	.559911E+01	43.33307	71.68864	
.787851E-01	.454385E+00	.8656488	.372588E+00	.718604E-02	.802077E+02	.143382E+02	.559400E+01	43.68777	70.59568	
.882101E-01	.480350E+00	.9079428	.388189E+00	.741463E-02	.791050E+02	.141543E+02	.558874E+01	43.92447	69.50540	
.981975E-01	.506315E+00	.9509269	.403785E+00	.766383E-02	.779559E+02	.139628E+02	.558311E+01	44.05702	68.41786	
.108754E+00	.532280E+00	.9947873	.419390E+00	.793521E-02	.767624E+02	.137639E+02	.557710E+01	44.09742	67.33312	
.119887E+00	.558285E+00	1.0395192	.434956E+00	.823058E-02	.755267E+02	.135579E+02	.557069E+01	44.05610	66.25122	
.131605E+00	.584210E+00	1.0851254	.450464E+00	.855191E-02	.742510E+02	.133452E+02	.556387E+01	43.94212	65.17219	
.143916E+00	.610174E+00	1.1316162	.465893E+00	.890144E-02	.729373E+02	.131262E+02	.555616E+01	43.76336	64.09605	
.156828E+00	.636139E+00	1.1790079	.481228E+00	.928163E-02	.715879E+02	.129013E+02	.554800E+01	43.52670	63.02279	
.170335E+00	.662104E+00	1.2273231	.496452E+00	.969526E-02	.702050E+02	.126708E+02	.554071E+01	43.23816	61.95239	
.184499E+00	.688069E+00	1.2765899	.511554E+00	.101454E-01	.687907E+02	.124350E+02	.553203E+01	42.90299	60.88483	
.199278E+00	.714034E+00	1.3268419	.526521E+00	.106357E-01	.673472E+02	.121943E+02	.552282E+01	42.52582	59.82005	
.214703E+00	.739999E+00	1.3781182	.541344E+00	.111698E-01	.658766E+02	.119492E+02	.551305E+01	42.11071	58.75798	
.230784E+00	.765964E+00	1.4304632	.556013E+00	.117523E-01	.643810E+02	.116999E+02	.550271E+01	41.66123	57.69854	
.247538E+00	.791929E+00	1.4839271	.570520E+00	.123891E-01	.628626E+02	.114468E+02	.549174E+01	41.18053	56.64162	
.264977E+00	.817893E+00	1.5385655	.584859E+00	.130827E-01	.613235E+02	.111902E+02	.548012E+01	40.67137	55.58709	
.283117E+00	.843858E+00	1.5944401	.599024E+00	.138426E-01	.597655E+02	.109304E+02	.546781E+01	40.13621	54.53480	
.301976E+00	.869823E+00	1.6516142	.613009E+00	.146749E-01	.581908E+02	.106679E+02	.545475E+01	39.57718	53.48458	
.321571E+00	.895788E+00	1.7101777	.626810E+00	.155878E-01	.566012E+02	.104029E+02	.544091E+01	38.99618	52.43624	
.341922E+00	.921753E+00	1.7701980	.640423E+00	.165905E-01	.549987E+02	.101357E+02	.542622E+01	38.39487	51.38955	
.363049E+00	.947718E+00	1.8317705	.653844E+00	.176937E-01	.533850E+02	.986669E+01	.541063E+01	37.77470	50.34428	
.384975E+00	.973683E+00	1.8949945	.667071E+00	.189095E-01	.517619E+02	.959608E+01	.539406E+01	37.13693	49.30014	
.407724E+00	.999648E+00	1.9599790	.680102E+00	.202520E-01	.501311E+02	.932419E+01	.537646E+01	36.48264	48.25868	
.431322E+00	.102541E+01	2.0268439	.692436E+00	.217373E-01	.484944E+02	.905129E+01	.535773E+01	35.81275	47.21403	
.455747E+00	.105158E+01	2.0957214	.705569E+00	.233839E-01	.468532E+02	.877764E+01	.533779E+01	35.12805	46.17134	
.481181E+00	.107754E+01	2.1667570	.718003E+00	.252136E-01	.452091E+02	.850350E+01	.531553E+01	34.42917	45.12836	
.507507E+00	.110351E+01	2.2401117	.730234E+00	.272514E-01	.435635E+02	.822910E+01	.529388E+01	33.71661	44.08464	
.534810E+00	.112947E+01	2.3159440	.742248E+00	.295289E-01	.419179E+02	.795470E+01	.526958E+01	32.99075	43.03967	
.563131E+00	.115544E+01	2.3945121	.754100E+00	.320765E-01	.402737E+02	.768049E+01	.524363E+01	32.25183	41.99291	
.592513E+00	.118140E+01	2.4754769	.765731E+00	.349349E-01	.386319E+02	.740670E+01	.521581E+01	31.49099	40.94375	

FIGURE 5. FINAL BLUNT BODY OUTPUT

properties of the flow field, R_{body} , B_{body} , and Δ/R_{body} .

Data along each shock-like coordinate line are printed out, starting with the shock itself. The solution is located in a Cartesian coordinate system with the origin located at the stagnation point on the shock (i.e., the intersection of the bow shock and the stagnation streamline). X and R are the abscissa and ordinate of the point, respectively, MACH NO is the Mach number, VELOCITY is V/V_{∞} , DELTA is the local flow direction in degrees, and THETA is the local inclination of the shock wave in degrees.

Figure 6 shows a typical final page output which represents the body. Note that the total pressure values are all identical. This is the distinguishing feature of the body point output. Also note that the maximum body surface Mach number is 1.0910140.

X	H	MACH NO	VELOCITY	TOT PRES	PRESSURE	TEMPERATURE	DENSITY	DELTA
.135813E+00	.115518E-01	.0146529	.672425E-02	.364284E-02	.119105E+03	.194312E+02	.612957E+01	88.61040
.136350E+00	.346535E-01	.0450707	.206916E-01	.364284E-02	.118953E+03	.194241E+02	.612401E+01	87.75170
.137425E+00	.577495E-01	.0752441	.345543E-01	.364284E-02	.118651E+03	.194100E+02	.611289E+01	86.50845
.139037E+00	.808361E-01	.1052335	.484055E-01	.364284E-02	.118199E+03	.193888E+02	.609622E+01	85.20960
.141140E+00	.103909E+00	.1352292	.622560E-01	.364284E-02	.117597E+03	.193606E+02	.607404E+01	83.89142
.143883E+00	.126465E+00	.1662070	.761048E-01	.364284E-02	.116847E+03	.193252E+02	.604637E+01	82.56355
.147120E+00	.150000E+00	.1966900	.899697E-01	.364284E-02	.115952E+03	.192828E+02	.601324E+01	81.22946
.150402E+00	.173009E+00	.2273011	.103438E+00	.364284E-02	.114913E+03	.192333E+02	.597469E+01	79.89053
.155233E+00	.195988E+00	.2580063	.117718E+00	.364284E-02	.113732E+03	.191766E+02	.593077E+01	78.54725
.160115E+00	.218933E+00	.2890047	.131612E+00	.364284E-02	.112412E+03	.191127E+02	.588152E+01	77.19965
.165554E+00	.241839E+00	.3201493	.145524E+00	.364284E-02	.110956E+03	.190417E+02	.582700E+01	75.84748
.171553E+00	.264701E+00	.3515276	.159458E+00	.364284E-02	.109367E+03	.189633E+02	.576726E+01	74.49028
.178117E+00	.287514E+00	.3831713	.173419E+00	.364284E-02	.107647E+03	.188777E+02	.570255E+01	73.12743
.185253E+00	.310272E+00	.4151159	.187413E+00	.364284E-02	.105801E+03	.187846E+02	.563233E+01	71.75813
.192965E+00	.332969E+00	.4474006	.201447E+00	.364284E-02	.103931E+03	.186840E+02	.555723E+01	70.38142
.201260E+00	.355600E+00	.4800695	.215529E+00	.364284E-02	.101741E+03	.185758E+02	.547710E+01	68.99614
.210148E+00	.378157E+00	.5131724	.229670E+00	.364284E-02	.995342E+02	.184597E+02	.539196E+01	67.60093
.219635E+00	.400632E+00	.5467665	.243982E+00	.364284E-02	.972124E+02	.183357E+02	.530184E+01	66.19414
.229731E+00	.423018E+00	.5804176	.258178E+00	.364284E-02	.947799E+02	.182034E+02	.520472E+01	64.77386
.240446E+00	.445305E+00	.6157022	.272577E+00	.364284E-02	.922377E+02	.180625E+02	.510458E+01	63.37779
.251791E+00	.467484E+00	.6512110	.287049E+00	.364284E-02	.895878E+02	.179127E+02	.500135E+01	61.88319
.263780E+00	.489543E+00	.6875518	.301770E+00	.364284E-02	.868712E+02	.177535E+02	.489094E+01	60.40679
.276426E+00	.511470E+00	.7248550	.316622E+00	.364284E-02	.839677E+02	.175842E+02	.477518E+01	58.90460
.289744E+00	.533251E+00	.7632804	.331695E+00	.364284E-02	.809957E+02	.174041E+02	.465183E+01	57.37182
.303753E+00	.554869E+00	.8030274	.347038E+00	.364284E-02	.779121E+02	.172121E+02	.452459E+01	55.80248
.318470E+00	.576307E+00	.8443486	.362715E+00	.364284E-02	.747110E+02	.170071E+02	.439294E+01	54.18922
.333920E+00	.597543E+00	.8875710	.378808E+00	.364284E-02	.713833E+02	.167871E+02	.425227E+01	52.52272
.350127E+00	.618551E+00	.9331278	.395428E+00	.364284E-02	.679153E+02	.165499E+02	.410366E+01	50.70112
.367121E+00	.639103E+00	.9810078	.412722E+00	.364284E-02	.642867E+02	.162923E+02	.394583E+01	48.97898
.384936E+00	.659763E+00	1.0330365	.430496E+00	.364284E-02	.604674E+02	.160097E+02	.377495E+01	47.04582
.403611E+00	.679488E+00	1.0910140	.450243E+00	.364284E-02	.564151E+02	.156955E+02	.359435E+01	45.02390

FIGURE 6. FLOW PROPERTIES ON THE BODY

In Figure 3, the input data listed an interpolation Mach number of 1.15, which is greater than the last body surface Mach number.

Figure 7 shows the sonic line and stagnation streamline data derived by interpolation. Along the stagnation line, the local flow angle should be zero, except at the last point (the body stagnation point), where a singularity exists. The results shown in Figure 7 represent reasonable values.

Figure 8 shows the resulting initial value line obtained by interpolation in the blunt body data. The initial message is caused by the fact that the interpolation Mach number was specified to be larger than the maximum Mach number on the body surface, calculated in the Blunt Body portion of the program. When this occurs, the program automatically resets the interpolation Mach number to be less than the final body surface Mach number.

The listing of the freestream properties and geometric properties of the blunt body solution is followed by the interpolated drag coefficient, the table in which the interpolation was carried out, and the value used for interpolation.

SONIC POINT DATA										
X	R	MACH NO	VELOCITY	TOT PRES	PRESSURE	TEMPERATURE	DENSITY	DELTA	THETA	
.110033E+00	.535332E+00	1.0000010	.421222E+00	.796869E-02	.766193E+02	.137400E+02	.699786E+03	44.09680	67.20578	
.155691E+00	.570406E+00	1.0000009	.421222E+00	.777957E-02	.748010E+02	.137400E+02	.699787E+03	45.80217		
.204209E+00	.604705E+00	1.0000018	.421222E+00	.746177E-02	.711685E+02	.137400E+02	.699787E+03	46.91614		
.264752E+00	.633135E+00	1.0000043	.421223E+00	.681925E-02	.657598E+02	.137400E+02	.699786E+03	47.51264		
.327921E+00	.648910E+00	1.0000117	.421226E+00	.613318E-02	.589705E+02	.137400E+02	.699784E+03	47.97760		
.375448E+00	.647354E+00	1.0000173	.421236E+00	.550363E-02	.529170E+02	.137399E+02	.699779E+03	48.24784		

STAGNATION POINT DATA										
X	R	MACH NO	VELOCITY	TOT PRES	PRESSURE	TEMPERATURE	DENSITY	DELTA	THETA	
.105048E+00	.111022E-15	.3902817	.173444E+00	.550365E-02	.901801E+02	.152942E+02	.102407E+04	-.04213	90.00000	
.262717E-01	0.	.3068528	.137435E+00	.550365E-02	.938346E+02	.155346E+02	.105154E+04	-.07108		
.568440E-01	0.	.2170013	.980253E-01	.550364E-02	.969314E+02	.158022E+02	.107427E+04	-.14715		
.424422E-01	.111022E-15	.1184624	.540254E-01	.550364E-02	.991820E+02	.161064E+02	.109409E+04	-.44152		
.133673E+00	-.111022E-15	.0013815	.637361E-03	.550364E-02	.100168E+03	.164834E+02	.110786E+04	42.66628		
.137210E+00	-.121426E-05	.0004386	.433041E-03	.550363E-02	.100169E+03	.164849E+02	.110787E+04	88.90918		

FIGURE 7. SONIC LINE AND STAGNATION STREAMLINE

*INTERPOLATION MACH NO. DECREASED TO 1.090 DUE TO LIMITATION ON BODY MACH NO.

INITIAL VALUE LINE DATA		
MACH NO.	GAMMA	
.8800000E+01	.1400000E+01	

DELTA	RBODY	RBODY
.1372834E+00	.1000000E+01	.1000000E+01

CD= .622474E+00 BASED ON THE FOLLOWING TABLE

Y(I)	CPR(I)
.682594E+00	.625498E+00
.662436E+00	.601610E+00
.641935E+00	.576398E+00

INTERPOLATED FOR Y= .679999E+00

IVL DATA STARTING AT SHOCK				
X	Y	DELTA	MACH NO.	PT/PT0
.2623376E+00	.8140287E+00	.4074896E+02	.1530358E+01	.1297562E-01
.2835064E+00	.7943341E+00	.4141026E+02	.1421652E+01	.1081439E-01
.3082310E+00	.7713309E+00	.4230574E+02	.1318021E+01	.9064620E-02
.3370515E+00	.7445169E+00	.4344350E+02	.1222897E+01	.7616691E-02
.3705602E+00	.7133409E+00	.4514656E+02	.1143817E+01	.6422311E-02
.4051535E+00	.6799995E+00	.4711418E+02	.10849626E+01	.5503634E-02

MASS-ENTROPY TABLE					
O.					
.6491218E-01	.5503634E-02	.1298244E-01	.5504835E-02	.3894731E-01	.5514453E-02
.1424068E+00	.5533738E-02	.9087705E-01	.5562789E-02	.1164419E+00	.5601756E-02
.2207014E+00	.5650804E-02	.1687717E+00	.5710297E-02	.1947365E+00	.5780439E-02
.2985960E+00	.5861636E-02	.2466663E+00	.5954321E-02	.2726311E+00	.6058995E-02
.3764906E+00	.6176229E-02	.3245609E+00	.6306672E-02	.3505258E+00	.6451057E-02
.4541852E+00	.6610207E-02	.4024555E+00	.6785045E-02	.4284204E+00	.6976605E-02
.5322794E+00	.7186039E-02	.4803501E+00	.7414634E-02	.5061150E+00	.7663826E-02
.6101745E+00	.7935213E-02	.5582447E+00	.8230579E-02	.5842096E+00	.8551913E-02
.6880691E+00	.8901436E-02	.6361393E+00	.9281628E-02	.6621042E+00	.9695262E-02
.7659637E+00	.1016544E-01	.7164339E+00	.1063566E-01	.7399988E+00	.1116981E-01
	.1175230E-01	.7919285E+00	.1238808E-01	.8140287E+00	.1297562E-01

FIGURE 8. INITIAL VALUE LINE

The final table is the mass-entropy table which is a listing of the shock point ordinates (which define the swallowed mass) and the associated total pressures. Each line consists of three pairs of data, with each pair being a shock ordinate and total pressure. The first pair represents the stagnation streamline and the final pair the initial value line shock point.

Figure 9 shows the first page of the Rotationally Symmetric Method of Characteristics output. The body geometric description occupies the upper portion of the output. The body is now located in a coordinate system centered at the body stagnation point. The blunt segment equation is then

$$Y = \sqrt{2RX - BX^2}$$

where the values of R and B are given in the output. The second section is a specialization of the general cubic equation

$$Y = A(X-X_1)^3 + B(X-X_1)^2 + C(X-X_1) + D$$

PAGE 1

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BLUNT SEGMENT 1  X2= .R26352F+00  Y2= .984808F+00  X*= .100164F+00
                  W= .100000F+01  R= .100000E+01
CURVIC SEGMENT 2  X2= .200000E+01  Y2= .119175F+01  X*= .104324F+00
                  SLOPE 1= 10.00000 DEG  SLOPE 2= 10.00000 DEG
                  A= 0.  H= 0.  C= .176327F+00  D= .984808E+00
*****ROTATIONALLY SYMMETRIC FLOW*****
33 ENTROPY VALUES READ

---C-SUMMARY NO. 1---
POINT  X      Y      DELTA  MACH  P/PTI  PT/PT0
1      .233277  .713341  45.167  1.1438  .937454  .642231E-02
2      .258242  .706202  45.282  1.1189  .873937  .595844E-02
3      .283815  .697910  45.740  1.0985  .848606  .550363E-02
DRAG COEF.= .643534E+00  (DELTA M)/(M TOTAL)= .422081E-01

---C-SUMMARY NO. 2---
POINT  X      Y      DELTA  MACH  P/PTI  PT/PT0
1      .199768  .744517  43.483  1.2229  1.00415  .761069E-02
2      .227292  .738517  43.699  1.1935  .950355  .693776E-02
3      .251657  .732613  43.646  1.1835  .890420  .642490E-02
4      .274805  .726505  44.072  1.1592  .856779  .599684E-02
5      .303571  .717626  44.141  1.1233  .822257  .550363E-02
DRAG COEF.= .666944E+00  (DELTA M)/(M TOTAL)= .111710E-01

---C-SUMMARY NO. 3---
POINT  X      Y      DELTA  MACH  P/PTI  PT/PT0
1      .170948  .771331  42.306  1.3180  1.05331  .906462E-02
2      .197288  .767619  42.458  1.2785  1.00756  .822413E-02
3      .221760  .763010  42.521  1.2477  .956394  .749726E-02
4      .247668  .758249  42.338  1.2141  .899161  .693122E-02
5      .269568  .753193  42.609  1.2087  .867818  .647396E-02
6      .296566  .746740  42.780  1.1893  .820562  .597573E-02
7      .325773  .738524  42.194  1.1622  .781742  .550363E-02
DRAG COEF.= .691241E+00  (DELTA M)/(M TOTAL)= .781880E-03

```

FIGURE 9. ROTATIONALLY SYMMETRIC METHOD OF CHARACTERISTICS OUTPUT

where A, B, C, D are given in the output. For each segment, X2, Y2 are the coordinates of the final point. For segment 1, these coordinates represent the juncture between the sphere and the cone of slope $\lambda - \alpha$ (body slope minus angle of attack).

Next is printed a reminder that this is rotationally symmetric flow, followed by the number of mass-entropy points read. This should correspond to the number prepared by the Initial Value Line portion of the program.

The data for each characteristic line are grouped under C-SUMMARY headings which are numbered consecutively. The first few C-Summaries will start from points on the IVL and these will not have shock points. Eventually, however, the C-Summaries will have shock points as Point 1. This is denoted by the value of the shock angle being printed out as THETA SHOCK 1 = XXX just beneath the C-Summary number and by a 1 being printed at the extreme right of the shock point data.

Each C-Summary contains, as a final item, the summed wave drag coefficient and the mass flow error. After the first few C-Summaries, this mass flow error should be much less than 0.10. Otherwise, a smaller step size is needed.

ANGLE OF ATTACK = 15.00 CONE ANGLE = 25.00000 DATA PLANE = .5773817					
8.800000 1.400000 15.000000 .57738174					
RING NO. 1					
Z	X	MACH	PT/PT0	THETA	PSI
-.9063078E+00	-.1726768E-11	1.2217258	.5503634E-02	24.99999979	90.00000000
-.8181791E+00	.3936596E+00	1.2883293	.5503634E-02	26.01400608	-45.34219559
-.5462947E+00	.7293347E+00	1.4203431	.5503634E-02	27.96334537	-5.19490444
-.1093817E+00	.9063078E+00	1.6273434	.5503634E-02	28.90455539	29.03199324
.3836754E+00	.8265352E+00	1.8940439	.5503634E-02	27.96334537	56.54005111
.7649038E+00	.4891902E+00	2.1225041	.5503634E-02	26.01400608	76.36295185
.9063078E+00	-.2219490E-11	2.1932926	.5503634E-02	24.99999979	90.00000000
RING NO. 2					
Z	X	MACH	PT/PT0	THETA	PSI
-.9723198E+00	-.1870498E-11	1.3527225	.6762385E-02	23.46334930	90.00000000
-.8783550E+00	.4272183E+00	1.4051956	.6802801E-02	25.04536870	-44.63441771
-.5868148E+00	.7967915E+00	1.5603617	.7006888E-02	28.26905526	-5.54567256
-.1093817E+00	.1003121E+01	1.7605251	.7230446E-02	31.37634749	26.06426598
.4462869E+00	.9312867E+00	1.9743205	.7376107E-02	32.75191677	51.81681644
.8923473E+00	.5602425E+00	2.1299215	.7456217E-02	33.00740706	72.44252829
.1042272E+01	-.2559474E-11	2.1854259	.7485228E-02	32.97651630	90.00000000
RING NO. 3					
Z	X	MACH	PT/PT0	THETA	PSI
-.1078332E+01	-.2014228E-11	1.5055606	.8831296E-02	22.28056799	90.00000000
-.9385309E+00	.4407771E+00	1.5614025	.9083405E-02	24.17716680	-43.95265369
-.6269348E+00	.8642483E+00	1.7257297	.9782160E-02	28.09339206	-5.34510087
-.1093817E+00	.1099934E+01	1.9429379	.1081324E-01	32.07705509	25.31077246
.5084947E+00	.1036034E+01	2.1627564	.1182286E-01	34.62248828	50.32562417
.1019741E+01	.6313349E+00	2.3247610	.1256621E-01	35.78567131	71.28336665
.1218235E+01	-.2899054E-11	2.3828647	.1283465E-01	36.10582939	90.00000000
RING NO. 4					
Z	X	MACH	PT/PT0	THETA	PSI
-.1106344E+01	-.2157957E-11	1.7138772	.1275552E-01	21.57700346	90.00000000
-.9987088E+00	.4943354E+00	1.7169999	.1342631E-01	23.74117593	-43.54185881
-.6672549E+00	.9117050E+00	1.9601956	.1552433E-01	28.36124020	-5.64988508
-.1093817E+00	.1196747E+01	2.2342465	.1926272E-01	32.77665704	24.59163242
.5715104E+00	.1140790E+01	2.5004086	.2365976E-01	36.03404669	49.29875027
.1147234E+01	.7024072E+00	2.6437877	.2728776E-01	37.76813957	70.54981016
.1374199E+01	-.3238643E-11	2.7620754	.2851835E-01	38.30402320	90.00000000
RING NO. 5					
Z	X	MACH	PT/PT0	THETA	PSI
-.1170356E+01	-.2301687E-11	1.9963238	.2104778E-01	21.11800828	90.00000000
-.1058883E+01	.5278946E+00	2.0764296	.2290993E-01	23.40411353	-43.30339389
-.7075749E+00	.9991618E+00	2.2785695	.2638318E-01	28.59447790	-5.91041171
-.1093817E+00	.1293559E+01	2.5971164	.3062772E-01	33.58825526	23.79562061
.4341222E+00	.1245541E+01	2.9382790	.4610073E-01	37.17580737	48.52184246
.1274678E+01	.7734746E+00	3.1780746	.7090419E-01	39.33140274	70.01710784
.1530163E+01	-.3574227E-11	3.2680198	.7726594E-01	40.00518452	90.00000000

FIGURE 10. INITIAL VALUE SURFACE

When the drag coefficient and the mass flow error no longer change, the C-Summaries no longer terminate on the body but out in the field.

Figure 10 shows the final output, the initial value surface, derived by interpolation in the RSMoC-generated data. The data are presented "ring-wise," with each of the points being located on one of the specified meridian planes in the wind axis system. These data are also written on TAPE4, which can be defined as the system punch tape or a utility tape, for later reading by the the Three-Dimensional Method of Characteristics Program.

SECTION III

OPERATIONAL ASPECTS

1. CORE AND TIME REQUIREMENTS

The program requires approximately 100,000₈ words of memory to load and execute on the CDC 6600 computer.

The program requires 30-40 seconds of Central Processor Unit (CPU) time to compile. A normal run will require 15-20 seconds CPU time for execution. Very little difference has been found between the execution times generated by the OPT = 1 and OPT = 2 compiler options.

2. ERROR MESSAGES

The built-in error messages in the program are listed below. They are arranged according to the OVERLAY segment and the program or subroutine in which they are generated. Probable causes and possible corrective measures are outlined.

However, no such discussion can be complete. The program is too complex to allow every eventuality to be foreseen. When failures do occur in the Blunt Body portion of the program, it is probably due to a poor choice in the number of steps to the body. If the failure is in the Rotationally Symmetric Method of Characteristics portion of the program, a slight change in the step size, the number of points on the initial value line, or M_{body} for the IVL will usually allow the program to continue. In the latter case, a plot of the characteristic network will usually reveal the problem.

A failure in the Rotationally Symmetric Method of Characteristics portion of the program will result in the print option, INCASE, being reset to a value of 4 and the control being set back to repeat the calculation of the present characteristic. The physical appearance is the sudden onset of extremely detailed print. If the failure occurs in the region governed by the initial value line (since the program cannot rewind the input tape) the next point on the IVL is read in, and a detailed print of that calculation up to but not including the body point is given. By plotting the characteristic data, the troublesome point is easily spotted.

OVERLAY (BLUNT, 1, 0)

Program BLUNTS

COMPUTED FEWER THAN 3 BODY POINTS TWICE

Not enough shock points. Increase number of shock points.
Too many steps to the body. Decrease number of steps.

FAILED TO FIND A SUPERSONIC BODY POINT IN 4 TRIES

Too few shock points. Increase number of shock points.

FAILED IN G CONVERGENCE

No solution for the η -step multiplier. Change number of steps to the body

EXCEEDED 9 ITERATIONS FOR BODY

Convergence criterion too small. Relax convergence criterion.
Roughness in the relationship between B_{body} and B_{shock} . Plot the individual data, and establish a starting value for B_{shock} .

ZERO OR NEGATIVE G

Too many steps to the body. Decrease number of steps.

Subroutine BODY

NO ROOT FOR DELTA

Poorly defined body due to roughness and/or few body points. Increase number of points on the shock and/or decrease number of steps to the body.

INSUFFICIENT NUMBER OF BODY POINTS FOR CURVE FIT

Not enough body points. Increase number of shock points and/or decrease number of steps to the body.

Subroutine IDTHER

ROOT2 FAILURE, TR= _____ BM= _____ AM= _____

Calculated static pressure is greater than calculated total pressure. Arrange number of points on the shock and number of steps to the body so that $\Delta\eta$ is approximately equal to $\Delta\xi$

OVERLAY (BLUNT, 2, 0)

Program IVLS

DID NOT FIND SUPERSONIC POINT M= ____

Not enough supersonic flow region in the Blunt Body portion of the program.
Increase number of points along the shock.

Subroutine BBOUT

EXTRAPOLATED SONIC POINT

Not enough supersonic flow region in the Blunt Body portion of the program.
Decrease number of steps to the body.

OVERLAY (BLUNT, 3, 0)

Subroutine BODI

X1 LIES BEYOND LAST SEGMENT

Probable error in body description and IVL geometry. Check input data

POINT LIES BEYOND END OF BODY X3= _____ XB= _____

Body description geometry is not sufficient for given data points. Plot characteristics to check for geometric incompatibilities, and check input data.

ITERATION FAILED

No convergence on body point. Plot each iteration and check for errors.

IM EXCEEDED 25

Body point Mach number is less than 1.0. Increase M_{body} in input data.

Subroutine FIELD

EXCEEDED 3*50 ITERATIONS IN FIELD POINT

Probable geometric inconsistency. Check input data, plot characteristics data.

FAILED TO CONVERGE S3 IN SPECIAL LOOP

Poor definition of the relationship between the stream function and total pressure.
Check mass-entropy table, may be a read error by computer.

FAILED TO CONVERGE D3 IN SLOW LOOP

Geometric inconsistency. Check input data.

DR FAILURE IN FIELD

First approximation gave the correct answer, making the residual almost zero.
The subsequent iteration was therefore thrown off. Change step size slightly.

FAILED IN FIELD, IMM= _____ P3= _____

Field point Mach number is less than 1.0. Plot characteristics data, check for geometric inconsistencies.

TRIED 10 TIMES TO CONVERGE POINT BUT STILL SUBSONIC

Field point Mach number is less than 1.0. Increase M_{body} in input data.

****NOTE***CONVERGENCE CRITERIA MULTIPLIED BY 10** , FOR POINT**

Poor convergence at field point. Plot characteristics data to determine troublesome point.

OSCILLATION IN FIELD FOR DELS

Convergence problem in determining the local value of the stream function.
Examine mass-entropy table for smoothness; may be a read error by computer.

Subroutine ENTROP

AFTER LAST ENTRY IN S/R TABLE. GMASS= _____, SR SET TO
LAST ENTRY, _____, W/CORRESPONDING MASS _____

BEFORE FIRST ENTRY IN S/R TABLE. GMASS= _____, SR SET TO
FIRST ENTRY, _____, W/CORRESPONDING MASS _____

BEFORE FIRST ENTRY IN S/R TABLE. S/R= _____. GMASS SET TO
FIRST ENTRY, _____, W/CORRES. S/R= _____

BEYOND LAST ENTRY IN S/R TABLE. S/R= _____. GMASS SET TO
LAST ENTRY, _____, W/CORRES. S/R= _____

These statements are advisory in nature, indicating that the mass-entropy table and the local calculations are poorly matched. While the calculation will continue, the mass-entropy table, the geometric parameters, and the input data should be examined for errors.

Subroutine WAVE

FAILED TO CONVERGE SHOCK ANGLE IN 50 TRIES

The subroutine was given an incorrect deflection angle across the shock. Trace origin of the deflection angle, using check-out print.

Subroutine SHOCK

SM IS ZERO OR NEGATIVE IN RSHOCK

A negative step size is specified or complications arising from the mesh build-up resulted in a negative step size. Check input data and/or plot characteristics data.

OSCILLATED THROUGH NGATE THEN IGATE

OSCILLATED THROUGH IGATE THEN NGATE

Both of the above messages indicate that base point data for the shock point solution are being determined by extrapolation rather than interpolation. Plot the progress of the shock point solution to find out where the incorrect extrapolation occurs.

EXCEEDED 50 ITERATIONS FOR POINT 4

Geometric inconsistencies in the mesh build-up. Plot characteristic mesh to locate trouble spot.

EXCEEDED 75 ITERATIONS FOR SHOCK

Poor initial data. Plot characteristic mesh to locate problem area.

SECTION IV

LOGICAL STRUCTURE

1. OVERLAY STRUCTURE, READ/WRITE LOGIC

The logic of the program is controlled by the master program and uses four first level OVERLAY segments. The master program consists of a main program to call each OVERLAY segment and one general use subroutine. The Blunt Body Program, the Initial Value Line Interpolation Program, the Rotationally Symmetric Method of Characteristics Program, and the Initial Value Surface Interpolation Program each comprise one OVERLAY segment. Figure 11 shows the OVERLAY structure and the storage requirements.

Figure 12 shows the read/write logic structure. TAPE2 and TAPE3 would be the same device if minor changes were made in the program logic. TAPE4 is shown as a dotted output device to indicate that this could be either the system punch file or a scratch tape, as the user specifies.

2. INTERDEPENDENCE OF SUBROUTINES

The Calling-Called matrices for three of the four OVERLAY segments are shown in Figure 13. The segment comprised of the Initial Value Surface Program consists of one main program which in turn calls two general purpose subroutines. This matrix, due to its simplicity, is not shown in Figure 13.

3. LISTING

The complete listing of the IVS program is given below, following Figure 13.

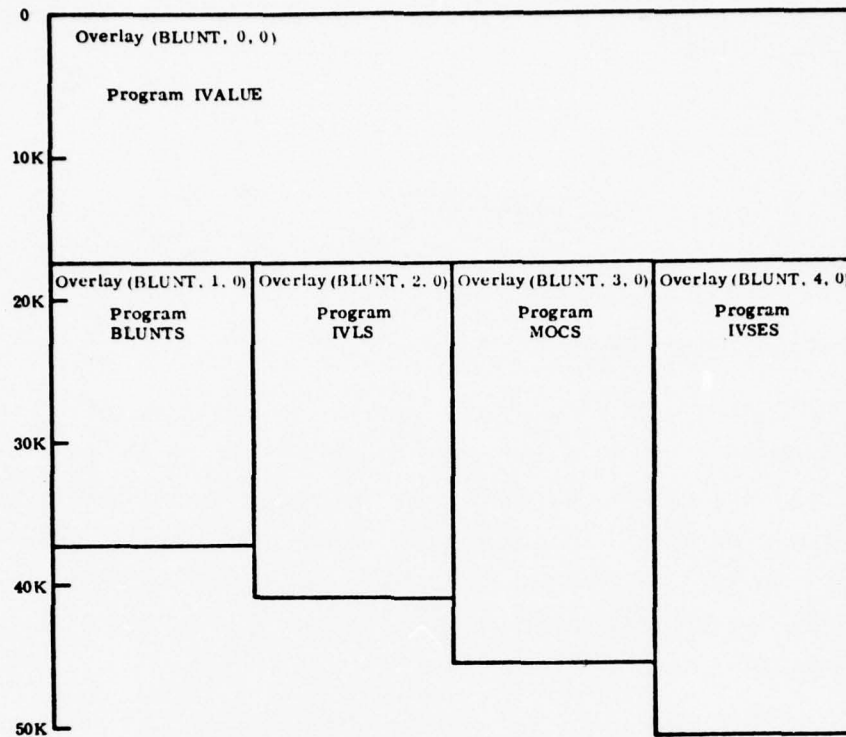


FIGURE 11. OVERLAY STRUCTURE

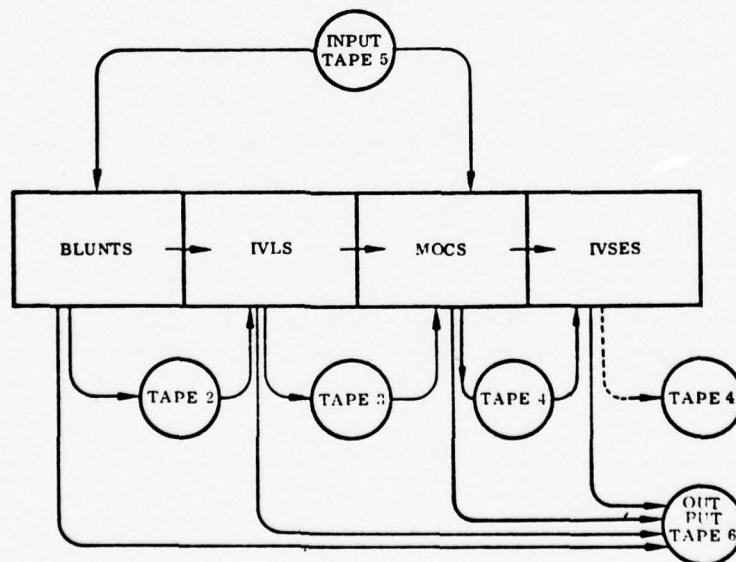


FIGURE 12. READ/WRITE LOGIC

Calling \ Called	BODY	XY	DIFATE	IDTHER	IMAIN	ENTRPG
BLUNTS					•	
IMAIN	•	•	•	•		•

(a) Program BLUNTS

Calling \ Called	DETER	BBOUT	ENTRPG
IVLS	•	•	•
DETER			•
BBOUT			•

(b) Program IVLS

Calling \ Called	BODI	OPER8	FIELD	VMACH	ENTROP	TSON	DIF	CHANGE	INPUT	SHAPE	DROP	OUTPUT	WAVE	SHOCK	MESH	PAGE	ANGLE	VELOC	ENTRPG
MOCS	•	•			•	•		•	•	•	•	•	•	•	•	•	•		
BODI			•												•				
OPER8			•																
FIELD				•	•											•			
ENTROP															•				•
SHAPE															•				
DROP								•											
OUTPUT																•			
WAVE					•												•		
SHOCK				•		•					•	•				•			

(c) Program MOCS

FIGURE 13. CALLING-CALLED MATRIX FOR IVS PROGRAM

A 2
 A 3
 A 4
 A 5
 A 6
 A 7
 A 8
 A 9
 A 10
 A 11
 A 12
 A 13
 A 14
 A 15
 A 16

```

OVERLAY(BLUNT,0,0)
PROGRAM IVALUE(INPUT,OUTPUT,PUNCH,TAPE5=INPUT,TAPE6=OUTPUT,
1 TAPE7=PUNCH,TAPE3,TAPE4,TAPE2)
COMMON /BETA/ G,DETB,DY,ARBE,BEE,CARD,AC,ACHM,GAMA,ALFA,ELAM,RINGS
1,CPR(88),ONE05,M,BDRAG
COMMON /TRANS/ LO,L1,LL,MS
INITIAL VALUE SURFACE PROGRAM
CALL FTNBIN (1,0,DUMMY)
REWIND 3
CALL OVERLAY (SMBLUNT,1,0)
CALL OVERLAY (SMBLUNT,2,0)
CALL OVERLAY (SMBLUNT,3,0)
CALL OVERLAY (SMBLUNT,4,0)
GO TO 1
END
  
```

C 1

C	2	OVERLAY (BLUNT,1,0)	
C	3	PROGRAM BLUNTS	
C	4		
C	5	COMMON /ALPHA/ X,R,PTOPI,CPI,DETA,ETASTG,XISON,ETASON,GG(15),ACHM2	
C	6	1,DEM,XXB(88),YYB(88),ACH(100),STAG,Q000FL(10),DETA02	
C	7	COMMON /BETA/ G,DETB,DY,ARBE,BEE,CARD,B,ACHM,GAMA,ALFA,ELAM,RINGS,	
C	8	ICPR(88),ONE05,M	
C	9	COMMON /KLAPHA/ IBY,META,KPRNT,NB,KDIM,KOM(10),MP	
C	10	DIMENSION XA(9),HOL(7)	
C	11	REWIND 2	
C	12	REWIND 3	
C	13	READ (5,45) HOL	
	56	IF(EOF(5)) 56,57	
	57	CALL EXIT	
		CONTINUE	
	1	DO 1 I=1,7	
		IF (HOL(I).EQ.10H) HOL(I)=10H* * * *
		WRITE (6,55) HOL	
		READ (5,44) ACHM,GAMA,ALFA,ELAM,RINGS,ONE05	
		READ (5,44) BBW,BTEST,STEPS,B,POINTS,EM	
		WRITE (6,51) ACHM,GAMA,ALFA,ELAM,RINGS,ONE05,BBW,BTEST,STEPS,B,	
		POINTS,EM	
		M=EM	
		DEM=1	
		GG(1)=GAMA	
		GG(2)=(GAMA-1.0)*0.5	
		GG(3)=GAMA/(GAMA-1.0)	
		GG(4)=1.0-1.0/GAMA	
		GG(5)=GAMA+1.0	
		GG(6)=GAMA-1.0	
		GG(7)=1.0/GAMA	
		GG(8)=2.0/(GAMA-1.0)	
		GG(9)=1.0/(GAMA-1.0)	
		GG(10)=2.0*GG(1)	
		GG(11)=4.0*GG(1)	
		ACHM2=ACHM**2	
		PTOPI=(1.0+GG(2)*(ACHM**2))*GG(3)	
		CPI=2.0/(GAMA*(ACHM**2))	
		B2=0.0	

39 C
40 C
41 C
42 C
43 C
44 C
45 C
46 C
47 C
48 C
49 C
50 C
51 C
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55 C
56 C
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58 C
59 C
60 C
61 C
62 C
63 C
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65 C
66 C
67 C
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69 C
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71 C
72 C
73 C
74 C
75 C
76 C
77 C
78 C

```

      B1=0.0
      B0D1=0.0
      B0D2=0.0
      IBY=0
      IF (ACHM) 2,2,3
      ACHM=ABS(ACHM)
      MP=4
      IBY=1
      GO TO 4
      MP=0
      NY=POINTS
      D1=ACHM**2-1.0
      DEM=1.0
      KDIM=DEM
      KOM(1)=1.0+DEM
      Q000FL(1)=1.0/(1.0+DEM)
      KOM(2)=KDIM-1
      KOM(3)=2*KDIM
      KOM(4)=2/(1+KDIM)
      Q000FL(3)=KOM(1)
      Q000FL(4)=GG(11)*ACHM2
      Q000FL(5)=GG(5)*ACHM2
      Q000FL(6)=1.0+GG(2)*ACHM2
      IF (B) 7,5,7
      B=0.5-0.559*((ACHM-1.0)**(-1.19))
      DY=0.02
      DELTA=(-0.02*(-.0576/(ACHM**2)))
      G=1.0
      GO TO 8
      READ (5,44) G,DELTA,DY
      IF (G) 6,6,8
      JLOOP=0
      DETB=DELTA
      KPRNT=MP
      ILOOP=0
      NY=POINTS
      IF (B-(-1.0/D1)) 12,10,10
      XSOUND=SQRT(D1/(B*D1+1.0))
      IF (XSOUND-(FLOAT(NY)-0.5)*DY) 11,12,12
      DY=XSOUND/POINTS
  
```

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11

Line	Code	Statement	Column
12	C 79	WRITE (6,54)	
	C 80	WRITE (6,53) ACMM,GAMA	
	C 81	CALL IMAIN (NY)	
	C 82	NB=NB	
	C 83	ILOOP=ILOOP+1	
13	C 84	IF (ABS(BBN-BEE)-8TEST) 36,36,13	
	C 85	DELETA=(1.0-ETASTG)*0.98	
14	C 86	IF (NB-3) 14,14,16	
	C 87	G=1.0	
	C 88	DETA=DELETA/STEPS	
	C 89	IF (ILOOP-1) 9,9,15	
15	C 90	WRITE (6,46)	
	C 91	WRITE (6,47) (XNB(1),YVB(1),I=1,NB)	
	C 92	GO TO 25	
16	C 93	IF (ILOOP-1) 21,21,17	
17	C 94	IF (ACH(NB)-1.0) 18,18,20	
18	C 95	IF (ILOOP-4) 21,21,19	
19	C 96	WRITE (6,48)	
	C 97	ILOOP=1	
	C 98	GO TO 34	
20	C 99	IF (ACH(NB-1)-1.0) 34,21,21	
21	C 100	DELETB=(1.0-DELETA-ETASON)*1.3	
	C 101	AM=STEPS+1.0	
	C 102	R=DELETB/DELETA	
	C 103	IG=0	
	C 104	GP=STEPS*(1.0+R)/AM	
22	C 105	IF (G-1.0) 26,22,26	
23	C 106	IF (GP-1.0) 23,23,28	
	C 107	G=1.0-2.0*(1.0-GP)	
	C 108	IF (G) 24,24,29	
24	C 109	WRITE (6,52) G,GP	
25	C 110	CALL EXIT	
26	C 111	IF (GP-1.0) 27,27,28	
27	C 112	G=0.7*GP	
	C 113	GO TO 29	
28	C 114	G=1.3*GP	
29	C 115	T2=G*AM	
	C 116	IG=IG+1	
	C 117	IF (IG-50) 31,31,30	
30	C 118	WRITE (6,49) G,F,FP,DELETA,DELETB	

C 119
C 120
C 121
C 122
C 123
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C 156
C 157
C 158

```

31      GO TO 25
      F=T2-(T2*(1.0+R))/G+R
      FP=(AM*T2-(STEPS*T2/G)*(1.0+R))/G
      RATF=F/FP
      IF (ABS(RATF)-.00001) 33,33,32
      G=G-RATF
      GO TO 29
32      DETA=DELETA*(G-1.0)/(T2/G-1.0)
      DETB=DETA
      GO TO 9
33      JLOOP=JLOOP+1
      IF (JLOOP-9) 38,38,35
34      WRITE (6,50)
      GO TO 25
35      DO 37 I=1,9
36      XA(I)=0.0
37      WRITE (2) (XA(I),I=1,6)
      WRITE (2) (XA(I),I=1,6)
      GO TO 43
38      B2=B1
      B1=B
      B002=B001
      B001=BEE
      REWIND 2
      IF (JLOOP-2) 39,40,40
39      SIG=SIGM(1.0,8)
      B=B*(B8M/BEE)**(SIG)
      GO TO 21
40      B=(B2-B1)/(B002-B001)
      IF (B) 41,41,42
41      B=B1+(B1-B2)
      B1=B2
      B001=B002
      GO TO 21
42      B=B*(B8M-B002)+B2
      GO TO 21
      C
43      BEE=B8M
      C
44      FORMAT (6E12.4)

```

45	FORMAT (7A10)	C 159
46	FORMAT (1X30NCOMPUTED FEWER THAN 3 BODY POINTS TWICE,80(1H*))	C 160
47	FORMAT (//9X6HX-BODY,9X6HY-BODY/(2E15.6))	C 161
48	FORMAT (1X,49HF FAILED TO FIND A SUPERSONIC BODY POINT IN 4 TRIES)	C 162
49	FORMAT (1X23H FAILED IN G CONVERGENCE/1X2HG=E15.6/1X2HF=E15.6/1X3HF	C 163
	IP=E15.6/1X7HDELETEA=E15.6/1X7HDELETEB=E15.6)	C 164
50	FORMAT (1X30NEXCEEDED 9 ITERATIONS FOR BODY)	C 165
51	FORMAT (1H0,T30,5H****/T30,15H* I * MACH NO.,T60,1H=,G12.5/T30,1H	C 166
	112H* N * GAMMA,T60,1H=,G12.5/T30,22H* P * ANGLE OF ATTACK,T60,1H	C 167
	2=,G12.5,T73,4HDEG./T30,17H* U * BODY SLOPE,T60,1H=,G12.5,T73,4HDE	C 168
	3G./T30,19H* T * NO. OF RINGS,T60,1H=,G12.5/T30,29H* * INTERPOL	C 169
	4ATION MACH NO.,T60,1H=,G12.5/T30,21H* D * BODY BLUNTNESS,T60,1H=,	C 170
	5G12.5/T30,14H* A * BLUNTNE,12HSS TOLERANCE,T60,1H=,G12.5/T30,12H*	C 171
	6 T * STEPS,T60,1H=,G12.5/T30,15H* A * B(SHOCK),T60,1H=,E16.7/T30	C 172
	7,20H* : * NO. OF POINTS,T60,1H=,G12.5/T30,23H**** NO. OF MERIDI	C 173
	8ANS,T60,1H=,G12.5)	C 174
52	FORMAT (10X18NZERO OR NEGATIVE G,10(6H***))	C 175
53	FORMAT (25X22HFREE STREAM CONDITIONS/15X2HM=E15.6/15X6HGAMMA=	C 176
	10PF10.6)	C 177
54	FORMAT (1H1)	C 178
55	FORMAT (2H1*,14(2H *),7A10,14(2H*))	C 179
	END	C 180

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D

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BETA=U2/DENOM
GAMMA=U3/DENOM
T1=-0.5*BETA/GAMMA
T2=ALPHA/GAMMA
T2=T1+T1-T2
IF (T2) 4,4,5
DELCHK=XXB(1)
GO TO 12
T2=SQRT(T2)
DELP=T1+T2
DELM=T1-T2
IF (DELP) 9,9,6
IF (DELM) 8,8,7
DELCHK=AMINI(DELM,DELP)
GO TO 12
DELCHK=DELP
GO TO 12
IF (DELM) 10,10,11
WRITE (6,29) DELP,DELM
RETURN
DELCHK=DELM
BEE=-GAMMA
ARBE=0.5*BETA-BEE*DELCHK
CARD=DELCHK
DO 15 J=1,N
MYCAL(J)=(2.0*ARBE*(XXB(J)-DELCHK)-BEE*(XXB(J)-DELCHK)**2)
IF (MYCAL(J)) 13,14,14
MYCAL(J)=0.0
GO TO 15
MYCAL(J)=SQRT(MYCAL(J))
CONTINUE
WRITE (6,28) DELCHK,BEE,ARBE
NDRAG=NDDY
CMP=(1.0+DEM)/(ARBE*(1+KDIM))
CD=0.5*CPR(1)*(YB(1)*KDIM)*CMP
CD1=CD
DO 16 J=2,NDRAG
CD=0.5*(CPR(J)+CPR(J-1))*((YB(J)-YB(J-1))*KDIM)*CMP+CD
CPR(J-1)=CD
DO 17 J=1,NDRAG

```

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D 121
 D 122
 D 123
 D 124
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 D 128
 D 129
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 D 131
 D 132
 D 133
 D 134
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 D 136
 D 137
 D 138
 D 139
 D 140
 D 141
 D 142
 D 143
 D 144
 D 145

```

    ETASTG=B1/A1
    IF (B2) 20,19,20
    XISON=1.005/A2
    GO TO 23
    XISON=(A2**2+4.0*B2*1.005)
    IF (XISON) 21,21,22
    XISON=1.005/A2
    GO TO 23
    XISON=(-A2+SQRT(XISON))/(2.0*B2)
    ETASON=(XISON**2+B1)/A1
    IF (B) 25,24,25
    XSTAG=0.5*(1.0-ETASTG**2)
    GO TO 26
    XSTAG=(1.-SQRT(1.-B*B*(ETASTG**2)))/B
    STAG=XSTAG
    RETURN
  C
  C
    FORMAT (1X119(1H*))/1X119(1H*))/5X6HDELTA=E15.7/3X8HB(BODY)=E15.7/
    13X8MR(BODY)=E15.7/1X119(1H*))/1X119(1H*)
    FORMAT (5X23HNO ROOT FOR DELTA,DELM=E15.7,5X5HDELP=E15.7)
    FORMAT (5X48HINSUFFICIENT NUMBER OF BODY POINTS FOR CURVE FIT)
    FORMAT (10X3HNO.,15X3HETA,15X2HXI,15X4HMACH)
    FORMAT (112,E25.6,3E18.6)
    END
  
```

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 C
 C
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1 2 3 4 5 6 7 8 9 10
E E E E E E E E E E

```

SUBROUTINE XY (XI,ETA,B,X,R,FA,SQROOT)
  SQROOT=SQRT(1.0-B*B*ETA**2)
  FA=SQRT(1.-B*(XI**2))
  IF (B) 2,1,2
  X=0.5*(1.0+XI**2-ETA**2)
  GO TO 3
  X=(1.0-FA*SQROOT)/B
  R=ETA*X
  RETURN
END

```

1 2 3

1	1	1	1
2	2	2	2
3	3	3	3
4	4	4	4
5	5	5	5
6	6	6	6
7	7	7	7
8	8	8	8
9	9	9	9
10	10	10	10
11	11	11	11
12	12	12	12
13	13	13	13
14	14	14	14
15	15	15	15
16	16	16	16
17	17	17	17
18	18	18	18
19	19	19	19
20	20	20	20
21	21	21	21
22	22	22	22
23	23	23	23
24	24	24	24
25	25	25	25
26	26	26	26
27	27	27	27
28	28	28	28
29	29	29	29
30	30	30	30
31	31	31	31
32	32	32	32
33	33	33	33
34	34	34	34
35	35	35	35
36	36	36	36
37	37	37	37
38	38	38	38
39	39	39	39
40	40	40	40

```

SUBROUTINE DIFATE (NX,OX,YBLK,DFX,D2FX)
DIMENSION YBLK(100),FBLK(9),DEL1(6),DEL2(5),DEL3(4),DEL4(3),DEL5(2)
1)
IF (NX-4) 3,1,1
DO 2 I=1,6
NXI=NX-4+I
DEL1(I)=YBLK(NXI+1)-YBLK(NXI)
GO TO 6
DO 4 I=1,6
FBLK(I+3)=YBLK(I)
FBLK(I)=YBLK(3)
FBLK(2)=YBLK(2)
FBLK(3)=YBLK(1)
DO 5 I=1,6
NXI=NX+I-1
DEL1(I)=FBLK(NXI+1)-FBLK(NXI)
DO 7 I=1,5
DEL2(I)=DEL1(I+1)-DEL1(I)
DO 8 I=1,4
DEL3(I)=DEL2(I+1)-DEL2(I)
DO 9 I=1,3
DEL4(I)=DEL3(I+1)-DEL3(I)
DO 10 I=1,2
DEL5(I)=DEL4(I+1)-DEL4(I)
DEL6=DEL5(2)-DEL5(1)
BIG1=AMAX1(ABS(DEL1(1)),ABS(DEL1(2)),ABS(DEL1(3)),ABS(DEL1(4)),ABS
1(DEL1(5)),ABS(DEL1(6)))
BIG2=AMAX1(ABS(DEL2(1)),ABS(DEL2(2)),ABS(DEL2(3)),ABS(DEL2(4)),ABS
1(DEL2(5)))
BIG3=AMAX1(ABS(DEL3(1)),ABS(DEL3(2)),ABS(DEL3(3)),ABS(DEL3(4)))
BIG4=AMAX1(ABS(DEL4(1)),ABS(DEL4(2)),ABS(DEL4(3)))
BIG5=AMAX1(ABS(DEL5(1)),ABS(DEL5(2)))
DFX=(DEL1(3)+DEL1(4))/(2.0*DX)
IF (BIG2-BIG1) 12,11,11
D2FX=0.0
GO TO 16
D2X=DX**2
D2FX=DEL2(3)/D2X
IF (BIG3-BIG2) 13,16,16
D2FX=DFX-(DEL3(2)+DEL3(3))/(12.0*DX)

```

41
F
42
F
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F
45
F
46
F
47
F

IF (BIG4-BIG3) 14,16,16
D2FX=D2FX-(DEL4(2)/(12.0*D2X))
IF (BIG5-BIG4) 15,16,16
DFX=DFX+(DEL5(1)+DEL5(2))/(60.0*DX)
D2FX=D2FX+(DEL6/(90.0*D2X))
RETURN
END

14
15
16

1	1	SUBROUTINE IDTHER (YA,E,F,P,AE,T,SY,SE,BM,FA,SQROOT)	6
2	2	COMMON /ALPHA/ X,R,PTOP,CPI,DETA,ETASTG,XISON,ETASON,GG(15),ACHM2	6
3	3	1,DEM,XXB(88),YV8(88),ACH(100),STAG,Q000FL(10),DETA02	6
4	4	COMMON /BETA/ G,DETB,DY,ARBE,BEE,CARD,R,ACHM,GAMA,ALFA,ELAM,RINGS,	6
5	5	1CPR(88),OME05,MDM	6
6	6	COMMON /KLAPHA/ IBY,META,KPRNT,NB,KDIM,KQM(10),MP	6
7	7	NETA=NETA	6
8	8	PR=GG(1)*ACHM2	6
9	9	PTR=(GG(1)*ACHM2*F)*(-GG(9))	6
10	10	TERM=PR/(PTOP)*PTR	6
11	11	IF (TERM-1.0) 2,2,1	6
12	12	WRITE (6,16) PR,PTR,TERM	6
13	13	TERM=1.0	6
14	14	BM=0.0	6
15	15	GO TO 3	6
16	16	TERM=TERM*(-GG(4))	6
17	17	BM=SQRT((TERM-1.0)*GG(8))	6
18	18	TR=(1.0+GG(2)*ACHM2)/(1.0+GG(2)*BM**2)	6
19	19	ROOT2=TR*(BM/ACHM)**2	6
20	20	IF (ROOT2) 4,5,5	6
21	21	WRITE (6,15) TR,BM,ACHM	6
22	22	VR=SQRT(ROOT2)	6
23	23	TD=57.29578*TR	6
24	24	IF (E-1.0) 7,6,6	6
25	25	DEL=T-ATAN(SIN(T))/(COS(T)*AE))	6
26	26	GO TO 8	6
27	27	DEL=ATAN((E/YA)*(FA/SQROOT))+ATAN((-SY/SE)*(FA/SQROOT))	6
28	28	DELD=57.29578*DEL	6
29	29	WRITE (2) X,R,BM,PTR,PR,DELD	6
30	30	IF (E-1.0) 10,9,9	6
31	31	WRITE (2) TD	6
32	32	IF (IBY) 13,13,11	6
33	33	WRITE (6,17) X,R,BM,VR,PTR,PR,AE,DELD	6
34	34	IF (E-1.0) 13,12,12	6
35	35	WRITE (6,14) TD	6
36	36	RETURN	6
37	37		6
38	38		6
39	39	FORMAT (1M+,110X,F9.5)	6
40	40	FORMAT (5X,17HROOT2 FAILURE,TR=E14.6,5X,3HBM=E14.6,5X,3HAM=E14.6)	6

16
17

FORMAT (5X3HPR=E13.6/10X4HPTR=E15.6/15X5HTERM=E15.6)
FORMAT (2E13.6,OPF11.7,5E13.6,OP2F9.5)
END

G 41
G 42
G 43


```

SUBROUTINE IMAIN (NYY)
  INITIAL VALUE PROGRAM FOR 3-D MOC
  COMMON /ALPHA/ X,R,PTOP,CPI,DETA,ETASTG,XISON,ETASON,GG(15),ACHM2
1,DEM,XXB(88),YVB(88),ACH(100),STAG,Q000FL(10),DETAQ2
  COMMON /BETA/ G,DETB,DY,ARBE,BEE,CARD,B,ACHM,GAMA,ALFA,ELAM,RINGS,
  ICPR(88),ONEOS,NOM
  COMMON /KLAPHA/ IBY,NETA,KPRNT,NB,KDIM,KOM(10),MP
  DIMENSION PR(100),PB(100),DEN(100),FNS(100),TH(100),STRM(100),
  IDSTRY(100),D2STRY(100),DSTRM(100),D2STNY(100),D2STRM(100),DPDN(100
  2),DPDY(100),DSORDS(100),DSORDP(100),DSORDD(100),SAV2(100),PBXY(3,
  388),FNXY(3,88),DSYXY(3,88),DSNX(3,88),STRXY(3,88)
  DATA CPR/88*0.0/
  REWIND 2
  Q000FL(2)=1.0-B
  DETAD2=DETA*0.5
  NBDY=0 SF00=0.0
  NY=NYY
  WRITE (6,89) B,DETA,DY,G
  NB=0
  NETA=1
  ETA=1.0
  ETAL=1.0
  Y=0.5*DY
  ACHL=ACHM
  LINES=16
  IF (KPRNT-1) 2,1,1
  WRITE (6,71)
  WRITE (6,82)
  DO 8 I=1,NY
    TH(I)=ATAN(SQRT(1.0-(B*Y**2)))/Y
    CALL XY (Y,ETA,B,X,R,FA,SQ)
    ACHN=ACHL*SIN(TH(I))
    ACHN2=ACHN**2
    PR(I)=(12.0*ACHN2)-GG(4))/Q000FL(5)
    PB(I)=PR(I)
    DEN(I)=(GG(5)*ACHN2)/(GG(6)*ACHN2+2.0)
    DRT=(Q000FL(6))/(1.0+GG(2)*(ACHL**2)))*GG(9)
    DEN(I)=DEN(I)*DRT
    FNS(I)=PR(I)/(DEN(I)*GG(11))
    CALL IOTHER (Y,ETA,FNS(I),PR(I),DEN(I),TH(I),0.0,0.0,ACH(I),FA,SQ)

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1 H
2 H
3 H
4 H
5 H
6 H
7 H
8 H
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11 H
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39 H

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C

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H

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3      STRM(I)=(Y*KOM(1))/Q000FL(3)
      DSTRY(I)=Y*KDIM
      D2STRY(I)=DEM*Y*(KOM(2))
      DSTRN(I)=DEN(I)*(Y*KOM(1))
      IF (I-88) 3,3,4
      FNXY(1,I)=FNS(I)
      PBXY(1,I)=PB(I)
      DSNXY(1,I)=DSTRY(I)
      DSNXY(1,I)=DSTRN(I)
      STRXY(1,I)=STRM(I)
      IF (KPRNT-1) 8,5,5
      IF (LINES-45) 7,7,6
      LINES=1
      WRITE (6,84)
      WRITE (6,82)
      LINES=LINES+1
      Y=Y+DY
      WRITE (6,70) META,ETA,NY
      X=0.0
      ACML=ACHH
      ACML=ACML**2
      PBST=((2.0*ACML)-GG(4))/(GG(5)*ACHL)
      DENST=(GG(5)*ACHL)/(GG(6)*ACHL+2.0)
      FNST=PBST/(DENST*GG(1))
      IF (KPRNT-3) 10,9,9
      WRITE (6,72) ETA
      WRITE (6,85)
      Y=0.5*DY
      IF (KPRNT-3) 13,11,11
      DO 12 I=1,NY
      WRITE (6,69) Y,STRM(I),DSTRY(I),D2STRY(I),DSTRN(I)
      Y=Y+DY
      NTR=1
      IF (KPRNT-3) 16,15,15
      WRITE (6,73) ETA
      WRITE (6,86)
      Y=0.5*DY
      DO 18 I=1,NY
      SSQ=Q000FL(3)*STRM(I)
      SSQ2=SSQ*(2.0*Q000FL(1))

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17	F1=1.0+(Q000FL(2))*SSQ2	M	90
18	F2=(ACHM2)*(1.0-B*SSQ2)	M	81
	F3=Q000FL(4)/(GG(6)*(SSQ*(KOM(2))))	M	82
	F4=(1.0/F2)*(1.0/(2.0*F1+GG(6)*F2))	M	83
	F5=(1.0/(F1*(GG(10)*F2-GG(6)*F1))	M	84
	DSORDS(1)=F3*(F4-F5)	M	85
	DSORDP(1)=GG(9)/PR(1)	M	86
	DSORDD(1)=-(GG(3)/DEN(1))	M	87
	IF (KPRNT-3) 18,17,17	M	88
17	WRITE (6,74) Y,SSQ,F1,F2,F3,F4,F5,DSORDS(1),DSORDP(1),DSORDD(1)	M	89
18	Y=Y+DY	M	90
	NY3=NY-3	M	91
	DO 19 I=1,NY3	M	92
	CALL DIFATE (1,DY,DSTRN,D2STNY(1),D2)	M	93
	CALL DIFATE (1,DY,PR,DPOY(1),D2)	M	94
19	CONTINUE	M	95
	IF (KPRNT-3) 21,20,20	M	96
20	WRITE (6,75) (D2STNY(1),I=1,NY3)	M	97
	WRITE (6,76) (DPOY(1),I=1,NY3)	M	98
	WRITE (6,77) ETA	M	99
	WRITE (6,87)	M	100
21	Y=0.5*DY	M	101
	AD=1.0-B	M	102
	D7=AD+(8*ETA**2)	M	103
	D16=ETA**2	M	104
	D17=DEM/ETA	M	105
	D18=-B*ETA	M	106
	DO 24 I=1,NY3	M	107
	YSQ=Y**2	M	108
	D1=1.0-B*YSQ	M	109
	D2=(Y*ETA)*(KOM(3))	M	110
	D3=(AD*YSQ)+D16	M	111
	DSTRY2=DSTRY(1)**2	M	112
	DSDN=DSORDD(1)*DEN(1)	M	113
	D1002=D1/D2	M	114
	D4=(DEN(1)*D3)+(D1002)*(DSTRY2)*(DSORDP(1)/DSDN)	M	115
	IF (D4) 25,25,22	M	116
22	D5=(D1002)*(DSORDS(1)*(DSTRY2)*DSTRN(1))/DSDN	M	117
	ETA003=ETA/D3	M	118
	D6=D1002*DSTRY2*((ETA003)+(D17)-(D2STNY(1)/DSTRY(1)))	M	119

23	DSTRN2=DSTRN(I)*2	H 120
	D8=ETA03*07*DSTRN2/D2	H 121
	D9=(DSOROS(I)*DSTRY(I)-DSOROP(I)*DPOY(I))/OSDN	H 122
	DIM0Y=DEM/Y	H 123
	D10=D10D2*(DSTRY(I)*DSTRN(I))*((B*Y/D1)+DIM0Y-(D2STRY(I)/DSTRY(I)	H 124
	1+D9)	H 125
	OPDN(I)=(D5+D6+D8-D10)/D4	H 126
	CY0D3=A0*Y/D3	H 127
	D11=(D7/D2)*DSTRN2*(-(CY0D3)-DIM0Y-D9+(D2STNY(I)/DSTRN(I)))	H 128
	D12=CY0D3*D1*DSTRY2/D2	H 129
	D13=DEM(I)*D3*DPOY(I)	H 130
	D14=(D2/(D7*DSTRY(I)))*(D11-D12+D13)	H 131
	D15=(DSOROS(I)*DSTRN(I))-(OPDN(I)*DSOROP(I))/DEM(I)	H 132
	D2STRN(I)=D14+DSTRN(I)*((D18)/D7)+D17+(D15/DSORDD(I))	H 133
	IF (KPRNT-3) 24,23,23	H 134
	WRITE (6,68) Y,D1,D2,D3,D4,D5,D6,D7,D8,D9,D10,D11,D12,D13,D14,D15,	H 135
	1OPDN(I),D2STRN(I)	H 136
	Y=Y+DY	H 137
	GO TO (26,52), NTR	H 138
24	NY3=1-1	H 139
25	NY=NY3+3	H 140
	GO TO (26,52), NTR	H 141
26	IF (ETA-1.0) 62,27,27	H 142
27	ETA=ETA-DETA	H 143
	Y=0.5*DY	H 144
	NY=NY-3	H 145
	NETA=NETA+1	H 146
	IF (KPRNT-3) 29,28,28	H 147
28	WRITE (6,67)	H 148
	WRITE (6,88)	H 149
29	DO 32 I=1,NY	H 150
	SAV1=DSTRN(I)	H 151
	SAV2(I)=OPDN(I)	H 152
	DSTRN(I)=DSTRN(I)-(DETA*D2STRN(I))	H 153
	STRN(I)=STRN(I)-DETA02*(SAV1+DSTRN(I))	H 154
	PR(I)=PR(I)-(DETA*OPDN(I))	H 155
	IF (PR(I)) 33,33,30	H 156
30	SSQ=(Q0000FL(3)*STRN(I))*((KOM(4))	H 157
	F1=1.0+Q0000FL(2)*SSQ	H 158
	F2=ACHW2*(1.0-8*SSQ)	H 159

31	F3=(2.0*F2-F1*GG(4))/(F1*Q000FL(5))	H 160
	F4=(2.0*F1+GG(6)*F2)/(GG(5)*F2)	H 161
	FNS(I)=F3*(F4*GG(1))	H 162
	DEN(I)=(PR(I)/FNS(I))*GG(7)	H 163
	IF (KPRNT-3) 32,31,31	H 164
	WRITE (6,66) Y,SAVI,SAV2(I),DSTRN(I),STRM(I),PR(I),SSQ,F1,F2,F3,F4	H 165
	1,FNS(I),DEN(I)	H 166
32	Y=V+DY	H 167
	GO TO 34	H 168
33	NY=I-2	H 169
34	IF (META-4) 48,35,35	H 170
35	Y=0.5*DY	H 171
	IF (KPRNT-2) 37,36,36	H 172
36	WRITE (6,84)	H 173
37	IKP=KPRNT	H 174
	KPRNT=KPRNT+2	H 175
	IBZ=IBY	H 176
	IBY=MP	H 177
	DO 44 I=1,NY	H 178
	IF (STRM(I)) 38,40,44	H 179
38	IF (STRXY(1,I)) 44,44,39	H 180
39	CALL ENTRPG (STRXY(1,I),STRXY(2,I),STRXY(3,I),ETA1,ETA2,ETA3,0.0,	H 181
	1ETA)	H 182
	CALL ENTRPG (ETA1,ETA2,ETA3,PBX(1,I),PBXY(2,I),PBXY(3,I),ETA,E,PBE	H 183
	1)	H 184
	FNE=FNST	H 185
	DENE=(PBE/FNE)*GG(7)	H 186
	CALL ENTRPG (ETA1,ETA2,ETA3,DSYXY(1,I),DSYXY(2,I),DSYXY(3,I),ETA,E,	H 187
	1DSYE)	H 188
	CALL ENTRPG (ETA1,ETA2,ETA3,DSNXY(1,I),DSNXY(2,I),DSNXY(3,I),ETA,E,	H 189
	1DSNE)	H 190
	CALL XY (Y,ETA,E,B,X,R,FA,SQROOT)	H 191
	CONTINUE	H 192
40	CALL IOTHER (Y,ETA,E,FNE,PBE,DENE,TH(1),DSYE,DSNE,ACHE,FA,SQROOT)	H 193
	ACH(I)=ACHE	H 194
	CPR(I)=(2.0*PBE-CPI)	H 195
	IF (ACHE-1.0) 41,41,43	H 196
	IF (I-NB-1) 42,42,43	H 197
41	NB=I	H 198
42		H 199
43	XXB(I)=X	

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44      YVB(I)=R
      NBDY=I
      Y=Y+DY
      IBY=IBZ
45      DO 45 I=1,NBDY
      CPR(I)=CPR(I)+YVB(I)
      KPRNT=IKP
      IF (NB) 48,48,46
46      NBI=NB+2
      DO 47 I=NBI,NY
      ACH(I)=0.0
      CALL BODY (NBDY)
      NB=NB+1
      GO TO 65
48      NY3=NY-3
      DO 49 I=1,NY3
      CALL DIFATE (I,DY,STRM,DSTRY(I),D2STRY(I))
49      CONTINUE
      IF (KPRNT-3) 51,50,50
50      WRITE (6,79) (DSTRY(I),I=1,NY3)
      WRITE (6,80) (D2STRY(I),I=1,NY3)
51      NTR=2
      GO TO 14
52      IF (KPRNT-2) 54,53,53
53      WRITE (6,81) ETA
      WRITE (6,78)
      WRITE (6,83)
54      Y=0.5*DY
      DO 59 I=1,NY3
      PB(I)=PB(I)-DETA02*(SAV2(I)+DPDN(I))
      IF (PB(I)) 61,61,55
55      DEN(I)=(PB(I)/FNS(I))*GG(7)
      CALL XY (Y,ETA,B,X,R,FA,SQROOT)
      CALL IDTHER (Y,ETA,FNS(I),PB(I),DEN(I),FOO,DSTRY(I),DSTRN(I),ACH(I)
      1),FA,SQROOT)
      IF (KPRNT-2) 59,56,56
56      IF (LINES-33) 58,58,57
57      LINES=1
      WRITE (6,84)
      WRITE (6,83)

```

H 240
H 241
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H 276
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H 278
H 279

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58 LINES=LINES+1
59 Y=Y+DY
60 NY=NY-3
61 WRITE (6,70) META,ETA,NY
62 GO TO 26
63 NY3=1-1
64 NY=NY3
65 GO TO 60
66 DETA=G*DETA
67 DETA02=DETA*0.5
68 DO 63 I=1,86
69 PBXY(3,I)=PBXY(2,I)
70 FNXY(3,I)=FNXY(2,I)
71 DSYXY(3,I)=DSYXY(2,I)
72 DSNXY(3,I)=DSNXY(2,I)
73 STRXY(3,I)=STRXY(2,I)
74 PBXY(2,I)=PBXY(1,I)
75 FNXY(2,I)=FNXY(1,I)
76 DSYXY(2,I)=DSYXY(1,I)
77 DSNXY(2,I)=DSNXY(1,I)
78 STRXY(2,I)=STRXY(1,I)
79 PBXY(1,I)=PB(I)
80 FNXY(1,I)=FNS(I)
81 DSYXY(1,I)=DSTRY(I)
82 DSNXY(1,I)=DSTRM(I)
83 STRXY(1,I)=STRM(I)
84 ETA3=ETA2
85 ETA2=ETA1
86 ETA1=ETA
87 NY3=NY-3
88 IF (STRM(NY3)) 65,65,64
89 IF (META-10) 27,65,65
90 RETURN
91
92 FORMAT (8F8.4,5E11.4)
93 FORMAT (17H1FIELD POINT DATA)
94 FORMAT (10F6.3,8F7.3)
95 FORMAT (5F12.5)

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OVERLAY (BLUNT,2,0)	1	2
PROGRAM IVLS	1	3
COMMON /BETA/ G,DETA,DY,RBODY,8BODY,DELTA,8,VN,GAMA,CM1,CM2,CM3,	1	4
ICPR(88),ONE05,MOM	1	5
DIMENSION X(100,10),Y(100,10),DF(100,10),VM(100,10),P(100,10),SR(1	6
1100,10),DUMMY(100,10,6),L(10),XA(10),YA(10),DFA(10),VMA(10),PA(10)	1	7
2,SRA(10),DUMMZ(10,6),TH(100)	1	8
DIMENSION ETA(10)	1	9
COMMON /ALPHA/ DUMMY,DUMMZ,TH	1	10
EQUIVALENCE (X(1,1),DUMMY(1,1,1)), (Y(1,1),DUMMY(1,1,2)), (DF(1,1)	1	11
1,DUMMY(1,1,3)), (VM(1,1),DUMMY(1,1,4)), (P(1,1),DUMMY(1,1,5)), (SR	1	12
2(1,1),DUMMY(1,1,6)), (XA(1),DUMMZ(1,1)), (YA(1),DUMMZ(1,2)), (DFA(1	13
31),DUMMZ(1,3)), (VMA(1),DUMMZ(1,4)), (PA(1),DUMMZ(1,5)), (SRA(1),	1	14
4DUMMZ(1,6))	1	15
RAD=57.29578	1	16
REWIND 2	1	17
ISLOPE=0	1	18
SBODY=1.0/RBODY	1	19
RBODY=1.0	1	20
DELTA=DELTA*SBODY	1	21
LBACK=0	1	22
I=1	1	23
J=1	1	24
1 READ (2) X(I,J),Y(I,J),VM(I,J),SR(I,J),P(I,J),DF(I,J)	1	25
X(I,J)=X(I,J)*SBODY	1	26
Y(I,J)=Y(I,J)*SBODY	1	27
IF (I-1) 3,3,2	1	28
IF (Y(I,J)-Y(I-1,J)) 7,7,3	1	29
IF (J-1) 4,4,5	1	30
READ (2) TH(I)	1	31
I=I+1	1	32
IF (I-100) 1,1,6	1	33
I=1	1	34
L(J)=100	1	35
GO TO 10	1	36
IF (I-2) 12,12,8	1	37
L(J)=I-1	1	38
DO 9 K=1,6	1	39
DUMMY(I,J+1,K)=DUMMY(I,J,K)	1	40
DUMMY(I,J,K)=0.0	1	41

10	I=2				1	42
	J=J+1				1	43
	IF (J-10) 1,1,11				1	44
11	J=10				1	45
	GO TO 13				1	46
12	J=J-1				1	47
13	IMAX=0				1	48
	WRITE (6,54) VM,GAMA,RBODY,BBODY,DELTA				1	49
	CALL BBOUT (J,L)				1	50
	M=1				1	51
	N=J				1	52
14	LL=L(N)				1	53
	DO 15 I=1,LL				1	54
	IF (VM(I,N)-1.0) 15,15,16				1	55
15	CONTINUE				1	56
16	WRITE (6,53) M,N,LL				1	57
	CALL ENTRPG (VM(I-2,N),VM(I-1,N),VM(I,N),X(I-1,N),X(I,N),				1	58
	11.0,X1)				1	59
	CALL ENTRPG (VM(I-2,N),VM(I-1,N),VM(I,N),Y(I-1,N),Y(I,N),				1	60
	11.0,Y1)				1	61
	IF (N-J) 18,17,17				1	62
17	X2=X1				1	63
	Y2=Y1				1	64
	SLOPET=1.0				1	65
	XMAX=X2				1	66
	YMAX=Y2				1	67
	ISB=1				1	68
	GO TO 20				1	69
18	SLOPES=((Y1-Y2)/(X1-X2))				1	70
	TLOPES=(ATAN(SLOPES))*RAD+175.0				1	71
	SLOPES=SIN(TLOPES/RAD)/COS(TLOPES/RAD)				1	72
	IF (SLOPES-SLOPET) 19,20,20				1	73
19	SLOPET=SLOPES				1	74
20	IF (1-IMAX) 22,21,21				1	75
21	IMAX=1				1	76
	XMAX=X1				1	77
	YMAX=Y1				1	78
22	N=N-1				1	79
23	IF (N) 23,23,14				1	80
	ETA(1)=1.0				1	81

DO 24 I=2,J	1	82
ETA(I)=ETA(I-1)-DETA	1	83
DETA=DETA*G	1	84
SLOPES=SLOPET	1	85
XO=RBODY+DELTA	1	86
WRITE (6,59)	1	87
SLOPE=YMAX/(XMAX-XO)	1	88
IF (SLOPE.GT.SLOPES) I SLOPE=1	1	89
CALL ENTRPG (VM(ISB-1,J),VM(ISB-2,J),VM(ISB-3,J),X(ISB-1,J),X(ISB-	1	90
12,J),X(ISB-3,J),ONE05,XQ)	1	91
CALL ENTRPG (VM(ISB-1,J),VM(ISB-2,J),VM(ISB-3,J),Y(ISB-1,J),Y(ISB-	1	92
12,J),Y(ISB-3,J),ONE05,YQ)	1	93
SLOPE=YQ/(XQ-XO)	1	94
IF (I SLOPE) 27,27,26	1	95
XO=XQ-YQ/SLOPES	1	96
SLOPE=SLOPES	1	97
DO 39 I=1,J	1	98
IF (I-J) 31,28,28	1	99
XB=((I SLOPE**2)*XO+RBODY+880DY*DELTA)/(SLOPE**2+880DY)	1	100
XC=((I SLOPE*XO)**2+(2.0*RBODY+880DY*DELTA)*DELTA)/(SLOPE**2+880DY)	1	101
XB=XB-SQRT(XB**2-XC)	1	102
LM=L(J)	1	103
DO 29 L4=ISB,LM	1	104
IF (XB-X(L4,J)) 30,30,29	1	105
CONTINUE	1	106
LBACK=LBACK+1	1	107
K=LM+1-LBACK	1	108
ONE05=FLOAT(IFIX(VM(K,J)*100.))/100.0	1	109
WRITE (6,52) ONE05	1	110
GO TO 25	1	111
F3=L4	1	112
L4=LM	1	113
F2=L4-1	1	114
F1=L4-2	1	115
NZ=F1	1	116
CALL ENTRPG (X(L4-2,J),X(L4-1,J),X(L4,J),F1,F2,F3,XB,FB)	1	117
CALL DETER (L4-2,J,FB)	1	118
GO TO 39	1	119
RM=SLOPE/ETA(I)	1	120
RP=RM*XO/SBODY	1	121

	RK=(1.0-B*B*(ETA(I)**2))	I 122
	TERM=B*RK*(RM**2)	I 123
	T1=B*(1.0+RK*RM*RP)/(B*TERM)	I 124
	T2=SQRT(B*RK*(TERM-(B*RP-RM)**2))/(B*TERM)	I 125
	XP=T1+T2	I 126
	XM=T1-T2	I 127
	IF (XP/XM) 32,35,35	I 128
	IF (XP) 33,33,34	I 129
	XI=XM	I 130
	GO TO 36	I 131
	XI=XP	I 132
	GO TO 36	I 133
	XI=AMIN1(XP,XM)	I 134
	Z1=SQRT(1.-(1.-B*XI)**2/RK)/B)	I 135
	Z=(Z1/DY)+0.5	I 136
	NZ=Z-1.0	I 137
	IF (NZ-L(I)+1) 37,38,38	I 138
	CALL DETER (NZ,I,Z)	I 139
	GO TO 39	I 140
	WRITE (6,58) NZ,L(I),I	I 141
	GO TO 51	I 142
	CONTINUE	I 143
	IF (NZ+2-L(J)) 42,42,41	I 144
	NZ=NZ-1	I 145
	GO TO 40	I 146
	SLOPE=(ATAN(RBODY-(XA(J)-DELTA)*BODY)/YA(J))*57.29578	I 147
	DSLOPE=(DFA(J)-SLOPE)/SQRT((XA(I)-XA(J))**2+(YA(I)-YA(J))**2)	I 148
	DO 43 I=2,J	I 149
	DFA(I)=DFA(I)-DSLOPE*SQRT((XA(I)-XA(I))**2+(YA(I)-YA(I))**2)	I 150
	IF (ISLOPE) 46,46,44	I 151
	DO 45 KJ=1,6	I 152
	DUMNZ(J,KJ)=DUMNY(ISB-1,J,KJ)	I 153
	CALL ENTRPG (Y(ISB-1,J),Y(ISB,J),Y(ISB+1,J),CPR(ISB-1),CPR(ISB),	I 154
	1,CPR(ISB+1),YA(J),CD)	I 155
	WRITE (6,60)	I 156
	WRITE (6,55) VN,GAMA	I 157
	WRITE (6,61)	I 158
	WRITE (6,55) DELTA,RODDY,BODY	I 159
	WRITE (6,57) CD,Y(ISB+1,J),CPR(ISB+1),Y(ISB,J),CPR(ISB),Y(ISB-1,J)	I 160
	1,CPR(ISB-1),YA(J)	I 161

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47 WRITE (6,62)
DO 47 I=1,J
WRITE (6,56) DUMMZ(I,1),DUMMZ(I,2),DUMMZ(I,3),DUMMZ(I,4),DUMMZ(I,6)
1)
CONTINUE
A=0.0
S=SR(1,J)
LL=L(1)
DO 48 NZ=1,LL
IF (Y(NZ,1)-YA(1)) 48,49,49
CONTINUE
DUMMY(NZ,1,2)=DUMMZ(1,2)
DUMMY(NZ,1,6)=DUMMZ(1,6)
WRITE (6,63)
WRITE (6,55) A,S,(DUMMY(I,1,2),DUMMY(I,1,6),I=1,NZ)
NZ=NZ+1
WRITE (3) CM1,CM2
K=J
WRITE (3) K,NMZ,CD,VN,GAMA,DELTA,CM3
WRITE (3) A,S,(DUMMY(I,1,2),DUMMY(I,1,6),I=1,NZ)
DO 50 LLL=1,J
I=J+1-LLL
WRITE (3) DUMMZ(1,1),DUMMZ(1,2),DUMMZ(1,3),DUMMZ(1,4),DUMMZ(1,6)
CONTINUE
REWIND 3

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52 FORMAT (37H0_INTERPOLATION MACH NO. DECREASED TO,611.4,34HDUE TO L
LIMITATION ON BODY MACH NO./)
53 FORMAT (5X32H0ID NOT FIND SUPERSONIC POINT,M=12/30X2HN=12/29X3HLL=
112)
54 FORMAT (1H15X3HCOMPLETE FLOW FIELD NORMALIZED BY R80DY///20X2HM=
1F15.6/20X5HGAMA=F12.6/20X3HRB=E18.6/20X2HB=E19.6/20X6HDELTA=E15.6)
55 FORMAT (6E20.7)
56 FORMAT (5E20.7)
57 FORMAT (11X6HCPA(1)/E45.6/E15.6/E45.6/E15.6/E45.6/E15.6/20X19HINTERPOL
ATED FOR Y=E20.6)
58 FORMAT (5X3HNZ=15,5X5HL(1)=15,2H1=15/5X14HCANNOT PROCEED)
59 FORMAT (1H1)

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60	FORMAT (1X,23HINITIAL VALUE LINE DATA/5X8MMACH NO.,12X5HGAMMA)	I 202
61	FORMAT (///5X5HDELTA,15X5HRCDDY,15X5HBBODY)	I 203
62	FORMAT (///5X26HIVL DATA,STARTING AT SHOCK/9X1HX,19X1HY,19X5HDELTA	I 204
	1,15X8MMACH NO.,12X6HPT/PTO)	I 205
63	FORMAT (///1X18HMASS-ENTROPY TABLE)	I 206
	END	I 207

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SUBROUTINE DETER (N1,J,Z)
  DIMENSION DUMMY(100,10,6),DUMMZ(10,6),TH(100)
  COMMON /ALPHA/ DUMMY,DUMMZ,TH
  F1=N1
  F2=N1+1
  F3=N1+2
  N2=N1+1
  N3=N1+2
  DO 1 I=1,6
    CALL ENTRPG (F1,F2,F3,DUMMY(N1,J,I),DUMMY(N2,J,I),DUMMY(N3,J,I),Z,
    1DUMMZ(J,I))
  CONTINUE
  RETURN
  END

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1	K	SUBROUTINE BBOUT (J,L)
2	K	DIMENSION X(100,10),Y(100,10),DF(100,10),VM(100,10),P(100,10),SR(
3	K	100,10),DUMMY(100,10,6),L(10),XA(10),YA(10),DFA(10),VMA(10),PA(10)
4	K	2,SRA(10),DUMMZ(10,6),TH(100)
5	K	DIMENSION T(9)
6	K	COMMON /ALPHA/ DUMMY,DUMMZ,TH
7	K	COMMON /BETA/ G,DETB,DY,ARBE,BEE,CARD,AC,ACHM,GAMA,ALFA,ELAM,RINGS
8	K	1,CPR(88),ONEOS,MDM
9	K	EQUIVALENCE (X(1,1),DUMMY(1,1,1)), (Y(1,1),DUMMY(1,1,2)), (DF(1,1)
10	K	1,DUMMY(1,1,3)), (VM(1,1),DUMMY(1,1,4)), (P(1,1),DUMMY(1,1,5)), (SR
11	K	2(1,1),DUMMY(1,1,6)), (XA(1),DUMMZ(1,1)), (YA(1),DUMMZ(1,2)), (DFA(
12	K	31),DUMMZ(1,3)), (VMA(1),DUMMZ(1,4)), (PA(1),DUMMZ(1,5)), (SRA(1),
13	K	4DUMMZ(1,6))
14	K	GG6=GAMA-1.0
15	K	GG2=GG6*0.5
16	K	GG7=1.0/GAMA
17	K	GG9=-GG6*GG7
18	K	VMM=1.0+GG2*(ACHM**2)
19	K	LIM=46
20	K	J=J
21	K	L(1)=L(1)
22	K	DO 6 I=1,J
23	K	MM=1
24	K	IF (I-1) 1,1,2
25	K	WRITE (6,30)
26	K	GO TO 3
27	K	WRITE (6,31)
28	K	MAX=L(1)
29	K	WRITE (6,28)
30	K	DO 7 M=1,MAX
31	K	IF (1.EQ.1) WRITE (6,27) TH(M)
32	K	IF (1.GT.1) WRITE (6,28)
33	K	TEM=VMM/(1.0+GG2*(VM(M,1)/ACHM)**2)
34	K	VEL=SQRT(TEM*(VM(M,1)/ACHM)**2)
35	K	DEN=(P(M,1)*GG7)/SR(M,1)*GG9
36	K	WRITE (6,33) X(M,1),Y(M,1),VM(M,1),VEL,SR(M,1),P(M,1),TEN,DEN,DF(M
37	K	1,1)
38	K	MM=MM+1
39	K	IF (MM-LIM) 7,7,4
40	K	LIM=55

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MM=1
WRITE (6,26)
IF (I-1) 5,5,6
WRITE (6,30)
GO TO 7
WRITE (6,31)
CONTINUE
WRITE (6,26)
DO 24 IP=1,2
GO TO (10,9), IP
WRITE (6,29)
GO TO 11
WRITE (6,25)
DO 24 I=1,J
MAX=L(I)
GO TO (12,16), IP
DO 13 M=1,MAX
IF (DUMMY(M,I,4)-1.0) 13,14,14
CONTINUE
C3=MAX
M3=MAX
WRITE (6,32)
GO TO 15
C3=M
M3=M
M2=M3-1
C2=M2
M1=M2-1
C1=M1
CALL ENTRPG (DUMMY(M1,I,4),DUMMY(M2,I,4),DUMMY(M3,I,4),C1,C2,C3,
11.0,AD)
GO TO 17
AD=0
C1=0.5
C2=1.5
C3=2.5
M1=1
M2=2
M3=3
DO 18 IT=1,6

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18 CALL ENTRPG (C1,C2,C3,DUMMY(M1,I,IT),DUMMY(M2,I,IT),DUMMY(M3,I,IT)
1,AD,T(IT))
IF (I-1) 19,19,23
GO TO (20,21), IP
20 CALL ENTRPG (C1,C2,C3,TH(M1),TH(M2),TH(M3),AD,IT)
GO TO 22
21 TT=90.0
22 WRITE (6,30)
IF (I.EQ.1) WRITE (6,27) TI
IF (I.GT.1) WRITE (6,28)
23 T(8)=VMM/(1.0+GG2*T(4))
T(7)=SQR(T(8)*(T(4)/ACHM)**2)
T(9)=(T(5)/T(6))*GG7
WRITE (6,33) T(1),T(2),T(4),T(7),T(6),T(5),T(8),T(9),T(3)
24 CONTINUE
RETURN
C
C
25 FORMAT (17HSONIC POINT DATA)
26 FORMAT (1M)
27 FORMAT (1H,112XF9.5)
28 FORMAT (1)
29 FORMAT (17HSTAGNATION POINT DATA)
30 FORMAT (120H0
1 TOT PRES PRESSURE TEMPERATURE X MACH NO
2) DENSITY DENSITY VELOCITY DELTA THETA
31 FORMAT (111H0
1 TOT PRES PRESSURE TEMPERATURE X MACH NO
2) DENSITY DENSITY VELOCITY DELTA
32 FORMAT (1X,24HINTERPOLATED SONIC POINT)
33 FORMAT (1H+,2E13.6,OPF11.7,5E13.6,OP2F9.5)
END

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C	OVERLAY (BLUNT,3,0)	L
	PROGRAM MOCS	L
	EXECUTIVE PROGRAM FOR IDEAL GAS CHARACTERISTICS	L
	COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(L
	1100,2),GF(115),VMASS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(L
	23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS	L
	3,VMSON,RAD,XLAST,AMUO,VMW,ISONIC,PO,TEST,R,DFP,BSONIC,PM,FMO,IHP,	L
	4VFS,TYPE,TESU,BL,PSONIC,XSTAR8,REF,RFIT,EL,TIN,DSONIC,RV2,CD,DET,	L
	5DW,SH	L
	COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,	L
	IKICK,NOW,ILK,NS2,ID(100,2),INCASE,ISPEC	L
	COMMON /TRANS/ LO,LI,LL,MS	L
	COMMON /BETA/ D(7),ACHM,GAMA,ALFA,ELAMDA,RINGS,CPR(90),BDRAG	L
	HOL(70)=RATIO OF PREVIOUS TO PRESENT MESH SIZE=HOL(I+2)/HOL(I+1)	L
	HOL(69)=1,BODY INDICATE TO MESH P.,MESH SIZE FOR NEW SEG NOT FINAL	L
	HOL(68)=SHOCK ANGLE FROM WAVE	L
	HOL(63)=1 RADIAN	L
	HOL(62)=PI	L
	HOL(60)=NUMBER OF POINTS CALCULATED ON CURRENT CHARACTERISTIC.	L
	HOL(59)=INDICATES POINT TO BE DROPPED AFTER SEC. SHOCK	L
	HOL(58)=VMAX/V-FREE STREAM	L
	HOL(57)=BODY SURFACE MASS FLOW RATIO	L
	HOL(54)=INDICATOR TO CARRY OUT IVL TRANSITION	L
	HOL(53)=STEP SIZE ALONG BODY DURING IVL TRANSITION	L
	HOL(52)=BODY SURFACE TOTAL PRESSURE	L
	HOL(50)=SUMMARY NO. FOR START OF CHECKOUT PRINT	L
	HOL(49)=SUMMARY NO. FOR END OF CHECKOUT PRINT	L
	HOL(48)=INDICATOR TO BODY SUBR TO CUT MESH SIZE DUE TO ENVELOPE SH	L
	HOL(47)=INDICATOR TO BODY PT S-R THAT MESH SIZE IS NOT FINAL	L
	HOL(46)=1, TELLS SHOCK PROGRAM TO TRY TERMINAL MODE	L
	HOL(45)=+1 FOR EXTERNAL MODE, =-1 FOR INTERNAL MODE	L
	HOL(40)=INDICATOR THAT A SPECIAL POINT FOLLOWS PREVIOUS ONE	L
	HOL(39)=STEP SIZE ADJUSTMENT	L
	HOL(3-28)=XSTAR8 OR MESH SIZE FOR SEG. 1,2,.....26 RESPECTIVELY	L
	HOL(2)=1, INDICATE TO MAIN,SUBSONIC PT.,AVOID DOWN S. ANGULAR CALC.	L
	HOL(1)=1, INDICATE TO BODY,SUBSONIC PT. ENCOUNTERED,NO (K-1,J-1)PT.	L
	PART 1 INITIAL VALUE LINE	L
	JOLT=0	L
	XSTAR8=0.0	L
	RAD=57.29578	L

```

1 CALL SLITE (1)
  CALL PAGE (0)
  DO 1 I=1,72
    HOL(1)=0.0
    HOL(63)=1.5707963
    HOL(62)=3.1415927
    HOL(38)=0.5
    HOL(39)=0.5*(1.0+HOL(38))
    TEST=1.0E-06
    TESU=2.0E-06
    ISPEC=0
    DO 2 I=1,2
      DO 2 J=1,100
        ID(J,I)=0
        ILK=0
        ISEG=0
        KICK=0
        XSTAR=0.0
        YIN=0.0
        NB=0
        LOOP=0
      2
    1
2
3
  MEND=0
  REF=0
  IST=0
  KPIO=1
  MID=1
  NSUM=1
  LO=1
  REF=1.0
  READ (5,74) INCASE,HOL(50),HOL(49),HOL(3)
  IPUNCH=4
  HOL(45)=+1.0
  DO 3 I=1,4
    AB(I)=0.0
    AC(I)=0.0
    AD(I)=0.0
    AE(I)=0.0
    READ (3) HOL(27),HOL(26)
    HOL(27)=HOL(27)/RAD
  3

```



```

HOL(26)=HOL(26)/RAD
HOL(25)=HOL(27)
HOL(24)=HOL(26)
ALFA=HOL(27)
ELAMDA=HOL(26)
HOLDIF=HOL(27)-HOL(26)
HOL(22)=1.0-SIN(ALFA+ELAMDA)
HOL(27)=TAN(HOL(27))
HOL(26)=SIN(HOLDIF)+1.0
HOL(24)=HOL(26)-HOL(27)*COS(HOLDIF)
HOL(23)=-HOLDIF
CALL SHAPE
NSEGM=NSEG-1
EL=XB(NSEGM)
XSPEC(1)=0.0
XSPEC(1)=XB(1)
XSPEC(2)=2.0
READ(3) NIV,NSRV,CD,VMFS,GF(1),DET,RINGS
RFIT=1.0
AMUO=ANGLE(VMFS)
GF(2)=GF(1)-1.0
GF(3)=GF(1)+1.0
GF(4)=(GF(1)-1.0)*0.5
GF(5)=(GF(1)+1.0)*0.5
GF(6)=(GF(1)-1.0)/(GF(1)+1.0)
GF(7)=GF(1)*0.5
GF(8)=(GF(1)+1.0)*2
GF(9)=GF(1)*2.0
GF(10)=GF(1)/(GF(1)-1.0)
GF(11)=1.0/(GF(1)-1.0)
GF(12)=2.0/(GF(1)-1.0)
GF(13)=(GF(1)-1.0)/GF(1)
GF(14)=SORT((GF(1)-1.0)/2.0)
GF(15)=1.0/GF(1)
HOL(58)=1.0/VELOC(VMFS,GF(4))
IF (HOL(50)) 4,5,5
NSRV=-NSRV
HOL(50)=ABS(HOL(50))
HID=1
WRITE (6,70)

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4

5

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KPR=KPIO
LEFT=0
VFS=VMFS
HOL(51)=LEFT
PFS=(1.0+GF(4)*VMFS**2)**(-GF(10))
RV2=GF(7)*(VMFS**2)*((1.0+GF(4)*(VMFS**2))**(-GF(10)))
NEX=0
CALL OUTPUT (1.0,0)
REF2=REF*(MID+1)
CD=CD*(R/REF)**(MID+1)
DEN=MID
IF (INCASE.GT.2) CALL OUTPUT (2.0,0)
DETERMINATION OF SONIC SHOCK PROPERTIES
TSONIC=TSON(VMFS,GF(2),GF(3),GF(1))
CALL WAVE (TSONIC,HOL(37),VMFS,PFS,1.0,1)
PSONIC=PM
VMSON=VMW
DSONIC=DM
BSONIC=ANGLE(VMW)
INTRODUCE CONSTANTS INTO ENTROPY AND READ IN ENTROPY W/Y-REF
CALL ENTROPY (VELOC(VMFS,GF(4))*((R/RFIT)**(MID+1)),DEM,3,NSRV)
NOW=1+NEX
CALL INPUT (2.1,1)
NS2=0
ID(1,1)=0
NNOW=1
HOL(52)=SR(1,1)
IF (X(1,1)-XB(1)) 6,7,7
X11=X(1,1)+HOL(41)
DF(1,1)=ATAN((R-BL*X11)/SQRT((2.0*R-BL*X11)*X11))
CALL OUTPUT (6.1,1)
IF (VM(1,1)-1.0) 8,8,9
NSKIP=1
HOL(1)=1.0
HOL(2)=1.0
GO TO 10
NSKIP=0
NB=NB+1
CPBMB=(P(NNOW,1)-PFS)/RV2
YLAST=Y(NNOW,1)

```

C

C

6

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11 XLAST=X(NNOW,1)
12 CPI=CPBMB*Y(NNOW,1)
    HOL(60)=1-LEFT+MEX
    DO 32 J=2,NIV
    NOW=HOL(60)
    HOL(60)=1.0
    CALL INPUT (1,1,2)
    IF (NIV-J) 12,12,13
    CALL WAVE (DF(1,2),HOL(37),VMFS,PFS,1.0,2)
    THS(1,2)=HOL(60)
    VM(1,2)=VMW
    P(1,2)=PW
    SR(1,2)=SW
    ID(1,2)=+1
    NS2=1
    CALL OUTPUT (6,1,2)
    IF (NOW) 19,19,14
    IF (HOL(2)) 15,15,19
    CALL DROP (1,2,NJUMP,IDROP)
    GO TO (16,30,30,30), NJUMP
    CALL OPER8 (IRD)
    IF (KICK-1) 17,20,32
    GO TO (19,18,32), IRD
    NOW=HOL(60)
    GO TO 23
    HOL(2)=0.0
    CALL BOD1
    NAM=HOL(60)+1.0
    IF (X(NAM,2).LE.HOL(22)) LO=NSUM
    L1=NSUM
    IF (KICK-1) 22,20,32
    IF (INCASE-4) 21,32,32
    INCASE=4
    GO TO 11
    HOL(60)=HOL(60)+1.0
    NOW=HOL(60)
    NB=NB+1
    CPBMB=(P(NOW,2)-PFS)/RV2
    CP2=CPBMB*Y(NOW,2)
    CD=(CPI+CP2)*(Y(NOW,2)-YLAST)/REF2+CD

```

24	CPI=CP2	L 202
25	CALL OUTPUT (8,1,2)	L 203
	IF (INCASE-1) 30,27,24	L 204
	IF (J-NIV) 26,25,25	L 205
	THP=THS(1,2)*RAD	L 206
	CALL OUTPUT (4,1,2)	L 207
	GO TO 30	L 208
26	CALL OUTPUT (5,1,2)	L 209
	GO TO 30	L 210
27	IF (J-NIV) 29,28,28	L 211
28	WRITE (6,72)	L 212
	CALL OUTPUT (7,1,2)	L 213
	THP=THS(1,2)*RAD	L 214
	WRITE (6,73) THP	L 215
	WRITE (6,69)	LA215
29	CALL OUTPUT (7,NOM,2)	L 216
C	SET FIRST DIM TO SECOND DIM. ELEMENTS THEN ALL SECOND DIM. TO 0	L 217
30	CALL CHANGE (7,1)	L 218
	CALL CHANGE (5,1)	L 219
	DO 31 K=1,2	L 220
	THS(K,1)=THS(K,2)	L 221
31	THS(K,2)=0.0	L 222
	XLAST=X(NOM,1)	L 223
	YLAST=Y(NOM,1)	L 224
	NS2=0	L 225
32	CONTINUE	L 226
	IF (KICK) 33,33,68	L 227
33	HOL(54)=1.0	L 228
	HOL(69)=1.0	L 229
	HS=NSUM-2	L 230
C	PART 2 SHOCK-TO BODY CALCULATIONS	L 231
	TIN=1.0	L 232
	HOL(51)=0.0	L 233
34	IF (HOL(40)) 36,36,35	L 234
35	ILK=HOL(40)	L 235
36	L5=1	L 236
	NS2=0	L 237
	IF (HOL(28).NE.0.0) XSTAR=XSTAR*1.1	L 238
	IF (TIN-1.0) 38,38,37	L 239
37	NOM=NOMH	L 240

C	RESET ALL FIRST DIM. ELEMENTS TO SAVED VALUES REG. W/ELEMENT TWO	L 241
	CALL CHANGE (2,1)	L 242
	GO TO 39	L 243
38	NOON=NOW	L 244
39	CALL SHOCK (1,L5)	L 245
	XLIM=HOL(24)+Y(1,2)*HOL(27)	L 246
	IGO=3	L 247
	IF ((X(1,2)-GT.XLIM).OR.(NOW.LT.3)) GO TO 44	L 248
	IF (KICK-1) 42,40,68	L 249
40	IF (INCASE-4) 41,68,68	L 250
41	INCASE=4	L 251
	GO TO 36	L 252
42	IF (MEND) 46,46,43	L 253
43	IF (NOW-2) 45,45,46	L 254
44	CONTINUE	L 255
45	NOW=1	L 256
	GO TO 62	L 257
46	CALL OPER8 (IRD)	L 258
	IF (HOL(28)) 48,48,47	L 259
47	IF (HOL(60).EQ.2.0) GO TO 67	L 260
	GO TO 55	L 261
48	CONTINUE	L 262
	IF (KICK-1) 51,49,68	L 263
49	IF (JOLT) 50,50,68	L 264
50	KICK=0	L 265
	JOLT=1	L 266
	GO TO 40	L 267
51	GO TO (52,55,68,39), IRD	L 268
52	IF (MEND) 54,54,53	L 269
53	NOW=HOL(60)	L 270
	GO TO 62	L 271
54	CALL BODI	L 272
	NEW=HOL(60)+1.0	L 273
	IF (X(NEW,2)-LE.HOL(22)) LO=NSUM	L 274
	IF (KICK-1) 56,49,68	L 275
55	NEW=HOL(60)	L 276
56	IF (INCASE-4) 58,57,58	L 277
57	WRITE (6,69)	L 278
	CALL OUTPUT (7,NEW,2)	L 279
58	NOON=NOW	L 280

59	NOW=NEW	L 281
	IF (HOL(28)) 59,59,62	L 282
	CONTINUE	L 283
	CALL MESH (IGO)	L 284
	NOW=NOON	L 285
	ILK=ILK	L 286
	GO TO (60,68,61,61), IGO	L 287
C	DROP ALL TEMPORARY SR ENTRIES	L 288
60	CALL ENTROP (0.0,0.0,6.0)	L 289
	GO TO 34	L 290
61	NB=NB+1	L 291
	NOW=NEW	L 292
	L1=NSUM	L 293
	CPBNS=(P(NOW,2)-PFS)/RV2	L 294
	CP2=CPBNS*Y(NOW,2)	L 295
	CD=(CP1+CP2)*(Y(NOW,2)-YLAST)/REF2+CD	L 296
	CP1=CP2	L 297
C	RETAIN ALL TEMPORARY SR ENTRIES	L 298
62	CALL ENTROP (0.0,0.0,5.0)	L 299
	XLAST=X(NOW,2)	L 300
	YLAST=Y(NOW,2)	L 301
C	SET FIRST DIM TO SECOND DIM. ELEMENTS THEN ALL SECOND DIM TO 0	L 302
	CALL CHANGE (7,1)	L 303
	CALL CHANGE (5,1)	L 304
	DO 63 K=1,2	L 305
	THS(K,1)=THS(K,2)	L 306
63	THS(K,2)=0.0	L 307
	THP=THS(1,1)*RAD	L 308
	TIN=1.0	L 309
	LOOP=0	L 310
	CALL OUTPUT(8,1,1)	L 3105
	IF (INCASE-1) 66,64,65	L 311
	WRITE (6,72)	L 312
64	CALL OUTPUT (7,1,1)	L 313
	IF (NOW.EQ.1) GO TO 68	L 3135
	WRITE (6,71)	L 314
	WRITE (6,69)	L 315
	CALL OUTPUT (7,NOW,1)	L 316
	GO TO 66	L 317
65	CALL OUTPUT (4,1,1)	L 318

66	CONTINUE	L 319
67	IF (NOW-1) 68,68,34	L 320
	MEND=1	L 321
	MOL(46)=1.0	L 322
	IGO=3	L 323
68	GO TO 34	L 324
	LL=NSUM-1	L 325
	BORAG=CD	
C		L 327
69	FORMAT (1X,10H800Y POINT)	L 328
70	FORMAT (1X,44(1H*),27HROTATIONALLY SYMMETRIC FLOW,56(1H*))	L 329
71	FORMAT (1H-)	L 330
72	FORMAT (1X,11HSHOCK POINT)	L 331
73	FORMAT (14X,12HTHETA SHOCK=E13.6)	L 332
74	FORMAT (11,F3.0,F2.0,E18.6)	L 333
	END	L 334


```

8  IF (ILK) 10,10,9
9  I=ILK
   XTRY=XSPEC(I)
   GO TO 29
10  XTRY=XLAST+XSTARB*MOL(39)
   IF (XTRY-MOL(31)) 11,12,12
11  XTRY=MOL(31)
   CONIC, CUBIC, ORRADIUS TYPE OF BODY
12  DO 13 KK=1,NSEG
   I=KK
   IF (XTRY-XB(I)) 14,13,13
13  CONTINUE
   WRITE (6,123)
   GO TO 31
14  IF (XSTAR) 15,15,16
15  ISEG=1
   XSTAR=MOL(1+2)
   XSTARB=XSTAR
   GO TO 28
16  ISEG1=ISEG-1
   IF (ISEG1) 17,20,20
17  IMO=1-1
   DO 18 M=ISEG,IMO
   IF (XSPEC(M)) 19,18,19
18  CONTINUE
   M=1
19  XSTARB=MOL(M+2)
   ISEG=M
   IF (MOL(54)) 24,24,21
20  MOL(54)=MOL(54)+1.0
21  IF ((XSTARB/MOL(53))-2.0) 22,23,23
22  MOL(54)=0.0
   MOL(69)=0.0
   GO TO 34
23  XSTAR=XSTAR*2.0
   GO TO 34
24  IF (ISEG1) 25,29,29
25  MOL(70)=MOL(1+2)/MOL(1+1)
   IF (MOL(70)-2.0) 26,27,27
26  XSTAR=XSTAR*MOL(70)

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27      HOL(69)=0.0
        GO TO 28
        XSTAR=2.0*XSTAR
        HOL(69)=1.0
        HOL(70)=HOL(70)/2.0
28      IF (HOL(72)) 34,34,33
29      IF (HOL(69)) 34,34,30
30      IF (HOL(70)-1.0) 31,32,32
31      HOL(69)=0.0
        GO TO 28
32      XSTAR=2.0*XSTAR
        HOL(70)=HOL(70)/2.0
33      GO TO 28
        HOL(72)=0.0
        GO TO 122
34      N11=1
        X3=XTRY
        D3=D1
        VM3=VM1
        AMU3=AMU1
        P3=((1.0+GF(4))*(VM3**2))*(-GF(10)))*S3
        DIMU1=D1-AMU1
35      N1=1
36      J1SEG=IABS(J1(I))+1
        IF (I-1) 37,37,38
37      J1SEG=1
38      X2=X3
        TANAV=TAN((DIMU1+D3-HOL(45)*AMU3)*.5)
        GO TO (39,46), J1SEG
39      BB=2.0*TANAV*(Y1-TANAV*X1)-2.0*R+2.0*BL*HOL(41)
        AAA=BL+TANAV**2
        CC=(Y1-TANAV*X1)**2+HOL(41)*(BL*HOL(41)-2.0*R)
        IF (AAA.NE.0.0) GO TO 40
        X3=-CC/BB
        GO TO 43
40      SQ=BB/(2.0*AAA)
        TQ=SQ**2-CC/AAA
        IF (TQ) 41,41,42
41      I=I+1
        GO TO 17

```

42	X3=-SQ-SORT(TQ)	M 121
43	Y3=SQRT(12.0*R-BL*(X3+HOL(41)))*(X3+HOL(41))	M 122
	IF (INCASE-4) 45,44,44	M 123
44	WRITE (6,130) X3,AAA,BB,CC	M 124
45	D3=ATAN((R-BL*(X3+HOL(41)))/Y3)	M 125
	GO TO 49	M 126
C	CUBIC TYPE BODY	M 127
46	IF (HOL(45)) 47,48,48	M 128
47	X3=(Y1-Y(L,M)+X(L,M)*AD(1)-X1*TANAV)/(AD(1)-TANAV)	M 129
	XX=X3-X(L,M)	M 130
	Y3=AD(1)*XX+AE(1)	M 131
	GO TO 77	M 132
48	XX=X3-XB(1-1)	M 133
	Y3=((AB(1)*XX+AC(1))*XX+AD(1))*XX+AE(1)	M 134
	D3=(3.0*AB(1)*XX+2.0*AC(1))*XX+AD(1)	M 135
	X3=X3-(Y3-(X3-X1)*TANAV-Y1)/(D3-TANAV)	M 136
	D3=ATAN(D3)	M 137
49	IF (N1-99) 52,50,50	M 138
50	WRITE (6,131) N1	M 139
51	KICK=KICK+1	M 140
	GO TO 122	M 141
52	IF (INCASE-4) 54,53,53	M 142
53	WRITE (6,132) N1,X3,I	M 143
54	N1=N1+1	M 144
	IF (ABS(X3)-TEST) 55,55,56	M 145
55	IF (ABS(X3-X2)-TEST) 57,38,38	M 146
56	IF (ABS((X2/X3)-1.0)-TEST) 57,38,38	M 147
57	IF (LOOP+IPOT) 58,58,69	M 148
58	IF (X3-XB(1)) 60,60,59	M 149
59	IUP=1	M 150
	I=I+1	M 151
	GO TO 63	M 152
60	IF (I-1) 69,69,61	M 153
61	IF (XB(1-1)-X3) 69,62,62	M 154
62	IDW=1	M 155
	I=I-1	M 156
63	IF (INCASE-4) 65,64,64	M 157
64	WRITE (6,133) I	M 158
65	IPOT=IUP+IDW	M 159
	IF (IPOT) 66,36,66	M 160

66	IF (ILK) 67,67,68	M 161
67	I=IUP	M 162
	GO TO 36	M 163
68	I=ILK	M 164
	GO TO 36	M 165
69	IF (N11-1) 70,70,76	M 166
70	IF (VM(NOW,1)-1.0) 71,71,74	M 167
71	P3=P(NOW,1)+((S3-PFS)*SIN(D3+DF(NOW,1))*SIN(D3-DF(NOW,1)))	M 168
72	VM3=SQRT(GF(12)*((P3/S3)*(-GF(13))-1.0))	M 169
	AMU3=ANGLE(VM3)	M 170
	IF (INCASE-4) 76,73,73	M 171
73	WRITE (6,141) P3,D3,VM3,AMU3	M 172
	GO TO 76	M 173
74	DNV=DF(NOW,1)-D3	M 174
	T1=VM(NOW,1)*2	M 175
	P3=(1.0-((GF(1)*T1)/SQRT(T1-1.0))*DNV)*P(NOW,1)	M 176
75	IF (P3) 75,75,72	M 177
	P3=P(NOW,1)	M 178
	GO TO 72	M 179
76	D3M1=D3-D1	M 180
77	DS=SQRT((X3-X1)*2+(Y3-Y1)*2)	M 181
	YAV=(Y1+Y3)*0.5	M 182
	AVD=(D1+D3)*0.5	M 183
	SAVD=SIN(AVD)	M 184
	IF (HOL(45)) 78,79,79	M 185
78	B2=SAVD*SIMU*DS/YAV	M 186
	RT=B1+B2	M 187
	B3=D1-RT	M 188
	RESID=D3-B3	M 189
	GO TO 80	M 190
79	AVMU=(AMU1+AMU3)	M 191
	S2MU=SIN(AVMU)	M 192
	AVMU=0.5*AVMU	M 193
	S1MU=SIN(AVMU)	M 194
	B1=G1/S2MU	M 195
	B2=D3M1-DEM*SAVD*SIMU*DS/YAV	M 196
	RT=B1+B2	M 197
	RESID=RT-ALOG(P3/P1)	M 198
80	IF (ABS(RESID)-TESU) 105,81,81	M 199
81	IF (INCASE-4) 83,82,82	M 200

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82 WRITE (6,136) RESID,P3,D3M1,DS,YAV,AVMU,AVD,SAVO,S2MU,SIMU,B1,B2,
1RT,S3

83 IF (MOL(45)) 84,85,85

84 D3=83

85 GO TO 102

86 IF (M11-1) 86,86,89

87 R1=RESID

88 P31=P3

89 IF (ABS(RT)-88.028) 88,87,87

90 MOL(61)=1.0

91 GO TO 122

92 P3=P1+EXP(RT)

93 MOL(61)=0.0

94 GO TO 93

95 IF (RESID/R1) 90,90,88

96 R2=RESID

97 P32=P3

98 P3=P31-R1*(P3-P31)/(R2-R1)

99 IF (INCASE-4) 92,91,91

100 WRITE (6,127) P3,P32,R2,P31,R1

101 P31=P32

102 R1=R2

103 IM=0

104 IMM=0

105 VM3=VMACH(P3,S3,GF(12),GF(13))

106 IF (VM3-1.0) 95,95,94

107 IM=0

108 GO TO 99

109 IM=IM+1

110 IF (TIM) 97,97,96

111 MOL(61)=1.0

112 GO TO 122

113 VM3=1.0

114 AMU3=1.5707963

115 P3=((1.0+GF(4))*(-GF(10)))*S3

116 IF (IM-25) 100,100,98

117 WRITE (6,140)

118 GO TO 51

119 AMU3=ANGLE(VM3)

120 IF (INCASE-4) 102,101,101

101	WRITE (6,128) N11	M 241
102	WRITE (6,129) X3,Y3,D3,P3,RESID,AMU3	M 242
103	N11=N11+1	M 243
104	IF (N11-50) 103,103,104	M 244
105	IF (MOL(45)) 38,35,35	M 245
106	WRITE (6,134) RESID,RT,I	M 246
107	GO TO 51	M 247
108	IF (MOL(45)) 116,106,106	M 248
109	IF (IMM+IM) 108,108,107	M 249
110	WRITE (6,135) IMM,IM,VM3	M 250
111	GO TO 51	M 251
112	IF (ILK) 109,109,116	M 252
113	IF (X3-XB(1)) 112,116,110	M 253
114	I=I+1	M 254
115	IF (I-NSEG) 35,35,111	M 255
116	WRITE (6,126) X3,XB(I-1)	M 256
117	GO TO 51	M 257
118	IF (I-2) 113,114,114	M 258
119	GO TO 116	M 259
120	IF (X3-XB(I-1)) 115,116,116	M 260
	I=I-1	M 261
	GO TO 35	M 262
	IF (INCASE-2) 118,118,117	M 263
	WRITE (6,125)	M 264
	WRITE (6,129) X3,Y3,D3,P3,RESID,VM3	M 265
	X(K+1,J)=X3	M 266
	Y(K+1,J)=Y3	M 267
	OF(K+1,J)=O3	M 268
	P(K+1,J)=P3	M 269
	VM(K+1,J)=VM3	M 270
	SR(K+1,J)=S3	M 271
	ID(K+1,J)=0	M 272
	MOL(53)=X3-X(MOW,1)	M 273
	IF (INCASE-4) 120,119,119	M 274
	WRITE (6,139) XSTAR0,MOL(53),MOL(54),ISEGMI	M 275
	CONTINUE	M 276
	RAY2=((P3/PFS)*GF(15))*GF(13)*GF(14)/SQRT(1.0+GF(4)*VM3**2	M 277
	1))*GF(13)*GF(14)/SQRT(1.0+GF(4)*VM3**2	M 278
	DS=SQRT((X3-X1)**2+(Y3-Y1)**2)	M 279
	FMASS=VMASS(K)-(1.0+DEM)*0.5*(RAY1+RAY2)*DS	M 280

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121 VMASS(K+1)=FMASS
122 HOL(57)=FMASS/VMASS(1)
123 IF (INCASE-4) 122,121,121
124 WRITE (6,138) FMASS,VMASS(1),HOL(57)
125 RETURN
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VMASS(K+1)=FMASS
 HOL(57)=FMASS/VMASS(1)
 IF (INCASE-4) 122,121,121
 WRITE (6,138) FMASS,VMASS(1),HOL(57)
 RETURN

 FORMAT (29H0 X1 LIES BEYOND LAST SEGMENT)
 FORMAT (1X125(1H*))
 FORMAT (1X,13H***BODY POINT)
 FORMAT (30H POINT LIES BEYOND END OF BODY,3HX3=E15.7,3HX8=E15.7)
 FORMAT (16H INTERPOLATED P=E15.6/4H P3=E15.7,4H R2=E15.6,5(1H),5H
 1 P31=E15.6,4H R1=E15.6)
 FORMAT (12H0 PITERATION15)
 FORMAT (5H0 X3=E15.8,4H Y3=E15.8,4H D3=E15.8,4H P3=E15.8,6HRESID=
 IE15.8,6H AMU3=E15.8)
 FORMAT (5(1H),4H X3=E15.6,4H AA=E15.6,4H BB=E15.6,4H CC=E15.6)
 FORMAT (19H0 ITERATION FAILED15)
 FORMAT (1H05X3MNI=15/9X3HX3=E15.6,5X5HISEG=15)
 FORMAT (5X20HSEGMENT CHANGE,ISEG=15)
 FORMAT (61HOFailure IN BODY PROG. EXCEEDED 50 ITERATIONS IN OUTER
 LOOP. 7H RESID=E13.6,5H RT=E13.6,10H SEGMENT=13)
 FORMAT (5H0IMN=13,4H IM=13,5H VM3=E13.6)
 FORMAT (10H RESIDUAL=E13.6,6H P3=E13.6,6H D3M1=E13.6,6H DS=
 IE13.6,6H YAV=E13.6,6H AVMU=E13.6/6X4HAYD=E13.6,6H SAVD=E13.6,6H S
 22MU=E13.6,6H SIMU=E13.6/7X3HB1=E13.6,6H B2=E13.6,6H RT=E13.6,6
 3H S3=E13.6,24H IN BODY AT STATEMENT 35)
 FORMAT (54H0BODY PROG. IF HOL(72)=1 FULL CHAR READ,ONLY 1ST LINE
 143HBELOW VALID. IF HOL(1)=1 SUBS.PT.-HOL(72)=F3.1,8H HOL(1)=F4.1,
 25H TIN=F4.1/4H X1=E12.5,4H Y1=E12.5,4H P1=E12.5,6H AMU1=E12.5,4H D
 31=E12.5,4H S3=E12.5,4H K=15,4H J=15)
 FORMAT (22H RATIO=FMASS/VMASS(1)=E13.6,1H/E13.6,1H=E13.6)
 FORMAT (8H XSTARD=E13.6,9H HOL(53)=E13.6,9H HOL(54)=E13.6,8H ISEGM
 11=15)
 FORMAT (5X5(3H(*)),14HIM EXCEEDED 25)
 FORMAT (5X16HFIRST APPROX P3=E15.6/21X3MD3=E15.6/20X4HVM3=E15.6/
 119X5HAMU3=E15.6)
 END

1	N	
2	N	
3	N	
4	N	
5	N	
6	N	
7	N	
8	N	
9	N	
10	N	
11	N	
12	N	
13	N	
14	N	
15	N	
16	N	
17	N	
18	N	
19	N	
20	N	
21	N	
22	N	
23	N	
24	N	
25	N	
26	N	
27	N	
28	N	
29	N	
30	N	
31	N	
32	N	

```

SUBROUTINE OPER8 (IRD)
COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SRI
100,2),GF(15),VMAS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(
23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS
3,VMSON,RAD,XLAST,AMUO,VMW,TSONIC,PO,TEST,R,DFP,BSONIC,PW,FMO,THP,
4VFS,TYPE,TESU,BL,PSONIC,XSTAR8,REF,RFIT,EL,TIN,DSOINIC,RV2,CD,DET,
5DW,SW
COMMON /INTEG/ JI(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,
1KICK,NOM,ILK,NS2,IDI(100,2),INCASE,ISPEC
LIMIT=0
LEFT=HOL(51)
IF (TIN) 1,1,2
11=1+LEFT
GO TO 3
11=2
DO 6 I=11,NOM
IF (HOL(59)) 5,5,4
HOL(59)=HOL(59)-1.0
GO TO 6
L=1
CALL FIELD (I,L)
IH=HOL(60)
XLIM=HOL(24)+Y(IH,2)*HOL(27)
IF ((X(IH,2).GT.XLIM).AND.(1.LT.NOW)) HOL(28)=1.0
IF ((X(IH,2).GT.XLIM).AND.(1.LT.NOW).AND.(TIN.GT.0.)) LIMIT=LIMIT+
11
IF (LIMIT.EQ.2) GO TO 7
CONTINUE
IRD=1
IF (KICK.GT.0) IRD=3
RETURN
END

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1	0	SUBROUTINE FIELD (I0,J0)
2	0	COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(
3	0	1100,2),GF(15),VMASS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(
4	0	23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS
5	0	3,VMSON,RAD,XLAST,AMUO,VMW,TSOINIC,PO,TEST,R,DFP,BSONIC,PW,FMO,IHP,
6	0	4VFS,TYPE,TESU,BL,PSONIC,XSTAR,REF,RFIT,EL,TIN,DSOINIC,RV2,CD,DET,
7	0	SDW,SW
8	0	COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,
9	0	1KICK,NOW,ILK,NS2,ID(100,2),INCASE,ISPEC
10	0	IBALL=0
11	0	LBLOCK=0
12	0	IND=0
13	0	TEST=.000001
14	0	TESU=2.0E-05
15	0	J=JB
16	0	I=IB
17	0	L=HOL(60)
18	0	IF (L-1) 1,1,3
19	0	IF (TIN) 2,2,3
20	0	CALL ENTROP TO GET MASS AT SHOCK POINT
21	0	CALL ENTROP (SR(1,J+1),VMASS(1),2,0)
22	0	M=J+1
23	0	PR=P(L,M)
24	0	SZ=SR(L,M)
25	0	WR=VM(L,M)
26	0	XR=X(L,M)
27	0	YR=Y(L,M)
28	0	X1=X(L,M)
29	0	Y1=Y(L,M)
30	0	D1=DF(L,M)
31	0	P1=P(L,M)
32	0	S1=SR(L,M)
33	0	W1=VM(L,M)
34	0	K=HOL(60)
35	0	X2=X(I,J)
36	0	Y2=Y(I,J)
37	0	D2=DF(I,J)
38	0	P2=P(I,J)
39	0	S2=SR(I,J)
40	0	W2=VM(I,J)

1 C 2 3

41	0	
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44	0	
45	0	
46	0	
47	0	
48	0	
49	0	
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52	0	
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IT=0
IL=0
AMU1=ANGLE(W1)
AMU2=ANGLE(W2)
RAY1=((PR/PFS)*GF(15))*GF(13))*GF(14)/SQRT(1.0+GF(4)*WR**2)
1)*(YR**MID)
IF (INCASE-4) 5,4,4
WRITE (6,104) RAY1,VMA SS(K),K
P3=0.5*(P1+P2)
S3=(S1+S2)*0.5
W3=VMACH(P3,S3,GF(12),GF(13))
AMU3=ANGLE(W3)
O12=0.5*(O1+O2)
D3=D12
P1L=ALOG(P1)
P2L=ALOG(P2)
BEGIN GEOMETRIC PROCESS
IF (INCASE-4) 8,7,7
WRITE (6,101) IT
WRITE (6,99) X3,Y3,P3,W3,D3,S3
A13=0.5*(AMU1+AMU3)
A23=0.5*(AMU2+AMU3)
SA23=SIN(A23)
S2A23=SIN(2.0*A23)
S2A13=SIN(2.0*A13)
SA13=SIN(A13)
O13=0.5*(O1+O3)
S13=0.5*(O1-AMU1+O3-AMU3)
S23=0.5*(O2+AMU2+O3+AMU3)
D23=0.5*(O2+O3)
SD23=SIN(D23)
SD13=SIN(O13)
TAN2=TAN(S23)
TAN1=TAN(S13)
DELS=(S2-S1)*0.1
SBASIC=51
IFM=0
IF (TAN2-2.0) 9,9,11
IF (TAN1+2.0) 10,10,13
9 C NEITHER TANGENT GREATER THAN 2

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10	X3=(Y2-Y1-(X2*TAN2-X1*TAN1))/(TAN1-TAN2)	0 81
	Y3=(TAN1*TAN2*(X1-X2)+Y2*TAN1-Y1*TAN2)/(TAN1-TAN2)	0 82
	GO TO 15	0 83
11	IF (TAN1+2.0) 12,12,14	0 84
C	BOTH TANGENTS GREATER THAN 2	0 85
12	X3=(X1*TAN1-X2*TAN2+Y2-Y1)/(TAN2-TAN1)	0 86
	Y3=((X2-X1)*TAN2*TAN1+Y1*TAN2-Y2*TAN1)/(TAN2-TAN1)	0 87
	GO TO 15	0 88
C	UPPER TANGENT EXCEEDS 2	0 89
13	X3=((Y2-Y1)/TAN1+X1-X2*TAN2/TAN1)/(1.0-TAN2/TAN1)	0 90
	Y3=((X2-X1)*TAN2+Y1*TAN2/TAN1-Y2)/(TAN2/TAN1-1.0)	0 91
	GO TO 15	0 92
C	LOWER TANGENT EXCEEDS 2	0 93
14	X3=((Y2-Y1)/TAN2+X1*TAN1/TAN2-X2)/(TAN1/TAN2-1.0)	0 94
	Y3=((X2-X1)*TAN1+(Y1-Y2*TAN1/TAN2))/(1.0-TAN1/TAN2)	0 95
C	BEGIN COMPATABILITY EQUATIONS	0 96
15	IF (INCASE-4) 17,16,16	0 97
16	WRITE (6,97) X3,Y3,S3,W3	0 98
17	Y23=0.5*(Y2+Y3)	0 99
	Y13=0.5*(Y1+Y3)	0 100
	DOY23=SQRT((Y2-Y3)**2+(X2-X3)**2)/Y23	0 101
	DOY13=SQRT((Y1-Y3)**2+(X1-X3)**2)/Y13	0 102
	SXA=S3	0 103
	IF (LBLOCK) 18,18,32	0 104
18	T1=S2A23+S2A13	0 105
	T2=SD13*DOY13	0 106
	T3=SD23*DOY23	0 107
	T4=GF(15)*(P2L-P1L)	0 108
	T5=(D1*S2A23+D2*S2A13)	0 109
	T6=0.5*(S2A23+S2A13)	0 110
	D3=(T6*(T4+DEMO(T2/COS(A13)-T3/COS(A23)))+T5)/T1	0 111
	T7=S2A13*P1L+S2A23*P2L	0 112
	T8=D2-D1	0 113
	T9=T2*SAL3	0 114
	T10=T3*S2A23	0 115
	RT=(T7+GF(9)*(T8-DEMO(T9+T10)))/T1	0 116
	RESID=ALOG(P3)-RT	0 117
	IF (17-1) 22,23,19	0 118
19	IF (ABS(RESID)-TEST) 20,20,21	0 119
20	IF (ABS(S3/S31-1.0)-TEST) 78,78,21	0 120

21	IF (IT) 22,22,23	0 121
22	P31=P3	0 122
	P3=EXP(RT)	0 123
	R1=RESID	0 124
	GO TO 32	0 125
23	R2=RESID	0 126
	IF (R1) 24,26,24	0 127
24	IF (RESID/R1) 25,25,31	0 128
25	P32=P3	0 129
	DR=R2-R1	0 130
	IF (DR) 28,26,28	0 131
26	IF (ABS(R2)-TEST) 70,78,27	0 132
27	WRITE (6,98)	0 133
	GO TO 74	0 134
28	P3=P31-R1*(P3-P31)/DR	0 135
	IF (INCASE-4) 30,29,29	0 136
29	WRITE (6,91) P3,P32,R2,P31,R1	0 137
30	P31=P32	0 138
	R1=R2	0 139
	GO TO 32	0 140
31	P3=EXP(RT)	0 141
32	DS=SQR((X3-XR)**2+(Y3-YR)**2)	0 142
	S31=S3	0 143
	KSR=0	0 144
	KBLOCK=0	0 145
	IF (INCASE-4) 34,33,33	0 146
33	WRITE (6,96) T1,T2,T3,T4,T5,T6,T7,T8,T9,T10,D3,RT	0 147
34	IF (IFM) 36,36,35	0 148
35	S3=SBASIC+DELS*FLOAT(IFM-1)	0 149
	S3=S3	0 150
36	W3=VMACH(P3,S3,GF(12),GF(13))	0 151
	RAY2=((P3/PFS)*GF(19))*GF(13)*GF(14)/SQRT(1.0+GF(4))*(W3**2	0 152
	1))*GF(14)/SQRT(1.0+GF(4))*(W3**2	0 153
	FMASS=VMASS(K)-(1.0+DEM)*0.5*(RAY1+RAY2)*DS	0 154
	CALL ENTROP (S3,FMASS,1.0)	0 155
	KSR=KSR+1	0 156
	IF (INCASE-4) 38,37,37	0 157
37	WRITE (6,106) RAY2,FMASS,S3,DS	0 158
38	CONTINUE	0 159
	IF (KSR-1) 39,39,40	0 160

39	SIT=S3	0 161
	GO TO 34	0 162
40	IF (IFM-1) 52,42,41	0 163
41	SH=SG	0 164
	DELH=DELG	0 165
42	SG=SS3	0 166
	DELG=SG-S3	0 167
	IF (IFM-1) 50,50,43	0 168
43	IF (INCASE-4) 45,44,44	0 169
44	WRITE (6,92) IFM,SG,DELG,SH,DELH,S3	0 170
45	IF (DELG=DELH) 51,51,46	0 171
46	IF (ABS(DELH)-ABS(DELG)) 47,50,50	0 172
47	DELS=-DELS	0 173
	IBALL=IBALL+1	0 174
	IF (IBALL-1) 48,48,49	0 175
48	IFM=1	0 176
	SBASIC=SH	0 177
	GO TO 34	0 178
49	WRITE (6,105)	0 179
	KICK=1.0	0 180
	GO TO 86	0 181
50	IBALL=0	0 182
	IFM=IFM+1	0 183
	GO TO 34	0 184
51	S3=SG-DELG*((SG-SH)/(DELG-DELH))	0 185
	SIT=S3	0 186
	KBLOCK=KBLOCK+1	0 187
	DELS=(SG-SH)*0.1	0 188
	SBASIC=SH	0 189
	IFM=0	0 190
	GO TO 34	0 191
52	IF (ABS((S3/SIT)-1.0)-TEST) 59,59,53	0 192
53	IF (KSR-10) 39,39,54	0 193
54	IF (KBLOCK) 56,56,55	0 194
55	IF (KBLOCK-10) 56,56,58	0 195
56	IFM=1	0 196
	ITSAVE=IT	0 197
	TEST=TESU	0 198
	IT=2	0 199
	IF (LBLOCK) 57,57,34	0 200

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57  LBLOCK=1
    GO TO 34
58  WRITE (6,93)
    GO TO 85
59  IF (INCASE-4) 61,60,60
60  WRITE (6,90) P3,D3,S3,R2,R1,RAY2,FMASS
61  IMM=0
    IF (LBLOCK-1) 70,62,63
62  SXB=SXA
    DXB=S3-SXA
    KBLOCK=0
    LBLOCK=2
    GO TO 70
63  KBLOCK=0
    LBLOCK=LBLOCK+1
    DXA=S3-SXA
    SAVG=0.5*(SXA+SXB)
    IF (ABS(DXA/SAVG)-TESU) 64,64,65
64  LBLOCK=0
    IT=ITSAVE
    GO TO 70
65  IF (LBLOCK-25) 67,67,66
66  WRITE (6,94)
    GO TO 85
67  S3=SXA-DXA*((SXA-SXB)/(DXA-DXB))
    W3=VMACH(P3,S3,GF(12),GF(13))
    IF (INCASE-4) 69,68,68
68  WRITE (6,95) SXA,SXB,DXA,DXB,S3
69  SXB=SXA
    DXB=DXA
    IF (W3-1.0) 71,71,75
    I1=I1+1
    IF (I1-10) 72,72,73
72  P3=((1.0+GF(4))*(-GF(10)))*S3
    W3=1.0
    AMU3=1.5707963
    D3=D12
    IMM=IMM+1
    GO TO 6
73  WRITE (6,102) W3,P3,S3

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74	KICK=KICK+1	0 241
	GO TO 86	0 242
75	AMU3=ANGLE(W3)	0 243
	IT=IT+1	0 244
	II=0	0 245
76	IF (IT-50) 6,6,76	0 246
77	IF (IND-4) 77,88,88	0 247
	IND=IND+1	0 248
	IT=1	0 249
	TEST=TEST+10.0	0 250
	GO TO 6	0 251
78	IF (IMM+II) 79,79,87	0 252
79	HOL(60)=HOL(60)+1.0	0 253
	L=HOL(60)	0 254
	IF (HOL(45)) 80,81,81	0 255
80	M=J	0 256
	GO TO 82	0 257
81	M=J+1	0 258
82	X(L,M)=X3	0 259
	Y(L,M)=Y3	0 260
	P(L,M)=P3	0 261
	VM(L,M)=W3	0 262
	DF(L,M)=D3	0 263
	SR(L,M)=S3	0 264
	ID(L,M)=ID(18,J8)	0 265
	VMAS(L)=FMAS	0 266
	IF (IND) 84,84,83	0 267
83	WRITE (6,103) IND,L	0 268
84	IF (INCASE-4) 86,85,85	0 269
85	WRITE (6,99) X3,Y3,P3,W3,D3,S3	0 270
86	RETURN	0 271
87	WRITE (6,100) IMM,P3	0 272
88	WRITE (6,89)	0 273
	GO TO 74	0 274
		0 275
		0 276
		0 277
		0 278
89	FORMAT (40M EXCEEDED 3*50 ITERATIONS IN FIELD POINT)	0 279
90	FORMAT (4M P3=E15.6,3HD3=E15.6,3HS3=E15.6,3HR2=E15.6,3HR1=E13.6,6H	0 280
	1 RAY2=E13.6,7H FMAS=E13.6)	

91	FORMAT (16H INTERPOLATED P=E15.6/4H P3=E15.7,4H R2=E15.6,5(1H),5H	0 281
	1 P31=E15.6,4H R1=E15.6)	0 282
92	FORMAT (5X15,(5E15.7))	0 283
93	FORMAT (1X20(1H+),37HFAILED TO CONVERGE S3 IN SPECIAL LOOP)	0 284
94	FORMAT (5X20(1H-),31HFAILED TO CONVERGE D3 SLOW LOOP)	0 285
95	FORMAT (1X10(1H-),4HSXA=E15.6,5X4HSXB=E15.6,5X4HDXA=E15.6,5X4HDXB=	0 286
	1E15.6,5X3HS3=E15.6)	0 287
96	FORMAT (6E20.6/6E20.6)	0 288
97	FORMAT (30X3HX3=E15.7,5X3HY3=E15.7,5X3HW3=E15.7)	0 289
98	FORMAT (20H DR FAILURE IN FIELD)	0 290
99	FORMAT (4H0X3=E15.8,3HY3=E15.8,3HP3=E15.8,3HM3=E15.8,3HD3=E15.8,3H	0 291
	1S3=E15.8)	0 292
100	FORMAT (5X20HFAILED IN FIELD,1MM=15/4H P3=E15.6)	0 293
101	FORMAT (12H0 ITERATION I3)	0 294
102	FORMAT (55H TRIED 10 TIMES TO CONVERGE POINT BUT STILL SUBSONIC.	0 295
	13HM3=E13.6,7H P3=E13.6,7H S3=E13.6)	0 296
103	FORMAT (52H0***NOTE***CONVERGENCE CRITERIA MULTIPLIED BY 10**11,	0 297
	110H FOR POINTI3)	0 298
104	FORMAT (6H RAY1=E12.6,10H VMASS(K)=E12.6,3H K=I3)	0 299
105	FORMAT (1X29HOSCILLATION IN FIELD FOR DELS)	0 300
106	FORMAT (7H RAY2 =E15.5,5X7HFMAS =E15.5,5X4HS3 =E15.5,5X3HDS=E15.6	0 301
	1)	0 302
	END	0 303

FUNCTION VMACH (P,SR,G12,G13)
VMACH=SQRT(G12*((P/SR)**(-G13)-1.0))
RETURN
END

P 2
P 3
P 4
P 5

C	1	SUBROUTINE ENTROP (VAR1,VAR2,I1,I2)	Q	1
	2	*****IDEAL GAS VERSION *****	Q	2
C	3	DIMENSION QUAN(2,100),SSRG(100),SGMASS(100)	Q	3
	4	WHERE QUAN(1,1)=S/R,QUAN(2,1)=FMASS	Q	4
	5	SRG=VAR1	Q	5
	6	GMASS=VAR2	Q	6
	7	I=11	Q	7
	8	GO TO (2,19,34,40,73,75), I	Q	8
C	9	DETERMINE MAX MASS FOR INTERNAL FLOW OPTION	Q	9
1	10	J=J+1	Q	10
2	11	IF (GMASS) 3,4,4	Q	11
3	12	SRG=QUAN(1,1)	Q	12
	13	GO TO 72	Q	13
4	14	CONTINUE	Q	14
5	15	IF (QUAN(2,J)-GMASS) 5,5,17	Q	15
6	16	IF (J-NSRV) 1,6,6	Q	16
7	17	IF (QUAN(2,J)-GMASS) 7,8,7	Q	17
	18	CALL PAGE (1)	Q	18
8	19	WRITE (6,78) GMASS,QUAN(1,J),QUAN(2,J)	Q	19
	20	SRG=QUAN(1,J)	Q	20
	21	GO TO 72	Q	21
9	22	J=J-1	Q	22
	23	IF (QUAN(2,J)-GMASS) 10,8,17	Q	23
10	24	IF (J+2-NSRV) 11,11,13	Q	24
11	25	IF (QUAN(2,J+1)-QUAN(2,J+2)) 12,13,12	Q	25
12	26	CALL ENTRPG (QUAN(2,J),QUAN(2,J+1),QUAN(2,J+2),QUAN(1,J),QUAN(1,J+	Q	26
	27	11),QUAN(1,J+2),GMASS,SRG)	Q	27
	28	GO TO 72	Q	28
13	29	IF (J-1) 14,14,15	Q	29
C	30	INTERPOLATE BETWEEN TWO VALUES-BEFORE AND AFTER MASS	Q	30
14	31	SRG=(GMASS-QUAN(2,J))*(QUAN(1,J+1)-QUAN(1,J))/(QUAN(2,J+1)-QUAN(2,	Q	31
	32	1J))+QUAN(1,J)	Q	32
	33	GO TO 72	Q	33
15	34	IF (QUAN(2,J-1)-QUAN(2,J)) 16,14,16	Q	34
16	35	J=J-1	Q	35
	36	GO TO 12	Q	36
17	37	IF (J-1) 18,18,9	Q	37
18	38	CALL PAGE (1)	Q	38
	39	WRITE (6,79) GMASS,QUAN(1,J),QUAN(2,J)	Q	39
	40	GO TO 8	Q	40

C	19	DETERMINE GMASS CORRESPONDING W/CURRENT SRG	Q	41
	20	IF (QUAN(1,JJ)-SRG) 31,22,20	Q	42
	21	IF (JJ-1) 21,21,23	Q	43
	22	WRITE (6,85) SRG,QUAN(2,JJ),QUAN(1,JJ)	Q	44
		GMASS=QUAN(2,JJ)	Q	45
		GO TO 72	Q	46
	23	JJ=JJ-1	Q	47
		IF (QUAN(1,JJ)-SRG) 24,22,20	Q	48
	24	IF (JJ+2-NSRV) 25,25,27	Q	49
	25	IF (QUAN(2,JJ+1)-QUAN(2,JJ+2)) 26,27,26	Q	50
	26	CALL ENTRPG (QUAN(1,JJ),QUAN(1,JJ+1),QUAN(1,JJ+2),QUAN(2,JJ),QUAN(Q	51
		2,JJ+1),QUAN(2,JJ+2),SRG,GMASS)	Q	52
		GO TO 72	Q	53
	27	IF (JJ-1) 30,30,28	Q	54
	28	IF (QUAN(1,J)-QUAN(1,J-1)) 29,30,29	Q	55
	29	JJ=JJ-1	Q	56
		GO TO 26	Q	57
	30	GMASS=(SRG-QUAN(1,J))*(QUAN(2,J+1)-QUAN(2,J))/(QUAN(1,J+1)-QUAN(1,	Q	58
		J))+QUAN(2,J)	Q	59
		GO TO 72	Q	60
	31	IF (JJ-NSRV) 32,33,33	Q	61
	32	JJ=JJ+1	Q	62
		GO TO 19	Q	63
	33	CALL PAGE (1)	Q	64
		WRITE (6,86) SRG,QUAN(2,JJ),QUAN(1,JJ)	Q	65
		GMASS=QUAN(2,JJ)	Q	66
		GO TO 72	Q	67
C	34	READ IN ENTROPY W/CORRESPONDING R-REF VALUES	Q	68
		NSRV=IABS(I2)	Q	69
		JJ=1	Q	70
		J=1	Q	71
		QUAN(2,1)=0.0	Q	72
		QUAN(1,1)=0.0	Q	73
		INCASE=12	Q	74
		MI=VAR2+1.0	Q	75
		CON1=VAR1	Q	76
		IF (NSRV-1) 35,35,36	Q	77
	35	NSRV=0	Q	78
		I2=0	Q	79
		GO TO 72	Q	80

36	READ (3) (QUAN(2,K),QUAN(1,K),K=1,NSRV)	Q 81
	I2=NSRV	Q 82
	J=NSRV	Q 83
	DO 37 K=1,NSRV	Q 84
	IF (QUAN(1,1)) 38,37,37	Q 85
37	QUAN(2,K)=QUAN(2,K)*MI*CONI	Q 86
38	QUAN(1,1)=ABS(QUAN(1,1))	Q 87
	WRITE (6,81) NSRV	Q 88
C	SAVE CURRENT GMASS-S/R VALUES IN TABLE	Q 89
	NSRV=NSRV	Q 90
	DO 39 L=1,NSRV	Q 91
	SSRG(L)=QUAN(1,L)	Q 92
39	SGMASS(L)=QUAN(2,L)	Q 93
	GO TO 67	Q 94
C	ADD NEW VALUES OF S/R AND FMASS	Q 95
40	DO 49 K=1,NSRV	Q 96
41	IF (QUAN(2,K)-GMASS) 48,41,53	Q 97
	KK=K	Q 98
	L=K	Q 99
42	IF (QUAN(1,K)-SRG) 45,48,42	Q 100
	L=L-1	Q 101
	IF (L-1) 53,53,43	Q 102
43	IF (QUAN(2,L)-QUAN(2,L-1)) 42,44,42	Q 103
C	POINTS TO BE DROPPED RANGE FROM L TO K-1 INCL.	Q 104
44	QUAN(2,L)=GMASS	Q 105
	QUAN(1,L)=SRG	Q 106
	IK=L	Q 107
45	IF (NSRV-KK) 52,50,50	Q 108
	L=L-1	Q 109
	IF (L-1) 48,48,46	Q 110
46	IF (QUAN(2,L)-QUAN(2,L-1)) 45,47,45	Q 111
47	QUAN(1,L)=QUAN(1,K)	Q 112
	QUAN(2,L)=QUAN(2,K)	Q 113
	L=L+1	Q 114
	KK=K+1	Q 115
	GO TO 44	Q 116
48	IF (K-NSRV) 49,53,53	Q 117
49	CONTINUE	Q 118
	GO TO 56	Q 119
50	DO 51 LL=KK,NSRV	Q 120

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51  L=L+1
    QUAN(1,L)=QUAN(1,LL)
    QUAN(2,L)=QUAN(2,LL)
    NSRV=L
    GO TO 56
52  NSRV=L+1
    GO TO 56
53  JL=-1
    DO 54 KK=K,NSRV
    JKL=NSRV-JL
    QUAN(1,JKL)=QUAN(1,JKL-1)
    QUAN(2,JKL)=QUAN(2,JKL-1)
    JL=JKL+1
54  QUAN(1,K)=SRG
    QUAN(2,K)=GMASS
    IK=K
    NSRV=NSRV+1
    GO TO 56
55  NSRV=NSRV+1
    QUAN(1,NSRV)=SRG
    QUAN(2,NSRV)=GMASS
    IK=NSRV
56  IF (NSRV-99) 65,57,57
    C    REDUCE S/R TABLE BY 20
57  DO 64 K=1,20
    NSRVH=NSRV-1
    SMALL=1.0
    AX=QUAN(2,2)-QUAN(2,1)
    AY=QUAN(1,2)-QUAN(1,1)
    AY=QUAN(1,2)-QUAN(1,1)
    A=SQRT(AX**2+AY**2)
    AX=AX/A
    AY=AY/A
    DO 62 KK=2,NSRVH
    BX=QUAN(2,KK+1)-QUAN(2,KK)
    BY=QUAN(1,KK+1)-QUAN(1,KK)
    B=SQRT(BX**2+BY**2)
    BX=BX/B
    BY=BY/B
    IF (BX) 58,61,58
  
```

58	IF (AX) 59,61,59	Q 161
59	TMALL=ABS(AX*BY-AY*BX)	Q 162
	IF (SMALL-TMALL) 61,61,60	Q 163
60	SMALL=TMALL	Q 164
	KKK=KK	Q 165
61	AX=BX	Q 166
62	AY=BY	Q 167
	NSRV=NSRV-1	Q 168
	DO 63 KK=KKK,NSRVH	Q 169
	QUAN(1,KK)=QUAN(1,KK+1)	Q 170
63	QUAN(2,KK)=QUAN(2,KK+1)	Q 171
64	CONTINUE	Q 172
65	IF (INCASE) 66,72,72	Q 173
66	CALL PAGE (6+(NSRV+9)/10*3)	Q 174
	WRITE (6,80) IK	Q 175
67	IF (INCASE.GT.0) GO TO 72	Q 176
	WRITE (6,82)	Q 177
	DO 71 K=1,NSRV,10	Q 178
	IF (NSRV-K-10) 68,69,69	Q 179
68	L2=NSRV	Q 180
	GO TO 70	Q 181
69	L2=K+9	Q 182
70	WRITE (6,83) (QUAN(2,11),11=K,L2)	Q 183
	WRITE (6,84) (QUAN(1,11),11=K,L2)	Q 184
71	CONTINUE	Q 185
72	CONTINUE	Q 186
	VAR1=SRG	Q 187
	VAR2=GMASS	Q 188
	GO TO 77	Q 189
73	NSRV=NSRV	Q 190
C	STORE ALL S/R VALUES. CHARACT. LINE ACCEPTED	Q 191
	DO 74 K=1,NSRV	Q 192
	SGMASS(K)=QUAN(2,K)	Q 193
74	SSRG(K)=QUAN(1,K)	Q 194
	GO TO 72	Q 195
C	RESTORE ALL S/R VALUES	Q 196
75	NSRV=NSRV	Q 197
	DO 76 L=1,NSRV	Q 198
	QUAN(1,L)=SSRG(L)	Q 199
76	QUAN(2,L)=SGMASS(L)	Q 200

77	GO TO 72	Q 201
C	RETURN	Q 202
C		Q 203
78	FORMAT (38H AFTER LAST ENTRY IN S/R TABLE. GMASS=E13.6,22H,SR SET	Q 204
	1 TO LAST ENTRY,E13.6,22H,W/CORRESPONDING MASS E13.6)	Q 205
79	FORMAT (40H BEFORE FIRST ENTRY IN S/R TABLE. GMASS=E13.6,23H SR SE	Q 206
	1 T TO FIRST ENTRY,E13.6,22H,W/CORRESPONDING MASS E13.6)	Q 207
80	FORMAT (1M044X9ENTRY NO.14,6H ADDED)	Q 208
81	FORMAT (1M052X13,20H ENTROPY VALUES READ)	Q 209
82	FORMAT (7X1M112X1M212X1H312X1H412X1H512X1H612X1H712X1H812X1H911X2H	Q 210
	110/5X4HMASS9(9X4HMASS)/6X3HS/R9(10X3HS/R))	Q 211
83	FORMAT (1M0E12.6,9(E13.6))	Q 212
84	FORMAT (10E13.6)	Q 213
85	FORMAT (40H BEFORE FIRST ENTRY IN S/R TABLE. S/R=E13.6,26H GMASS	Q 214
	1 SET TO FIRST ENTRY,E13.6,15H,W/CORRES. S/R=E13.6)	Q 215
86	FORMAT (39H BEYOND LAST ENTRY IN S/R TABLE. S/R=E13.6,25H.GMASS	Q 216
	1 SET TO LAST ENTRY,E13.6,15H,W/CORRES. S/R=E13.6)	Q 217
	END	Q 218
		Q 219

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R R R R R R

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FUNCTION TSON (VM,G2,G3,G1)
  TSON=(G3*(VM**2)-(3.0-G1)+SQRT(G3*(G3*(VM**2)-2.0*(3.-G1))*(VM**2
  1)+G1+9.0)))/(4.0*G1*(VM**2))
  TSON=ATAN(SQRT(TSON)/SQRT(1.0-TSON))
  RETURN
END

```



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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
S S S S S S S S S S S S S S S S S S

FUNCTION DIF (XX,YY,M,N,L)
COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(
1100,2),GF(15),VMASS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(
23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HCL(72),XSPEC(3),XSTAR,DEM,PFS
3,VMSON,RAD,XLAST,AMUD,VMW,TSONIC,PO,TEST,R,DFP,BSCNIC,PH,FMO,THP,
4VFS,TYPE,TESU,BL,PSONIC,XSTARB,REF,RFIT,EL,TIN,DSONIC,RV2,CO,DET,
5OW,SW
COMMON /INTEG/ JI(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,
IKICK,MON,ILK,NS2,IO(100,2),INCASE,ISPEC
MML=M-L
TX=X(M-1,N)-X(M,N)
TY=Y(M-1,N)-Y(M,N)
IF (ABS(TX)+ABS(TY)) 1,1,2
DIF=10.0
GO TO 3
DIF=SQRT(((XX-X(MML,N))**2+(YY-Y(MML,N))**2)/(TX**2+TY**2))
RETURN
END

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3

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```

SUBROUTINE INPUT (LA,LB,LC)
COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(
1100,2),GF(15),VMASS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(
23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS
3,VMSON,RAD,XLAST,AMUD,VMW,ISONIC,PO,TEST,R,DFP,BSONIC,PW,FMD,THP,
4VFS,TYPE,TESU,BL,PSONIC,XSTARB,REF,RFIT,EL,TIN,DSONIC,RV2,CD,DET,
5DN,SN
COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,
1KICK,NOM,ILK,NS2,ID(100,2),INCASE,ISPEC
GO TO (1,2), LA
N=LB
GO TO 3
N=NOM
DO 6 I=LB,M
READ (3) X(I,LC),Y(I,LC),DF(I,LC),VM(I,LC),SR(I,LC)
P(I,LC)=(1.0+GF(4)*VM(I,LC)*2)**(-GF(10)))*SR(I,LC)
IF (DET) 4,5,4
X(I,LC)=(X(I,LC)-DET)*R/RFIT-HOL(41)
Y(I,LC)=Y(I,LC)*R/RFIT
IF( (MID.EQ.1) .OR. (HOL(37).EQ.0.0 ) ) GO TO 5
XP=X(I,LC)-R+HOL(41)
YP=Y(I,LC)
XPP=XP+HOL(32)-YP*HOL(33)
YPP=YP+HOL(32)+XP*HOL(33)
X(I,LC)=XPP+R-HOL(41)
Y(I,LC)=YPP
DF(I,LC)=DF(I,LC)/RAD
DF(I,LC)=DF(I,LC)+HOL(37)
CONTINUE
RETURN
END

```

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C


```

SUBROUTINE SHAPE
COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(
100,2),GF(15),VMASS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(
23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HQL(72),XSPEC(3),XSTAR,DEM,PFS
3,VMSON,RAD,XLAST,AMUD,VMH,ISONIC,PO,TEST,R,DFP,BSONIC,PM,FMO,TMP,
4VFS,TYPE,TESU,BL,PSONIC,XSTARB,REF,RFIT,EL,TIN,DSONIC,RV2,CD,DET,
5DM,SN
COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,
1KICK,MOM,ILK,NS2,ID(100,2),INCASE,ISPEC
COMMON /BETA/ D(102)
DIMENSION NUMBER(3)
EM=TAN(HOL(23))
EM2=EM*EM
BL=D(5)
R=1.0
XB(1)=(1.0-EM/SQRT(D(5)+EM2))/D(5)
YB(1)=SQRT(1.0-D(5)*XB(1))*XB(1)
SLOPE2(1)=ATAN(EM)*RAD
J1(1)=0
J1(2)=1
HOL(4)=HOL(3)
HOL(5)=HOL(3)
NSEG=2
NSEGM=NSEG
NSEG=NSEG+1
XF(1)=0.0
XB(2)=2.0
SLOPE1(2)=EM
SLOPE1(3)=EM
DO 5 I=2,NSEG
IF (1-NSEG) 2,1,1
J1(I)=1
XB(I)=1.1*XB(I-1)
GO TO 3
J=1+2
XF(I)=XB(I-1)
YF(I)=YB(I-1)
YB(I)=YF(I)+SLOPE1(I)*(XB(I)-XF(I))
SLOPE2(I)=SLOPE1(I)
AB(I)=0.0

```

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3

41	V	AC(I)=0.0
42	V	AD(I)=SLOPE1(I)
43	V	AE(I)=YF(I)
44	V	IF (I-NSEGM) 5,4,5
45	V	SLOPE1(NSEG)=SLOPE2(NSEG)
46	V	CONTINUE
47	V	DO 7 I=3,J
48	V	DX=XB(I-2)-XF(I-2)
49	V	NUMBER(I-2)=DX/(HOL(39)*HOL(I))
50	V	FIGURE=NUMBER(I-2)
51	V	IF (FIGURE) 7,7,6
52	V	HOL(I)=DX/(HOL(39)*FIGURE)
53	V	CONTINUE
54	V	HOL(J+1)=HOL(J)
55	V	WRITE (6,18)
56	V	DO 11 I=1,NSEGM
57	V	K=I+2
58	V	IF (I-1) 9,9,8
59	V	SLOPE1(I)=ATAN(SLOPE1(I))*RAD
60	V	SLOPE2(I)=SLOPE1(I)
61	V	GO TO 10
62	V	CALL PAGE (2)
63	V	WRITE (6,12)
64	V	WRITE (6,14) I,XB(I),YB(I),HOL(K)
65	V	WRITE (6,15) R,D(5)
66	V	GO TO 11
67	V	CALL PAGE (3)
68	V	WRITE (6,13)
69	V	WRITE (6,14) I,XB(I),YB(I),HOL(K)
70	V	WRITE (6,16) SLOPE1(I),SLOPE2(I)
71	V	WRITE (6,17) AB(I),AC(I),AD(I),AE(I)
72	V	CONTINUE
73	V	SLOPE1(NSEG)=ATAN(SLOPE1(NSEG))*RAD
74	V	SLOPE2(1)=0.0
75	V	RETURN
76	V	
77	V	
78	V	
79	V	
80	V	
		FORMAT (15H BLUNT SEGMENT)
		FORMAT (15H CUBIC SEGMENT)
		FORMAT (1H+,14X13,2X3HX2=E13.6,3X3HY2=E13.6,3X3HX*=E13.6)

V 81
V 82
V 83
V 84
V 85

FORMAT (1M 29X2MA=E13.6,3X2MB=E13.6)
FORMAT (1M 29X8MSLOPE 1=F10.5,4H DEG,3X8MSLOPE 2=F10.5,4H DEG)
FORMAT (1M 29X2MA=E13.6,5X2MB=E13.6,5X2MC=E13.6,5X2MD=E13.6)
FORMAT (1M)
END

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18

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40

```

SUBROUTINE DROP (I,J,K,L)
COMMON /FLDAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(
1100,2),GF(15),VMASS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(
23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS
3,VMSON,RAD,XLAST,AMUO,VMW,TSONIC,PQ,TEST,R,DFP,BSONIC,PW,FMO,IHP,
4VFS,TYPE,TESU,BL,PSONIC,XSTARB,REF,RFIT,EL,TIN,DSONIC,RV2,CD,DET,
5DW,SH
COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,
1KICK,NOW,ILK,NS2,ID(100,2),INCASE,ISPEC
IF (ITIN) 1,1,2
IF (I-1) 3,3,2
IF (L-1) 18,18,11
L=I
IZ=I
JZ=J
MZ=L
LZ=J-1
CMINUS=DF(IZ,JZ)-ANGLE(VM(IZ,JZ))-0.02
CPLUS=DF(MZ,LZ)+ANGLE(VM(MZ,LZ))+0.02
DELX=X(IZ,JZ)-X(MZ,LZ)
DELY=Y(IZ,JZ)-Y(MZ,LZ)
IF (DELX) 6,5,6
GEO=-HOL(63)
GO TO 8
GEO=ATAN(DELY/DELX)
IF (DELX) 8,8,7
GEO=GEO-HOL(62)
IF ((CMINUS-GEO) 11,11,9
GEP=GEO+HOL(62)
IF (GEP-CPLUS) 11,11,10
K=1
GO TO 18
NSKIP=NSKIP+1
K=2
IF (ITIN-1.0) 12,12,13
HOLD ALL ELEMENTS FROM FIRST DIM. BEGINING W/ELEMENT TWO
CALL CHANGE (1,1)
STEP DOWN ALL ELEMENTS FROM DIM. ONE BEGINING W/ELEMENT TWO
CALL CHANGE (6,2)
IF (ITIN) 15,15,14

```

1 2 3 4

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C

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C

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14 IMOP=HOL(45)
15 TIN=1+(1+IMOP)/2-HOL(46)
16 NOW=NOW-1
17 IF (NOW-1) 17,17,16
18 IF (TIN.LE.0.) GO TO 4
19 L=L-1
20 GO TO 2
21 KICK=1
22 IF (INCASE-4) 20,19,19
23 WRITE (6,21) I,J,K,TIN,NOW,NSKIP,GEO,CHINUS,CPLUS
24 RETURN
25
26 FORMAT (14H DROP PROG. I=I3,3H J=J3,3H K=K3,5H TIN=E13.6,5H NOW=I3
27 1,7H NSKIP=I3/5H GEO=E13.6,5H CHI=E13.6,5H CPL=E13.6)
28 END

```


X	42
X	43
X	44
X	45
X	46
X	47
X	48
X	49
X	50
X	51
X	52
X	53
X	54
X	55
X	56
X	57
X	58
X	59
X	60
X	61
X	62
X	63
X	64
X	65
X	66
X	67
X	68
X	69
X	70
X	71
X	72
X	73
X	74
X	75
X	76
X	77
X	78
X	79
X	80
X	81

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13 CALL PAGE (6)
14 WRITE (6,35) NSUM,THP,TYPE
14 DO 17 I=LB,NOW
14 DFP=DF(I,LC)*RAD
14 PR=(P(I,LC)-PFS)/RV2
14 IF (LA-6) 15,18,19
15 CALL PAGE (1)
15 WRITE (6,29) I,X(I,LC),Y(I,LC),DFP,VM(I,LC),PR,SR(I,LC)
15 IF (ID(I,LC)) 16,17,18
16 WRITE (6,36) ID(I,LC)
17 CONTINUE
17 CALL PAGE (3)
17 WRITE (6,32) CD
17 WRITE (6,26) HOL(57)
17 NSUM=NSUM+1
17 GO TO 25
18 IF (INCASE.LT.4) GO TO 25
18 CALL PAGE (4)
18 WRITE (6,33) X(I,LC),Y(I,LC),DFP,VM(I,LC),TYPE,PR,SR(I,LC)
18 GO TO 25
19 CONTINUE
19 CALL PAGE (1)
19 WRITE (6,34) X(I,LC),Y(I,LC),DFP,VM(I,LC),TYPE,PR,SR(I,LC)
19 IF (LC-1) 25,29,20
20 CALL PAGE (1)
20 WRITE (6,27) HOL(57)
20 GO TO 25
21 CALL PAGE (4)
21 WRITE (6,30) NSUM,TYPE
21 GO TO 14
22 CONTINUE
22 DO 23 I=1,NOW
22 DF3(I)=DF(I,LC)*RAD
23 CONTINUE
23 WRITE (4) NSUM,NOW
23 DO 24 J=1,NOW
24 WRITE (4) X(J,LC),Y(J,LC),DF3(J),VM(J,LC),SR(J,LC)
25 IF (INCASE.LT.2.AND.(LB.EQ.NOW.AND.LA.EQ.7)) NSUM=NSUM+1
25 RETURN
C

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26	FORMAT (1H+,60X20H(DELTA M)/(M TOTAL)=E15.6/1H 119(1H-))	X	82
27	FORMAT (5X,20H(DELTA M)/(M TOTAL)=E15.6)	X	83
28	FORMAT (36H0----FREE STREAM AND CONSTANT VALUES84(1H-)/12H0 (P/PT)	X	84
	11NF=E15.6/12H MACH NO =OPF9.5/5X7HGAMMA =F9.5/5X7HR-REF =E15.6/	X	85
	21X,119(1H-))	X	86
29	FORMAT (2X,13,2G15.6,2G12.5,3G14.6)	X	87
30	FORMAT (18H0----C-SUMMARY NO.13,99(1H-)/6H0POINT7X1MX14X1HY11X5HDE	X	88
	11TA,7X,4HMACH,7X,A6,9X,6HPT/PT0,/)	X	89
31	FORMAT (26H0----INITIAL VALUE LINE DATA92(1H-)/14X12HTHETA SHOCK=	X	90
	1E13.6/6H0POINT7X1MX14X1HY11X5HDELTA7X4HMACH7XA6,9X6HPT/PT0/)	X	91
32	FORMAT (26H0 DRAG COEF.=E13.6)	X	92
33	FORMAT (28H0----INITIAL VALUE LINE DATA92(1H-)/5X2HX=E13.6,4H Y=	X	93
	1E13.6,8H DELTA=OPF10.5,7H MACH=F10.5,2X,A6,1H=E13.6,9H PT/PT0=	X	94
	2E13.6/1X,119(1H-))	X	95
34	FORMAT (5X2HX=E13.6,2X2HY=E13.6,2X6HDELTA=OPF10.5,2X5HMACH=OPF10.5	X	96
	1,2XA6,1H=E13.6,9H PT/PT0=E13.6)	X	97
35	FORMAT (18H0----C-SUMMARY NO.13,99(1H-)/14X12HTHETA SHOCK=E13.6/6H	X	98
	10POINT,7X,1MX,14X,1HY,11X,5HDELTA,7X,4HMACH,7X,A6,9X,6HPT/PT0,/)	X	99
36	FORMAT (1H+101X12)	X	100
	END	X	101

[illegible]

10	VMN2=VMN*2	41
	PR=((GF(9)*VMN2-GF(2))/GF(3))	42
	PH=P1*PR	43
	DW=ATAN((2.0*(VMN2-1.0)/TAN(THDTA)))/(2.0+GF(3)*QM2-2.0*VMN2))+	44
	1 DEL TO	45
	SW=S1*((GF(3)*VMN2/(GF(2)*VMN2+2.0))*GF(10))*((-GF(11)))	46
	VMN=(GF(8)*VMN2*(QM2)-4.0*(VMN2-1.0)*(GF(1)*VMN2+1.0))/(2.0*GF(1)	47
	1*VMN2-GF(2))*GF(2)*VMN2+2.0))	48
	VMN=SQRT(VMN)	49
	IF (INCASE-4) 12,11,11	50
	WRITE (6,14) PH,DW,SW,VMN	51
	RETURN	52
11		53
12		54
C		55
C		56
13	FORMAT (5X42H FAILED TO CONVERGE SHOCK ANGLE IN 50 TRIES)	57
14	FORMAT (10X3HPH=E15.6,5X3HDW=E15.6,5X3HSW=E15.6,5X4HVMN=E15.6)	58
15	FORMAT (9H IN WAVE/5X6HDELTA=E15.6,5X6HDELTO=E15.6,5X4HLM=15)	
	END	

```

1  SUBROUTINE SMOCK (IRS,JRS)
2  COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(
3  100,2),GF(15),VMAS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XB(3),YB(
4  23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS
5  3,VMSON,RAD,XLAST,AMUO,VMW,TSOIN,PO,TEST,R,DFP,BSONIC,PW,FMO,THP,
6  4VFS,TYPE,TESU,BL,PSONIC,XSTAR,REF,RFIT,EL,TIN,DSOIN,RV2,CD,DET,
7  SON,SW
8  COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,I,PUNCH,NSUM,IT,ISEG,LOOP,MID,
9  IKICK,MOM,ILK,NS2,ID(100,2),INCASE,ISPEC
10 DIMENSION RESID(2),TH(2),TAN2S(99)
11 IDROP=0
12 G1=GF(1)
13 I=IRS
14 J=JRS
15 JP1=J+1
16 NS=10(1,J)
17 TWO=2.0
18 NHOL=-1
19 IT=NOW-1
20 DO 1 K=1,IT
21 TAN2S(K)=0.0
22 IF (ABS(Y(K,J)-Y(K+1,J))+ABS(X(K,J)-X(K+1,J)).NE.0.0) TAN2S(K)=(Y(
23 K,J)-Y(K+1,J))/(X(K,J)-X(K+1,J))
24 IF (INCASE=4) 3,2,2
25 WRITE (6,84) ((K,TAN2S(K)),K=1,NOW)
26 IT=0
27 IT1=0
28 IWAY=1
29 ISS=0
30 D2=DF(1,J)
31 AMU2=ANGLE(VM(I,J))
32 THO=THS(1,1)
33 IF (INCASE=4) 4,5,5
34 IP=1
35 GO TO 6
36 IP=2
37 N=1
38 IHOW=HOL(46)
39 NHOL=1+IHOW-1
40 DO=HOL(37)

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7	SO=1.0	41
	IF (HOL(46)) 0,0,7	42
	XU=X(I,J)	43
	YU=Y(I,J)	44
	X4=X(I+1,J)	45
	Y4=Y(I+1,J)	46
	D4=DF(I+1,J)	47
	P4=P(I+1,J)	48
	VM4=VM(I+1,J)	49
	AMU4=ANGLE(VM4)	50
	TAN3=TAN(D4+HOL(45)*AMU4)	51
	IDROP=I+1	52
	GO TO 19	53
8	IF (INCASE-4) 10,9,9	54
9	WRITE (6,73) HOL(53),HOL(54),HOL(69),XSTAR,XSTAR8	55
10	IF (HOL(54)-1.0) 13,11,13	56
11	XSTAR=HOL(53)*0.5	57
12	IF (INCASE-4) 13,12,12	58
13	WRITE (6,86) XSTAR	59
	SM=XSTAR	60
	IF (INCASE-4) 15,14,14	61
14	WRITE (6,87) XSTAR	62
15	IF (SM) 16,16,18	63
16	WRITE (6,72) SM,XSTAR,AMU2,D2,THS(NS,J),NS,J	64
17	KICK=KICK+1	65
	GO TO 69	66
18	SAVS=SIN(THS(NS,J))	67
	SAVC=COS(THS(NS,J))	68
	XU=SM*(SAVC-SAVS)+X(I,J)	69
	YU=SM*(SAVC+SAVS)+Y(I,J)	70
	TANC=-SAVC/SAVS	71
19	THS3=TSONIC	72
	D3=DSOINIC	73
	P3=PSOINIC	74
	VM3=VHSON	75
	AMU3=BSOINIC	76
20	GO TO (21,20), IP	77
21	WRITE (6,78) NS,J,THS(NS,J),XU,YU,D3,P3,THS3,AMU3	78
	TANAV=TAN((THO+THS3)*0.5)	79
	IF (NHOL) 23,22,23	80

22	X3=(YU-Y4-XU*TANAV+X4*TAN3)/(TAN3-TANAV)	Z 81
	Y3=((X4-XU)*(TAN3*TANAV)-Y4*TANAV+YU*TAN3)/(TAN3-TANAV)	Z 82
	GO TO 24	Z 83
23	X3=(YU-Y(I,J))-XU*TANC+X(I,J)*TANAV/(TANAV-TANC)	Z 84
	Y3=YU+TANC*(X3-XU)	Z 85
24	FMO=VFS	Z 86
	PD=(1.0+GF(4)*(FMO**2))*(-GF(10))	Z 87
	THSAVE=ANGLE(FMO)	Z 88
	GO TO (26,25), IP	Z 89
25	WRITE (6,79) X3,Y3,TANAV	Z 90
26	TAN2=TAN2S(I)	Z 91
	IF (NHOL) 27,28,27	Z 92
27	TAN3=TAN(.5*(D3+D2+(AMU3+AMU2)*HOL(45)))	Z 93
28	IF (NHOL) 29,54,29	Z 94
29	L=1	Z 95
	TAN2=TAN2S(L)	Z 96
30	X4=(Y(L,J))-Y3+X3*TAN3-X(L,J)*TAN2/(TAN3-TAN2)	Z 97
	Y4=Y(L,J)+TAN2*(X4-X(L,J))	Z 98
	IDROP=L	Z 99
	GO TO (32,31), IP	Z 100
31	WRITE (6,80) X4,Y4,ITL,X(L,J),Y(L,J),TAN2,TAN3,L,J	Z 101
32	IGATE=0	Z 102
	NGATE=0	Z 103
	DEL3=DIF(X4,Y4,L+1,J,1)	Z 104
	IF (DEL3-1.0) 38,38,33	Z 105
33	L=L+1	Z 106
	IF (L-NOW) 35,34,34	Z 107
34	XSTAR=XSTAR+0.5	Z 108
	ISS=ISS+1	Z 109
35	IF (ISS-3) 18,18,17	Z 110
	IGATE=1	Z 111
	IF (NGATE) 37,37,36	Z 112
36	WRITE (6,74)	Z 113
	GO TO 17	Z 114
37	TAN2=TAN2S(L)	Z 115
	GO TO 30	Z 116
38	DEL1=DIF(X4,Y4,L+1,J,0)	Z 117
	IF (DEL1-1.0) 40,40,39	Z 118
39	WRITE (6,75)	Z 119
	GO TO 17	Z 120

40	K=J	Z 121
	LL=L+1	Z 122
	IF (DEL3-1.0) 42,42,41	Z 123
41	L=L+1	Z 124
	TAN2=TAN2S(L-1)	Z 125
	WRITE (6,85) DEL3	Z 126
	GO TO 17	Z 127
42	D4=DF(L,J)+DEL3*(DF(LL,K)-DF(L,J))	Z 128
	P4=P(L,J)+DEL3*(P(LL,K)-P(L,J))	Z 129
	VM4=VM(L,J)+DEL3*(VM(LL,K)-VM(L,J))	Z 130
	AMU4=ANGLE(VM4)	Z 131
	TAN3=TAN((D4+D3)+(AMU4+AMU3)*HOL(45))*0.5)	Z 132
	GO TO (44,43), IP	Z 133
43	WRITE (6,81) D4,P4,VM4,AMU4,TAN3,IT	Z 134
44	IF (IT1) 45,45,47	Z 135
45	IT1=1	Z 136
46	X4A=X4	Z 137
	Y4A=Y4	Z 138
	D4A=D4	Z 139
	P4A=P4	Z 140
	VM4A=VM4	Z 141
	GO TO 28	Z 142
47	IT1=IT1+1	Z 143
	IF (IT1-50) 49,49,48	Z 144
48	WRITE (6,76) X3,Y3,NSUM	Z 145
	X4=0.5*(X4+X4A)	Z 146
	Y4=0.5*(Y4+Y4A)	Z 147
	D4=0.5*(D4+D4A)	Z 148
	P4=0.5*(P4+P4A)	Z 149
	VM4=0.5*(VM4+VM4A)	Z 150
	GO TO 54	Z 151
49	IF (ABS(X4A/X4-1.0)-TEST) 50,50,46	Z 152
50	IF (ABS(Y4A/Y4-1.0)-TEST) 51,51,46	Z 153
51	IF (ABS(D4A/D4-1.0)-TEST) 52,52,46	Z 154
52	IF (ABS(P4A/P4-1.0)-TEST) 53,53,46	Z 155
53	IF (ABS(VM4A/VM4-1.0)-TEST) 54,54,46	Z 156
54	AMAV=(AMU3+AMU4)*0.5	Z 157
	DAV=(D3+D4)*0.5	Z 158
	C1=HOL(45)*(D3-D4)+DEM*(SIN(DAV)*SIN(AMAV)*SQRT((X3-X4)**2+(Y3-Y4)**2)/(-.5*(Y3+Y4)))	Z 159
		Z 160

55	C2=G1/SIN(2.0*AMAV)	Z 161
56	RT=2.0*C1*C2	Z 162
57	RESID(IWAY)=ALOG(P3/P4)+RT	Z 163
	TH(IWAY)=THS3	Z 164
	IT1=0	Z 165
	GO TO (56,55), IP	Z 166
	WRITE (6,82) AMAV,DAV,C1,C2,RESID(IWAY),TH(IWAY),IWAY	Z 167
	GO TO (57,58), IWAY	Z 168
	IT=1	Z 169
	IWAY=2	Z 170
	THS3=THS(NS,J)	Z 171
	D3=DF(1,J)	Z 172
	P3=P(1,J)	Z 173
	AMU3=AMU2	Z 174
	VM3=VM(1,J)	Z 175
	S3=SR(1,J)	Z 176
	GO TO 21	Z 177
58	SHINC=TH(1)-TH(2)	Z 178
	CORR=RESID(1)*(SHINC/(RESID(2)-RESID(1)))	Z 179
	RATIO=CORR/SHINC	Z 180
59	IF (ABS(RATIO)-2.0) 60,60,59	Z 181
60	CORR=SHINC*SIGN(TWO,RATIO)	Z 182
	THS3=TH(1)+CORR	Z 183
	IF ((THS3-THSAVE)*HOL(45)) 61,61,62	Z 184
61	THS3=THSAVE	Z 185
62	GO TO (64,63), IP	Z 186
63	WRITE (6,83) TH(1),RESID(1),TH(2),RESID(2),THS3,IT	Z 187
64	TH(1)=TH(2)	Z 188
	RESID(1)=RESID(2)	Z 189
	IT=IT+1	Z 190
65	IF (IT-75) 67,67,65	Z 191
	WRITE (6,77)	Z 192
	GO TO 17	Z 193
66	CALL WAVE (THS3,DO,FMO,PO,SO,1)	Z 194
	D3=DN	Z 195
	P3=PN	Z 196
	VM3=VMH	Z 197
	AMU3=ANGLE(VM3)	Z 198
	IF (HOL(46).GT.0.0) TAN3=TAN(0.5*(D3+D4+(AMU3+AMU4)*HOL(45)))	Z 199
	S3=SN	Z 200

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67      GO TO 21
68      IF (ABS(RESID(2))-TESU) 68,66,66
      HOL(60)=N
      K=N
      X(K,JP1)=X3
      Y(K,JP1)=Y3
      IHOG=HOL(45)
      ID(K,JP1)=NS2+(1+IHOG)/2
      DF(K,JP1)=03
      P(K,JP1)=P3
      VM(K,JP1)=VM3
      SR(K,JP1)=S3
      THS(NS2+1,JP1)=THS3
      DELY=Y3*COS(HOL(37))-(X3-R)*SIN(HOL(37))
      VMAS(1)=(DELY*(MID+1))/HOL(58)
      INSERT TEMPORARY SR VALUE INTO TABLE FROM BOW WAVE
      CALL ENTROP (SR(1,2),VMAS(1),4,0)
      ICALL=1
      IF (HOL(61)) 70,70,71
      CALL DROP (ICALL,J,IDMY,IDROP)
      RETURN
C
69
70
71
C
C
C
72      FORMAT (5X32HSM IS ZERO OR NEGATIVE IN RSHOCK/10X3HSM=E15.6/15X6MX
1STAR=E15.6/20X3HAMU2=E15.6/25X3MD2=E15.6/30X9HTH(NS,J)=E15.6/35X3M
2NS=15/40X2MJ=15)
73      FORMAT (5X8MHOL(53)=E15.6/5X8MHOL(54)=E15.6/5X8MHOL(69)=E15.6/7X6M
1XSTAR=E15.6/6X7MXSTAR8=E15.6//)
74      FORMAT (5X3SHOSCILLATED THROUGH NGATE THEN IGATE)
75      FORMAT (5X3SHOSCILLATED THROUGH IGATE THEN NGATE)
76      FORMAT (5X34HEXCEEDED 50 ITERATIONS FOR POINT 4,5X3MX3=E15.7,5X3MY
13=E15.7,5X3HC=14)
77      FORMAT (5X32HEXCEEDED 75 ITERATIONS FOR SHOCK)
78      FORMAT (10X7MNO. 202/11X3HNS=15,5X2HJ=15/15X10HTHS(NS,J)=E15.6/
120X3HXU=E15.6/25X3MYU=E15.6/30X3MD3=E15.6/40X5HTMS3=
2E15.6/45X3HAMU3=E15.6)
79      FORMAT (20X3M206/15X3MX3=E15.6/20X3HY3=E15.6/25X6HTANAV=E15.6)
80      FORMAT (5X3MX4=E15.8,5X3MY4=E15.8,5X4HTI1=15/10X7HX(L,J)=E15.8,5X7
1HY(L,J)=E15.8,5X5HTAN2=E15.8,5X5HTAN3=E15.8/10X,2HL=15,5X2HJ=15)
Z 201
Z 202
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81	FORMAT (10X3H213/15X3HD4=E15.6/20X3HP4=E15.6/25X4HVM4=E15.6/35X\$HA	Z 241
	1MU4=E15.6/40X5MTAN3=E15.6/45X3HIT=I5)	Z 242
82	FORMAT (10X3H213/15X\$HAMAV=E15.6/20X4HDAV=E15.6/25X3MCI=E15.6/30X3	Z 243
	1HC2=E15.6/35X12HRESID(IWAY)=E15.6/40X9HTH(IWAY)=E15.6/45X5HIWAY=I5	Z 244
	2)	Z 245
83	FORMAT (10X3H217/10X6HTH(1)=E15.6,5X9HRESID(1)=E15.6/15X6HTH(2)=	Z 246
	1E15.6,5X9HRESID(2)=E15.6/20X5HTHS3=E15.6,10X3HIT=I5)	Z 247
84	FORMAT (10X1HK,7X8HTAN2S(K)/(11,E15.6))	Z 248
85	FORMAT (5X16H\$FAILED AT 68,DEL3=E15.6)	Z 249
86	FORMAT (5X16H\$AFTER 244,XSTAR=E15.6)	Z 250
87	FORMAT (5X16H\$AFTER 243,XSTAR=E15.6)	Z 251
	END	Z 252

	1	AA
	2	AA
	3	AA
	4	AA
	5	AA
	6	AA
	7	AA
	8	AA
	9	AA
	10	AA
	11	AA
	12	AA
	13	AA
	14	AA
	15	AA
	16	AA
	17	AA
	18	AA
	19	AA
	20	AA
	21	AA
	22	AA
	23	AA
	24	AA
	25	AA
	26	AA
	27	AA
	28	AA
	29	AA
	30	AA
	31	AA
	32	AA
	33	AA
	34	AA
	35	AA
	36	AA
	37	AA
	38	AA
	39	AA
	40	AA

```

SUBROUTINE MESH (IGO)
COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(
1100,2),GF(15),VMAS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),XR(3),YB(
23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS
3,VMSON,RAD,XLAST,AMUD,VMW,TSONIC,PO,TEST,R,DFP,BSONIC,PM,FMO,THP,
4VFS,TYPE,TESU,BL,PSONIC,XSTARB,REF,RFIT,EL,TIN,DSONIC,RV2,CD,DET,
5DW,SW
COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,
1KICK,NOW,ILK,NS2,ID(100,2),INCASE,ISPEC
IT=0
IGOG=0
IF (INCASE=4) 2,1,1
WRITE (6,43)
1  WRITE (6,44) XSTAR,XSTARB,XLAST,XSPEC(ILK),XSAVE,DX1,XINTP,DXSTAR,
    2  IMOL(48),HOL(54),MOL(69),XS2,DXRATO,IXS,IGO,LOOP,ISPEC,ILK
    2  DXSTAR=X(NOW,2)-XLAST
    3  IF (MOL(69)) 3,3,24
    4  IF (LOOP) 4,4,5
    4  IXS=0
    4  XS2=XSTAR
    4  DX2=X(NOW,2)
    5  IF (DXSTAR) 6,6,8
    6  WRITE (6,40) DXSTAR
    7  IGO=2
    7  GO TO 30
    8  LOOP=LOOP+1
    9  IF (LOOP=25) 10,10,9
    9  WRITE (6,41) XSTAR,XSAVE,DXRATO,DX1,XSTARB
    10 GO TO 7
    10 IF (ISPEC) 15,15,11
    11 DXRATO=DXSTAR/DX1
    12 IF (ABS(DXRATO-1.)-.0005) 23,12,12
    13 IF (IXS=2) 13,20,20
    13 IXS=IXS+1
    13 XS2=XSTAR
    13 DX2=X(NOW,2)
    14 XSTAR=XSTAR/DXRATO
    14 NOW=NOW-1
    14 IGO=1
    14 GO TO 30

```

15	IF (DXSTAR-XSTAR) 16,16,17	41	AA
16	DXRATO=DXSTAR/XSTAR	42	AA
17	IF (DXRATO-HOL(38)) 17,24,24	43	AA
18	IF (IXS) 18,18,19	44	AA
	IXS=1	45	AA
	XSTAR=0.9*XSTAR*XSTARB/DXSTAR	46	AA
	GO TO 14	47	AA
19	XINTP=XLAST+HOL(39)*XSTARB	48	AA
20	DX3=X(NOW,2)	49	AA
	XST=XS2+(XSTAR-XS2)*(XINTP-DX2)/(X(NOW,2)-DX2)	50	AA
21	IF (XST) 22,22,21	51	AA
	XSTAR=XST	52	AA
	GO TO 14	53	AA
22	XSTAR=0.5*XS2	54	AA
	WRITE (6,42) XSTAR,XS2	55	AA
	DX2=DX3	56	AA
	GO TO 14	57	AA
23	ISPEC=0	58	AA
	XSTARB=HOL(ILK+3)	59	AA
	IGOGO=1	60	AA
	XSPEC(ILK)=0.0	61	AA
	HOL(40)=ILK	62	AA
	XSTAR=XSAVE	63	AA
	IT=1	64	AA
24	DO 25 ILK=1,MSEG	65	AA
	IF (XSPEC(ILK)) 25,25,33	66	AA
25	CONTINUE	67	AA
26	IF (HOL(54)) 27,27,28	68	AA
27	XSTAR=HOL(39)*XSTAR/DXRATO	69	AA
28	ILK=HOL(40)	70	AA
	HOL(40)=0.0	71	AA
	IGO=3+IGOGO	72	AA
29	XLAST=X(NOW,2)	73	AA
30	IF (INCASE=4) 32,31,31	74	AA
31	WRITE (6,44) XSTAR,XSTARB,XLAST,XSPEC(ILK),XSAVE,DX1,XINTP,DXSTAR,	75	AA
	1HOL(48),HOL(54),HOL(69),XS2,DXRATO,IXS,IGO,LOOP,ISPEC,ILK	76	AA
32	RETURN	77	AA
33	XXM=XSPEC(ILK)-X(NOW,2)	78	AA
	IF (XXM) 34,34,35	79	AA
34	LGO=1	80	AA

35	XPAST=MLAST	AA 81
	GO TO 37	AA 82
	CONTINUE	AA 83
	IF (XMX-XSTAR*1.2) 36,36,26	AA 84
36	LGO=2	AA 85
	XPAST=X(NOW,2)	AA 86
37	ISPEC=1	AA 87
	HOL(69)=0.0	AA 88
	ILK=ILK	AA 89
	XSAVE=XSTAR	AA 90
	DX1=XSPEC(ILK)-XPAST	AA 91
	XSTAR=DX1+XSTAR/DXSTAR	AA 92
	XINTP=XSPEC(ILK)	AA 93
	GO TO (14,38), LGO	AA 94
38	IGO=3+IGOGO	AA 95
	IF (HOL(40)) 29,29,39	AA 96
39	ISV=ILK	AA 97
	ILK=HOL(40)	AA 98
	HOL(40)=ISV	AA 99
	GO TO 29	AA 100
C		AA 101
C		AA 102
C		AA 103
40	FORMAT (14H0NEG. BODY INCREMENT--PROGRAM STOPPED--INC.=E13.6)	AA 104
41	FORMAT (40HOCANNOT CONVERGE TO SPECIAL BODY POINT /5X6HXSTAR= 1E13.6/10X6HXSARE=E13.6/15X8HDXRATIO=E13.6/20X4HDX1=E13.6/25X7HXSTA 2RB=E13.6)	AA 105 AA 106 AA 107
42	FORMAT (1X6HXSTAR=E13.7,5X4HXS2=E13.7)	AA 108
43	FORMAT (1X10IH.),21MINITIAL VALUE IN MESH)	AA 109
44	FORMAT (7E18.6/6E18.6/6I18)	AA 110
	END	AA 111

1	AB	SUBROUTINE PAGE (LINE)	1
2	AB	COMMON /FLOAT/ X(100,2),Y(100,2),P(100,2),DF(100,2),VM(100,2),SR(2
3	AB	1100,2),GF(15),VMAS(100),SLOPE1(3),SLOPE2(3),XF(3),YF(3),X8(3),Y8(3
4	AB	23),AB(3),AC(3),AD(3),AE(3),THS(2,2),HOL(72),XSPEC(3),XSTAR,DEM,PFS	4
5	AB	3,VMSON,RAD,XLAST,AMUD,VMW,TSONIC,PO,TEST,R,DFP,BSONIC,PM,FMO,THP,	5
6	AB	4VFS,TYPE,TESU,BL,PSONIC,XSTAR8,REF,RFIT,EL,TIN,DSOIC,RV2,CD,DET,	6
7	AB	SDW,SH	7
8	AB	COMMON /INTEG/ J1(3),NSEG,KPR,NSKIP,IPUNCH,NSUM,IT,ISEG,LOOP,MID,	8
9	AB	1KICK,NOW,ILK,NS2,ID(100,2),INCASE,ISPEC	9
10	AB	IF (LINE) 1,1,2	10
11	AB	IPAGE=0	11
12	AB	LPP=52	12
13	AB	NLINE=0	13
14	AB	GO TO 5	14
15	AB	IF (INCASE-2) 3,3,8	15
16	AB	IF (NLINE+LINE-LPP) 4,4,5	16
17	AB	NLINE=NLINE+LINE	17
18	AB	GO TO 8	18
19	AB	RESTORE CARRIAGE AND PRINT PAGE HEADING	19
20	AB	IPAGE=IPAGE+1	20
21	AB	WRITE (6,9) IPAGE	21
22	AB	IF (LINE-LPP) 7,6,6	22
23	AB	NLINE=LINE-LPP+3	23
24	AB	GO TO 8	24
25	AB	NLINE=LINE+3	25
26	AB	RETURN	26
27	AB		27
28	AB	FORMAT (1H1,11X,4HPAGE,14)	28
29	AB	END	29

1 2 3 4 5
AC AC AC AC AC

FUNCTION ANGLE (X)
ANGLE=ASIN(1.0/X)
RETURN
END

C

1
2
3
4
5
AD
AD
AD
AD
AD

FUNCTION VELOC (VM,G4)
VELOC=G4*(VM**2)
VELOC=SQRT(VELOC/(1.0+VELOC))
RETURN
END

OVERLAY (BLUNT,4,0)	AE	2
PROGRAM IVSES	AE	3
COMMON /BETA/ D(7),XM,GAMA,ALFA,RAMDA,RINGS,E(89),MERID,BDRAG	AE	4
COMMON /TRANS/ LO,LI,LL,MS	AE	5
DIMENSION X(42,44),Y(42,44),DF(42,44),VM(42,44),SR(42,44),NO(40),	AE	6
IPSI(19),YH(40),DFH(40),VMH(40),SRH(40),RP(19,20),TH(19,20),PT(19,	AE	7
2 20),XH(19,20),VV(19,20)		
REWIND 4	AE	9
RAD=57.295779513	AE	10
NRING=RINGS	AE	11
SINA=SIN(ALFA)	AE	12
COSA=COS(ALFA)	AE	13
TANA=SINA/COSA	AE	14
ALDEG=ALFA*RAD	AE	15
RADEG=RAMDA*RAD	AE	16
XI=1.-SIN(RAMDA)	AE	17
WRITE (6,11) ALDEG,RADEG,XI	AE	18
M=(LL-LO)/40+1	AE	19
M=LL/40+1	AE	20
M2=(LL-LO+1)/M+2	AE	21
MX=0	AE	22
LX=0	AE	23
KX=1	AE	24
DO 4 J=1,LL	AE	25
K=J-LO+2	AE	26
JX=0	AE	27
READ (4) NSUM,NOW	AE	28
DO 3 I=1,NOW	AE	29
READ (4) A1,A2,A3,A4,A5	AE	30
L=J-MS	AE	31
IF (I.GT.1.OR.(L/M)*M.NE.L.OR.(L.LT.1)) GO TO 1	AE	32
MX=MX+1	AE	33
X(MX,M2)=A1	AE	34
Y(MX,M2)=A2	AE	35
DF(MX,M2)=A3	AE	36
VM(MX,M2)=A4	AE	37
SR(MX,M2)=A5	AE	38
IF (I.NE.NOW.OR.-J.GT.L1) GO TO 2	AE	39
LX=LX+1	AE	40
X(LX,1)=A1	AE	41

1

AE 42
AE 43
AE 44
AE 45
AE 46
AE 47
AE 48
AE 49
AE 50
AE 51
AE 52
AE 53
AE 54
AE 55
AE 56
AE 57
AE 58
AE 59
AE 60
AE 61
AE 62
AE 63
AE 64
AE 65
AE 66
AE 67
AE 68
AE 69
AE 70
AE 71
AE 72
AE 73
AE 74
AE 75
AE 76
AE 77
AE 78
AE 79
AE 80
AE 81

```

YILX,1)=A2
DFILX,1)=A3
VM(LX,1)=A4
SR(LX,1)=A5
2  IF (K.LT.2.OR.(K/N)*N.NE.K) GO TO 3
    IF (JX.EQ.0) KX=KX+1
    IF (JX.EQ.0) JX=1
    X(I,KX)=A1
    Y(I,KX)=A2
    DF(I,KX)=A3
    VM(I,KX)=A4
    SR(I,KX)=A5
    NO(KX)=NOW
3  CONTINUE
4  CONTINUE
    NO(1)=LX
    NO(M2)=MX
    MERIDS=MERID*2-1
    FLOATM=MERIDS-1
    DA=180./FLOATM
    COSO=1.
    SINO=0.
    DO 9 I=1,MERIDS
    XI=I-1
    PSI(I)=DA*X1-90.
    COSI=1./SQRT(1.+(SIN(PSI(I)/RAD)*TANA)**2)
    SINI=-SIN(PSI(I)/RAD)*TANA*COSI
    ANG=ASIN(SINI)*RAD
    SIN2=SINI*COSO-COSI*SINO
    COS2=COSI*COSO+SINI*SINO
    M=0
    DO 7 J=1,M2
    NOW=NO(J)
    IF (NOW.LT.3.AND.(J.NE.1.OR.J.NE.M2)) GO TO 7
    IF (NOW.LT.2) GO TO 7
    DO 5 K=1,NOW
    5  CALL ROTATE (X(K,J),Y(K,J),SIN2,COS2,1.0)
    IF (J.EQ.1.OR.J.EQ.M2) GO TO 6
    IF (X(1,J).GE.X1.OR.X(NOW,J).LE.X1) GO TO 7
    6  M=M+1

```

```

7
CALL SECOND (X(I,J),Y(I,J),NOW,XI,YH(M))
IF (M.EQ.1) YH(1)=SQRT(2.0*X1-X1*X1)
CALL SECOND (X(I,J),DF(I,J),NOW,XI,DFH(M))
IF (M.EQ.1) DFH(1)=ATAN(1.0-X1)/YH(1)*RAD+ANG
CALL SECOND (X(I,J),VM(I,J),NOW,XI,VMH(M))
CALL SECOND (X(I,J),SR(I,J),NOW,XI,SRH(M))
CONTINUE
DR=(YH(M)-YH(1))/(IRINGS-1.)
DO 8 J=1,NRING
XJ=J-1
XH(I,J)=X1
RP(I,J)=YH(1)+XJ*DR
CALL SECOND (YH,DFH,M,RP(I,J),TH(I,J))
CALL SECOND (YH,VMH,M,RP(I,J),VV(I,J))
CALL SECOND (YH,SRH,M,RP(I,J),PT(I,J))
IF (J.EQ.1) PT(I,J)=SR(I,1)
CALL ROTATE (XH(I,J),RP(I,J),-SIN1,COS1,1.0)
SINO=SIN1
COSO=COS1
WRITE (6,13) XM,GAMA,ALDEG,X1,BDRAG
WRITE (4,13) XM,GAMA,ALDEG,X1,BDRAG
DO 10 I=1,NRING
WRITE (6,12) I
DO 10 J=1,MERIDS
XX=RP(J,I)*COS(PSI(J)/RAD)
Z=RP(J,I)*SIN(PSI(J)/RAD)
PTS=PT(J,I)
THS=TH(J,I)
PSIS=PSI(J)
STIS=SIN(THS/RAD)
U=STIS*COS(PSIS/RAD)
V=COS(THS/RAD)
W=STIS*SIN(PSIS/RAD)
CALL ROTATE (XH(J,I),Z,-SINA,COSA,1.0)
CALL ROTATE (V,W,-SINA,COSA,0.0)
SQ=U**2+W**2
PSIS=SIGN(ACOS(U/SQ),W)*RAD
THS=ACOS(V/SQ)*RAD
WRITE(6,14) Z,XX,VV(J,I),PTS,THS,PSIS
WRITE(4,14) Z,XX,VV(J,I),PTS,THS,PSIS

```

```

AE 82
AE 83
AE 84
AE 85
AE 86
AE 87
AE 88
AE 89
AE 90
AE 91
AE 92
AE 93
AE 94
AE 96
AE 97
AE 98
AE 99
AE 100
AE 101
AE 102
AE 103
AE 104
AE 105
AE 106
AE 107
AE 108
AE 109
AE 110
AE 111
AE 112
AE 113
AE 114
AE 115
AE 116
AE 117
AE 118
AE 119

```

AE 122
AE 123
AE 124
AE 125
AE 126
AE 127
AE 128
AE 129
AE 130
AE 131

CONTINUE

10

C

C

11 FORMAT (1M1,5X,17HANGLE OF ATTACK =,F5.2,5X,12HCONE ANGLE =,F12.5,
15X,12HDATA PLANE =F12.7)

12 FORMAT (9M-RING NO.,13/6X,1HZ,13X,1HX,12X,4HMMACH,10X,6HPT/PTO,8X,5
1HTHETA,8X,3HPSI)

13 FORMAT(3F10.5,2F10.8)

14 FORMAT (2E15.7,F10.7,E15.7,F12.8,F13.8)
END

1
2
3
4
5
6

AF
AF
AF
AF
AF
AF

SUBROUTINE ROTATE (X,Y,SINE,COSINE,D)
TEMP=X-D
X=COSINE*TEMP+SINE*Y-D
Y=-SINE*TEMP+COSINE*Y
RETURN
END


```

C
SUBROUTINE SECOND (X,Y,N,XP,YP)
2ND ORDER LAGRANGE INTERPOLATION SUBROUTINE
DIMENSION X(1),Y(1)
M=N-1
ARROW=XP-X(1)
N1=N/2+1
IF ((X(N1)-X(1))*ARROW) 1,1,2
1 IP=2
GO TO 4
2 DO 3 I=2,M
IP=1
IF ((XP-X(I))*ARROW) 4,4,3
3 CONTINUE
4 A=XP-X(IP-1)
B=XP-X(IP)
C=XP-X(IP+1)
D=X(IP-1)-X(IP)
E=X(IP-1)-X(IP+1)
G=X(IP)-X(IP+1)
T1=Y(IP-1)/(D+E)
T2=-Y(IP)/(D+G)
T3=Y(IP+1)/(E+G)
YP=T1*B+C+T2*A+C+T3*A*B
IF (N.EQ.2) YP=(Y(IP)*A-Y(IP-1)*B)/(A-B)
RETURN
END

```

```

AG 1
AG 2
AG 3
AG 4
AG 5
AG 6
AG 7
AG 8
AG 9
AG 10
AG 11
AG 12
AG 13
AG 14
AG 15
AG 16
AG 17
AG 18
AG 19
AG 20
AG 21
AG 22
AG 23
AG 24
AG 25
AG 26

```

SECTION V

FUNCTIONAL DESCRIPTION OF SUBROUTINES

OVERLAY (BLUNT, 0, 0)

- IVALUE - Main program. Calls each subordinate program in sequence.
- ENTRPG - General Lagrangian interpolation.

OVERLAY (BLUNT, 1, 0)

- BLUNTS - Main program for blunt body solution. Reads in data, sets up initial parameters, and governs course of iteration for the correct shock wave shape.
- BODY - Determines equation for body, given the set of body points, and determines the coefficients for the equations describing the Mach number variation along the body.
- XY - Calculates the Cartesian coordinates of a field, body or shock point.
- DIFATE - Performs a seven point central difference calculation to determine the first and second derivatives of data along a given shock, field or body line.
- IDTHER - Determines the ideal gas thermodynamic properties of a given point in the flow field.
- IMAIN - Carries out the inverse blunt body solution based on the parameters specified by BLUNTS

OVERLAY (BLUNT, 2, 0)

- IVLS - Main program for determining the properties along a line through the blunt body flow field in order to start the rotationally symmetric method of characteristics solution
- DETER - Interpolates for all properties at a given point.
- BBOUT - Prints out the final correct blunt body solution.

OVERLAY (BLUNT, 3, 0)

- MOCS - Main program for rotationally symmetric method of characteristics solution.
- BODI - Carries out body point solution.

- OPER8 - Organizes the field and body point solutions and determines when the calculations have been carried sufficiently far downstream.
- FIELD - Carries out field point solution.
- VMACH - Calculates Mach number from static and total pressures.
- ENTROP - Keeps track of the relationship between total pressure and stream function, and, given one of these, determines the other.
- TSON - Calculates the shock wave angle necessary to develop a downstream Mach number of unity.
- DIF - Performs linear interpolation along characteristics.
- CHANGE - Promotes and demotes characteristics during the calculation.
- INPUT - Reads the input data and makes the necessary dimensional changes.
- SHAPE - Generates the values of the coefficients defining the body and the step sizes required.
- DROP - Checks the geometric relationship between points on the initial value line and just downstream of the bow shock and drops any unnecessary points.
- OUTPUT - Arranges and prints the program output.
- WAVE - Solves the Rankine-Hugoniot relations to determine the properties downstream of a shock wave.
- SHOCK - Carries out shock point solution.
- MESH - Controls step size along the bow shock in order to achieve desired step size along the body.
- PAGE - Keeps track of lines printed and skips to a new page when necessary. Also prints page number in upper right hand corner.
- ANGLE - Computes Mach angle from Mach number.
- VELOC - Calculates V/V_{\max} from Mach number.

OVERLAY (BLUNT, 4, 0)

- IVSES - Main program for the interpolation of the initial value surface.
- ROTATE - Rotates a vector through a specified angle.
- SECOND - A specialized second order Lagrangian interpolation.

PART 2: THE THREE-DIMENSIONAL METHOD OF CHARACTERISTICS PROGRAM

SECTION I

INTRODUCTION

The Three-Dimensional Method of Characteristics Program calculates inviscid supersonic flows about smooth three-dimensional bodies at angles of attack. Given an initial value surface (IVS), freestream conditions, and a properly described body, the program determines the flow field downstream of the IVS until a user-specified station is reached. The program can also run back-to-back with the Initial Value Surface Program. In this case, the IVS is automatically provided by the Initial Value Surface Program, and only the freestream conditions and the body description need be provided by the user.

The program uses two temporary files TAPE2 and TAPE4, and on options it reads the IVS from TAPE4 and writes the output on TAPE1.

The Three-Dimensional Method of Characteristics Program has computed a variety of flow fields and has proven to be efficient and versatile. Certain limitations of the program are noted here. The local Mach number must be greater than 1.0 everywhere. Hence the freestream must be supersonic, and the configuration must be such that no subsonic region exists at the juncture between the canopy and the fuselage or between the wing leading edge and fuselage. The body must be smooth, without any surface slope discontinuity (i. e., at any point on the body a unique normal exists). Different numbers of data points per ring (up to a maximum of 48 points) may be assigned in different body regions (up to 20 regions).

SECTION II

BODY DESCRIPTION

Every configuration has a number of generating lines, such as the upper profile, the lower profile, the maximum breadth line, or the wing leading edge. In the present body description procedure, each generating line is divided into a number of segments to permit each segment to be described by a conic-section curve. At each cross section of the configuration, simple analytic curves, e.g., the ellipse or cubic, connect any two adjacent generating lines to form the contour of the cross section. The configuration is thus described analytically by simple low-order curves. For a smooth body a unique normal to the surface exists everywhere, and this condition usually requires slope continuity at the junctures between two contour curves or two segments of a generating line.

The fuselage is located in a right-handed coordinate system where the Y-axis is aligned with the fuselage axis; the X-axis is spanwise and the Z-axis is up. All generating lines are represented by a general curve fit of conic sections in several segments. The conic-section curve takes the form

$$\begin{pmatrix} Z \\ X \end{pmatrix} = PY + Q + SG(RY^2 + SY + T)^{1/2}$$

where $SG = \pm 1$. A straight line is a special case with $R = S = T = 0$. Each curve can be divided into as many segments as necessary to provide adequate body description. Each segment must be continuous with the previous segment and with very few exceptions the slope must be continuous at the junctures to satisfy the requirement of a unique normal to the surface.

A typical cross section of the wing-body configuration is shown in Figure 14. Through each point marked by a dot, a generating line which is a function of Y passes. For input cards, the following Table shows the curve number corresponding to the two projections of each of the generating lines.

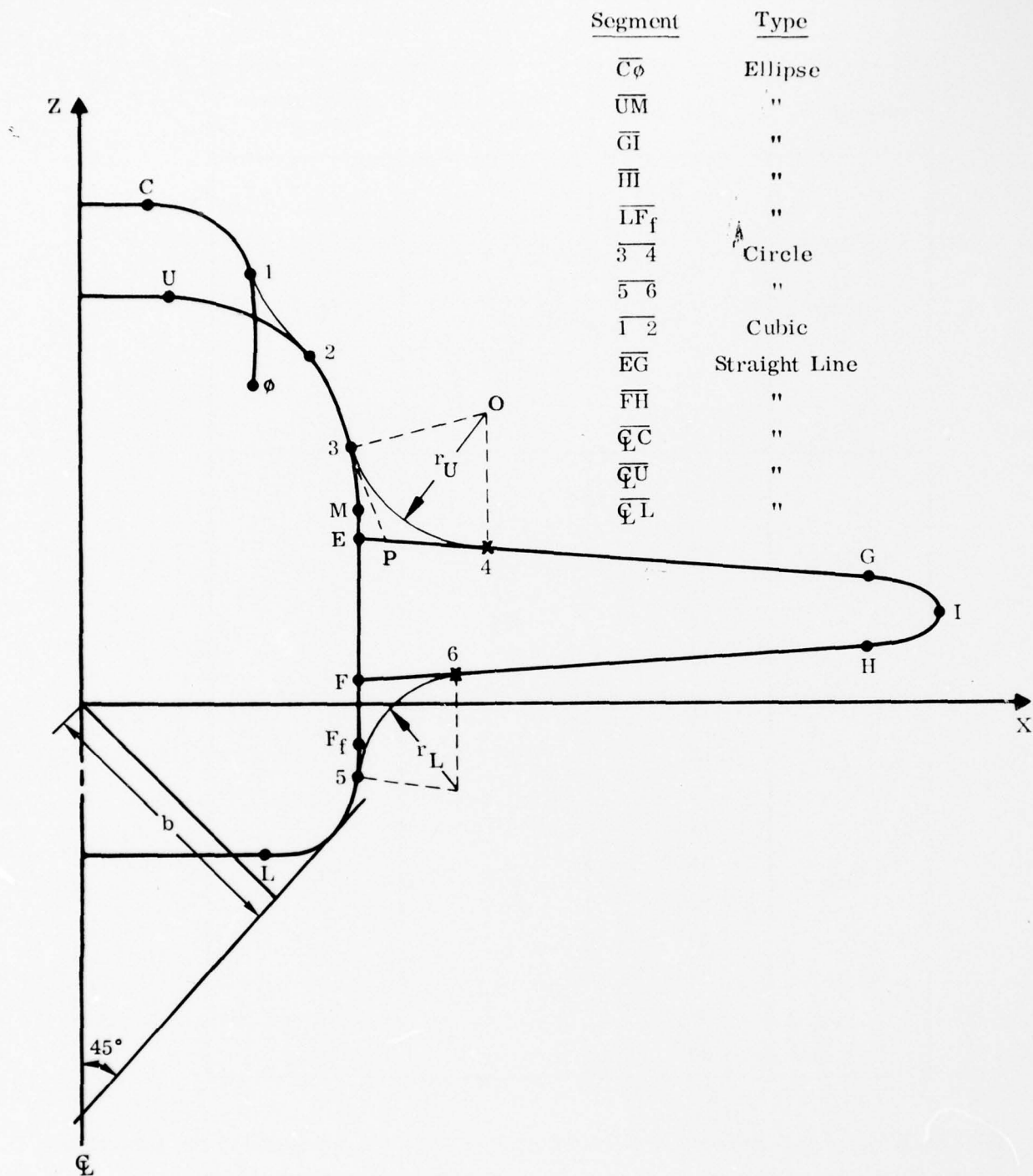


FIGURE 14. SCHEMATIC OF FUSELAGE AND WING CROSS SECTIONS DESCRIPTION

Geometry	Curve No.	Designation Phase I	Designation Phase II
Fuselage	1	Z_U	Z_U
	2	Z_M	Z_M
	3	Z_L	Z_L
	4	X_U	X_U
	5	X_M	X_M
	6	X_L	X_L
	7	b	Z_{Ff}
Canopy	8	Z_1	Z_1
	9	Z_2	Z_2
	10	Z_c	Z_c
	11	Z_ϕ	Z_ϕ
	12	X_ϕ	X_ϕ
	13	X_c	X_c
Wing	14		Z_E
	15		Z_F
	16		Z_G
	17		Z_H
	18		Z_I
	19		X_G
	20		X_H
	21		X_I
	22		Z_3
	23		Z_5

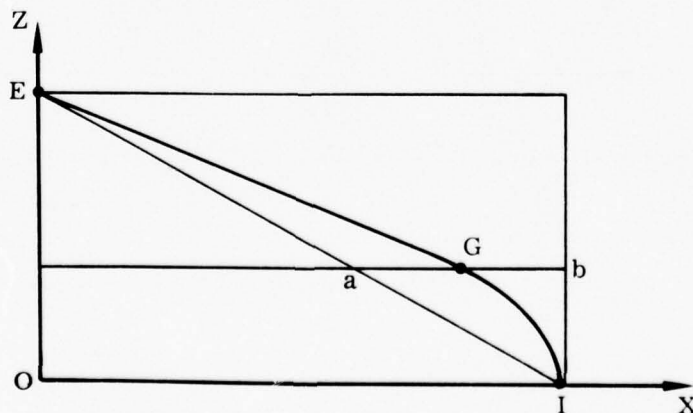
For instance, curve number 3 denotes the projection on the Y-Z plane of the generating line that passes through point L for both Phase I and Phase II designations. Aside from the wing, the only difference between these two phases is in curve 7. While a shape factor b was used in Phase I to alter the lower fuselage, a side flat section was used in Phase II.

As shown in Figure 14, the contour of the cross section begins with a straight line representing the canopy flat. The canopy contour from points C to ϕ is circular but can be elliptic in general. The upper fuselage is represented by an elliptic curve

from points U to M. A straight side flat from points M to F_f joins the upper fuselage to the lower fuselage, which is also represented by an elliptic curve from F_f to L. A straight line from point L to the centerline describes the bottom flat. For the description of the wing, straight lines EG and FH represent the upper and lower surfaces of the wing, respectively. Partial ellipses GI and HI complete the wing description near the leading edge I. The wing-body blending is effected by circular arcs 34 and 56 with radii r_U and r_L , respectively.

In general, the configuration are divided into a number of sections since some of the generating lines can only be described by a composite of conic-section curves. Some of the conic-section curves, however, may remain valid throughout a few sections. To avoid repetition of the input data, the body description subroutine FIGURE reads the data in the following manner (see also Section IV, Input/Output Description). For the first body section, the first card specifies the end of the section and seven conic-section curves. This is followed by 7 cards of body description coefficients, each describing one curve. For a subsequent body section, the first card specifies the end of that particular section and the total number, KT, of conic-section curves that require new values of the coefficients for that section. Only KT cards are then used to supply these new values.

In Figure 14, the projections of lines passing through E, F, G, H and I on the Z-Y plane and X-Y plane are input quantities for defining the wing. In order for the partial ellipses GI and HI to exist, points G and H must be located within a certain range, which depends on the relative position of these five points. When the wing span is very small, it is difficult to input both projections of lines through G and H such that these points are located within acceptable ranges. In such cases, the X coordinates of G and H are calculated inside the program to satisfy the range requirement. As shown in the sketch,



when the projections X_E , Z_E , X_I , Z_I and Z_G are given through input, X_G can be calculated when the ratio $R = Gb/ab$ is specified.

Indeed,

$$\frac{RGb}{X_I - X_E} = \frac{ab}{X_I - X_E} = \frac{Z_G - Z_I}{Z_E - Z_I}$$

$$\text{and } X_G = X_I - Gb = X_I + \frac{Z_G - Z_I}{R} \left(\frac{X_E - X_I}{Z_E - Z_I} \right)$$

when fitting the generating lines, a fuselage station is selected ahead of which the projection X_G is not fitted because X_G will be generated by the program according to the above formula with a constant R taken at this fuselage station and input to the program. Since at this station the derivative of X_G with respect to Y can be calculated from the formula, this derivative should be used to fit the projection X_G for fuselage stations immediately behind the selected station.

SECTION III

GRID ARRANGEMENT

Since the geometry of the wing-body configuration is fairly complicated, a procedure was developed to arrange the grid points for efficient calculation. The contour of a wing-body cross section has a number of regions that undergo sharp changes of curvature, where a very fine grid structure is needed. On the other hand, in regions only mild changes of curvature occur, a coarse grid structure suffices.

A sketch of a typical contour is shown in Figure 15, together with the grid points and the labeling of controlling key points. Quantities K_1, K_2, \dots, K_8 are specified through input data; for instance, if $K_7 = 20$, it means K_7 is the 20th point counting from the lower profile. Quantities K_9 to K_{12} are obtained by adding to K_7 the differences between K_7 and K_6 to K_3 , respectively; for instance, if $K_6 = 17$, then $K_9 = 23$. The quantity K_8 specifies the number of points to be added in regions near the wing-body juncture and the wing leading edge; for instance, $K_8 = 2$ as illustrated. Basically, single grid spacings are assigned from K_1 to K_2 , K_3 to K_{5+1} , K_{6-1} to K_{9+1} , K_{10-1} to K_{12} , not counting the additional points specified by K_8 . Anywhere else double spacings are assigned. The grid size below the wing leading edge, where K_7 is located, is in general different from that above the leading edge and the difference depends on the value of K_7 . Additional points specified by K_8 are added to each single grid space from K_4 to K_5 , K_6 to K_9 , K_{10} to K_{11} . Care and some experience are needed in assigning the K 's. However, the program has the capability to center the series of points from K_4 to K_5 (and hence K_{10} to K_{11}) around the wing-body juncture. The group of points from K_1 to K_2 is designed to cover the fuselage-canopy juncture. All K 's are set to zero at fuselage stations before the canopy. Between fuselage-canopy juncture and the wing-body juncture only K_1 and K_2 are assigned proper values while all other K 's are set to zero.

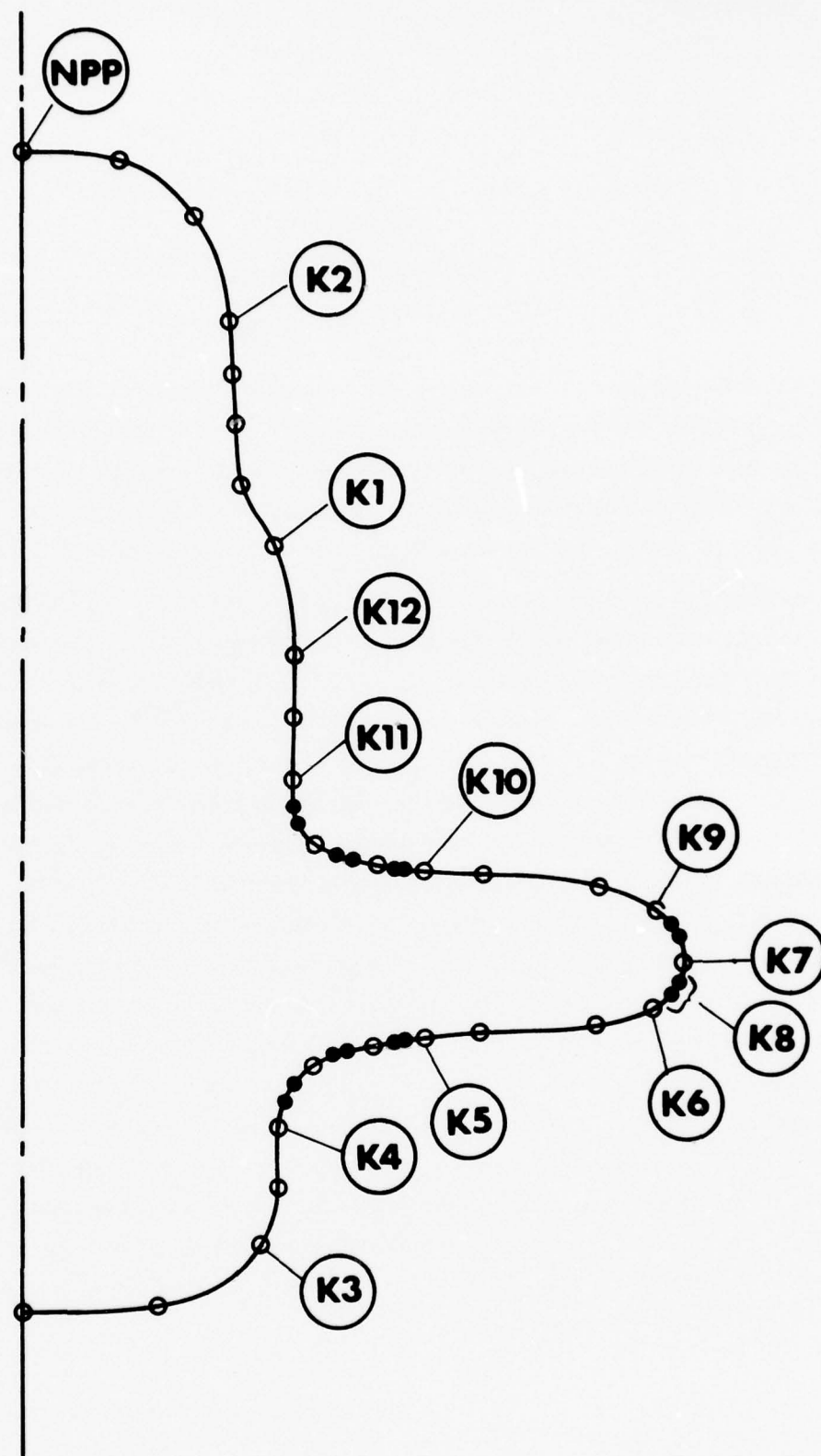


FIGURE 15. GRID STRUCTURE AND CONTROLLING DATA POINTS

SECTION IV

INPUT/OUTPUT DESCRIPTION

1. INPUT DESCRIPTION

The Three-Dimensional Method of Characteristics Program offers some input and output options. The program can run using the IVS data on punched cards or it can run back-to-back with the initial Value Surface Program, which provides the IVS data through a temporary file, TAPE4.

The input data cards required by the Three-Dimensional Method of Characteristics Program are shown in Figure 16. They are described in detail below.

Card No	Variable	Format	Description
①	LIT	18A4	Problem identification
②	DP	F10.5	Convergence criterion for P, 0.1 to 10^{-5}
	DTHETA	F10.5	Convergence criterion for θ^* , 0.1 to 10^{-5}
	DPSI	F10.5	Convergence criterion for ψ^* , 0.1 to 10^{-5}
	EPSLN	F10.5	Convergence criterion for μ , 0.1 to 10^{-5}
	DYC	F10.5	Initial step size which satisfies the Courant-Friedrichs-Lewy stability condition, i.e., $DYC \cdot \tan \mu < \sqrt{2} d$, where μ is the local Mach angle and d is the shortest distance between two data points. If $DYC = 0$, the program will generate an initial step size.
	YSTOP	F10.5	Computation stops when $Y \geq YSTOP$. YSTOP cannot be set equal to 0.
	STEMP	F10.5	Maximum step size (when $STEM > 0$)
	WINGST [†]	F10.5	Fuselage station at which the wing begins (110 for the sample case)

*The relationship between the flow angle θ or ψ and the coordinate system is shown in Figure 16a.

[†]Variables or cards so marked are not needed for the Phase I program.



Card No	Variable	Format	Description
③	NSURF	I5	Total number of surfaces desired, counting from IVS, even for a restart from a data surface
	LINE	I5	Number of data rings per surface. LINE is updated by data from card 7 for a restart from cards
	NPC	I5	Number of data points per ring. NPC is updated by data from card 7 for a restart from cards
	NR	I5	Number of regions having different NPC. $1 \leq NR \leq 20$
	IFT	I5	Control for reading IVS data. <div style="margin-left: 40px;"> If IFT = 0, IVS data is on cards = 1, IVS data is on TAPE4 </div> Also, if $IFT = K < 0$, then number of rings per data surface is increased by $ K $ during restart from TAPE1. $ K \leq 2$ is recommended.
	ISTART	I5	Restart control* <div style="margin-left: 40px;"> If ISTART $\begin{cases} < 0, \text{ restart from cards} \\ = 0, \text{ initial run} \\ = 1 > 0, \text{ restart from Ith data surface on TAPE1} \end{cases}$ </div>
	KP4	I5	Output control. If $KP4 = K > 0$, every data surface is written on TAPE1, with every Kth surface printed out. If $KP4 = K \leq 0$, every data surface is printed out. If $K = 0$, every 10th data surface is written on TAPE1. If $K < 0$, every Kth data surface is punched out on cards.
	NS	I5	Identifying number of the surface on which print level KPRINT (1) will apply
	NL	I5	Identifying number of the ring on data surface NS along which print level KPRINT (2) will apply
	NP	I5	Identifying number of the data point along ring NL on data surface NS at which print level KPRINT (3) will apply
	KPRINT (1)	I5	Print level control,** usually 0 <div style="margin-left: 40px;"> If KPRINT (1) $\begin{cases} = 0, \text{ normal print} \\ = 1, \text{ moderate default print} \\ = 2, \text{ extensive default print} \end{cases}$ </div>
	KPRINT (2)	I5	Print level control, usually 0 or 1
	KPRINT (3)	I5	Print level control. See Section V

*For restart, insure $ISTART \neq 0$, or data on TAPE1 will be ruined

**See Section V for warning on print level

Card No	Variable	Format	Description
④	YSET(I)	F10.5	For all $Y \leq YSET(I)$, the number of points per ring to be calculated is specified by the variable NPSET(9I-8), and the grid size is specified by NPSET(9I-7) . . . NPSET(9I) (See Section III where K_1 denotes NPSET(9I-7) . . . K_8 denotes NPSET(9I))*
	NPSET(9I-8)	I5	
	NPSET(9I-7)	I5	
	⋮	⋮	
	NPSET(9I) [†]	I5	

• There now follow cards, I = 2, NR

⑤	FMSTR	F10.5	Freestream Mach number
	GF (1)	F10.5	Ratio of specific heats
	ALFA	F10.5	Angle of attack, in degrees
	Y0	F10.5	Y-Coordinate of initial value surface. Needed only for an initial run using IVS data from cards. May be left blank for all other cases.
⑥	YA	F10.5	Y-coordinate of center of spherical nose
	ZA	F10.5	Z-coordinate of center of spherical nose
	SCALE	F10.5	Scale factor (radius of spherical nose)
	WINGA	F10.5	Wing area, Sq. Ft. (reference area for C_{DW})
	DBLNL [†]	F10.5	Distance between points 5 and F in Figure 14 (0.5 for sample case)
⑦ [†]	NCQ	I5	Number of sections needed to fit the blending curve (#22 for the sample case) by conic sections
⑧ [†]	J	I2	Section number
	CQ(1, J)	E15.7	Fuselage station representing lower limit of the section
	CQ(2, J)	E15.7	Fuselage station representing higher limit of the section

*Note that for the Phase I program only K_1 and K_2 are used.

[†]Variables or cards so marked are not needed for the Phase I program.

Card No	Variable	Format	Description
⑨ [†]	IC	I2	Curve number for blending (#22 for the sample case)
	CQ(3, J)	E15.7	Conic coefficient P(J)
	⋮	⋮	⋮
	CQ(7, J)	E15.7	Conic coefficient T(J)
	CQ(8, J)	F2	Conic coefficient SG(J)

- There now follow sets of cards, $J = 2, NCQ$, each set describing a section.
- If $ISTART \geq 0$, omit cards 10, 11, 12, 13
- Note: Cards 10, 11, 12, 13 are required only for a restart using data on punched cards. They are generated by the 3DMoC Program when the flow field data is punched out through the KP4 option. Value of the restart parameters are also part of the printout for each data surface. The variable INGRES may be set at a different value as explained below.

⑩	ISURF	I5	} Restart parameters
	LINE	I5	
	ILL	I5	
	KURE	I5	
	MESS	I5	
	INGRES	I5	
⑪	NPC	I5	} Restart parameters*
	KI(1)	I5	
	⋮	⋮	
	⋮	⋮	
	KI(8) [†]	I5	
⑪	SINE	E15.8	} Restart parameters
	COSINE	E15.8	
	S2	E15.8	
	C2	E15.8	

*When making a restart after an initial run, be sure to remove IVS data cards, if they were present for the initial run.

Card No	Variable	Format	Description
⑫	DYC	E15.8	Restart Parameters
	STEP	E15.8	
	Y0	E15.8	
	DRAG	E15.8	
⑬	ALIFT	E15.8	Restart Parameters
	TORQUE	E15.8	
	● GO TO card 15 unless		$\left. \begin{array}{l} \text{I} \text{START} = 0 \text{ and } \text{I} \text{FT} = 0, \text{ or} \\ \text{I} \text{START} < 0 \end{array} \right\}$
⑭	A(J, 3, I)	E15.8	Z-coordinate of data point
	A(J, 1, I)	E15.8	X-coordinate of data point
	A(J, 7, I)	F10.7	Mach number at data point
	A(J, 8, I)	E15.8	Total pressure ratio, $P_t/P_{t\infty}$
	THETT(J, I)	F12.8	Flow angle θ
	PSIT(J, I)	F13.8	Flow angle ψ
	● There now follow cards, J = 2, NPC which describe a ring on the data surface		
	● There now follow sets of cards, I = 2, LINE with each set describing a ring on the data surface		
⑮	YMAX	F10.5	Y-coordinate of the end of the first body section described by the coefficients to follow.
	N	I5	Number of body description curves for the body sections. Must be set equal to 7.
	MOD [†]	I5	= 1, fuselage only; = 2, fuselage - canopy; = 3, fuselage - wing; = 4 fuselage - canopy-wing
	RATIO [†]	F10.5	Ratio for partial ellipse (see Section II) If Ratio > 0, curves 19 and 20 are generated by the program. **

**For the sample case, RATIO > 0 between F.S. 110 and F.S. 220

Card No	Variable	Format	Description
①⑥	L	I2	Identifying number of the body description curve
	P(L)	E15.8	Body description coefficients (See Section II)
	Q(L)	E15.8	
	R(L)	E15.8	
	S(L)	E15.8	
	T(L)	E15.8	
	SG(L)	F2.0	

- There now follow cards, $L = 2, 6$
- If the body is described by only one section, no further data is required

①⑦	YMAX	F10.5	Y-coordinate of the end of the next body section described by the coefficients to follow
	KT	I5	Total number of body description curves that need new values of P, Q, R, S, T, SG for this body section
	MOD [†]	I5	See card 15
	RATIO [†]	F10.5	See card 15

①⑧	M	I2	Identifying number of the body description curve which requires new coefficients
	P(M)	E15.8	Body description coefficients
	Q(M)	E15.8	
	R(M)	E15.8	
	S(M)	E15.8	
	T(M)	E15.8	
	SG(M)	F2.0	

- There now follow a total of $KT-1$ cards, giving the new coefficients for this body section
- There now follow sets of cards, starting with card type 17, each set describing the subsequent body sections to the end of the configuration

2. OUTPUT DESCRIPTION

A number of output options are available through the control index KP4, which is part of the input data. If $KP4 = K > 0$, every data surface is written on TAPE1 with every Kth data surface printed out for sampling. If $KP4 = K < 0$, every data surface is printed out, while retaining certain data surfaces for a restart (see also Section V, Operational Aspects). If $K = 0$, every 10th data surface is written on TAPE1. If K is negative, then every Kth surface is punched on cards.

When any output is written on TAPE1, the user should either use a physical tape as TAPE1, through a request control card, or copy TAPE1 to a physical tape as many times as there are data surfaces through a COPYCF control card before termination. Otherwise, information on TAPE1, which is a scratch disc file, will be lost upon termination of the run. A restart at a later time can be made from the physical tape. The data surfaces on the tape can be printed out by copying them to OUTPUT through a control card COPYCF (NAME, OUTPUT, N), where NAME is the tape designation and N is the number of data surfaces to be printed out. The tape can also be taken to a peripheral processor for printing of the data surfaces.

Figure 17 shows a normal printout for a data surface. X, Y, Z, are the coordinates of a data point (see Figure 15 for the coordinate system). P is the static pressure and PT is the total pressure, with the subscript 0 referring to freestream quantities. The angles OUTWASH and UPWASH, in degrees, are included since they are more meaningful than θ and ψ . These angles are related to the direction cosines u, v, w of the velocity vector by: $OUTWASH = \text{atan}(u/v)$, $UPWASH = \text{atan}(w/v)$, $\theta = \text{acos}(v)$, and $\psi = \text{atan}(w/u)$.

Figure 18 shows a data surface where the CFL stability condition was violated at certain data points. When the velocity vector is aligned with the Y-axis, certain flow angles are undefined. When this condition is detected by the program, the coordinate system is automatically rotated and the particular data surface is recomputed. An example of such occurrences is shown in Figure 19.

When the normal output is written on TAPE1, every Kth surface is printed out for sampling. An example of this is shown in Figure 20, where the 5th data surface is printed out completely, while the upper and lower centerline pressure coefficients on the body surface are printed out for data surfaces 6 through 9.

DATA SURFACE NO 50

***TO USE THIS AS AN INITIAL VALUE SURFACE, KEY PUNCH FIRST 6 COLUMNS OF DATA AS INPUT CARDS

SURFACE NO 50, STATION Y = .69602455E+01

BODY POINTS											
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	--PSI--DEG--	-----CP-----	-----P/P0-----	-----P/PT0-----	OUTWASH	SHIPWASH	
-.26323191E+01	-.20385704E-11	1.6777867	-.67039950E-02	14.99999998	-90.00000000	.33202E+00	.62428E+02	.12416E-02	0.00	15.00	
-.26930217E+01	.84481781E+00	1.7119138	.67039950E-02	15.14021458	-58.90000772	.31581E+00	.59428E+02	.12200E-02	8.06	13.22	
-.20918693E+01	.15977245E+01	1.8123940	.67039950E-02	16.19329874	-29.94616641	.27245E+00	.51407E+02	.10554E-02	14.12	-8.25	
-.14762228E+01	.21743025E+01	1.9760670	.67039950E-02	17.1117257	-4.23829123	.21421E+00	.40632E+02	.83416E-03	17.13	-1.31	
-.71647510E+00	.25328111E+01	2.1886184	.67039950E-02	17.88033751	18.05198180	.15704E+00	.30054E+02	.61700E-03	17.05	5.71	
.10587877E+00	.26100771E+01	2.4306471	.67039950E-02	18.12135956	37.34813305	.11077E+00	.21493E+02	.44125E-03	14.58	11.23	
.91089550E+00	.24686906E+01	2.6926111	.67039950E-02	17.93319195	54.35713544	.76300E+01	.15133E+02	.31068E-03	10.64	14.74	
.16181831E+01	.20761614E+01	2.9180800	.67039950E-02	17.18787480	67.9816241	.55742E+01	.11133E+02	.23225E-03	6.64	15.99	
.21687872E+01	.14945004E+01	3.0737217	.67039950E-02	16.17658692	77.93828499	.44925E+01	.93117E+01	.19117E-03	3.47	15.84	
.25136693E+01	.78121145E+00	3.1527414	.67039950E-02	15.32772121	84.89024934	.40276E+01	.84516E+01	.17351E-03	1.40	15.27	
.26323191E+01	-.95484356E-12	3.1740096	.67039950E-02	14.99999998	90.00000000	.39110E+01	.82358E+01	.16908E-03	0.00	15.00	
FIELD POINTS											
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	--PSI--DEG--	-----CP-----	-----P/P0-----	-----P/PT0-----	OUTWASH	SHIPWASH	
-.27976734E+01	-.30708077E-11	2.6656985	.27292557E-01	13.31310132	-90.00000000	.33940E+00	.63829E+02	.13104E-02	0.00	13.31	
-.26524812E+01	.90366439E+00	2.6963417	.27043901E-01	13.51892781	-61.23774330	.32294E+00	.60748E+02	.12472E-02	6.60	11.90	
-.22346296E+01	.17137388E+01	2.7888730	.26363194E-01	14.04846027	-34.16076513	.27812E+00	.52492E+02	.10776E-02	11.70	-8.00	
-.15948933E+01	.23547420E+01	2.9377430	.25123766E-01	14.71087442	-9.76328100	.21812E+00	.41355E+02	.84901E-03	14.51	-2.55	
-.79941041E+00	.27727044E+01	3.1232295	.23336648E-01	15.34037100	11.69186140	.15945E+00	.30500E+02	.62616E-03	15.04	3.18	
.75389643E+01	.29387271E+01	3.3255777	.21341877E-01	15.78929729	30.20675453	.11277E+00	.21864E+02	.44887E-03	13.73	8.10	
.10540670E+01	.28449322E+01	3.5724237	.19633626E-01	16.04806564	47.64526664	.76288E+01	.15114E+02	.31029E-03	10.97	12.00	
.19396953E+01	.24431095E+01	3.7451265	.17649843E-01	16.06534175	61.98431124	.55166E+01	.11204E+02	.23003E-03	7.70	14.26	
.26457122E+01	.17857145E+01	3.8498956	.16066152E-01	15.84616070	73.40760919	.43773E+01	.90985E+01	.18679E-03	4.63	15.22	
.31012417E+01	.94243880E+00	3.8991642	.15053060E-01	15.58485241	82.40581374	.38294E+01	.80848E+01	.16598E-03	2.11	15.45	
.32587489E+01	-.18649713E-11	3.9115300	.14693739E-01	15.47540440	90.00000000	.36690E+01	.77881E+01	.15989E-03	0.00	15.48	
FIELD POINTS											
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	--PSI--DEG--	-----CP-----	-----P/P0-----	-----P/PT0-----	OUTWASH	SHIPWASH	
-.29665304E+01	-.30161765E-11	3.2299571	.54116050E-01	11.91968148	-90.00000000	.33045E+00	.62137E+02	.12757E-02	0.00	11.92	
-.28122352E+01	.97196388E+00	3.2810111	.54748474E-01	12.13770459	-60.35933663	.31423E+00	.59136E+02	.12141E-02	6.07	11.59	
-.23697403E+01	.14450779E+01	3.4319847	.54536971E-01	12.46522871	-33.07388660	.27096E+00	.51131E+02	.10474E-02	10.66	-8.99	
-.16971259E+01	.25444420E+01	3.6658618	.54368023E-01	13.27107181	-9.18257228	.21324E+00	.40652E+02	.83048E-03	13.11	-2.16	
-.86170126E+00	.30200117E+01	3.9486194	.59265227E-01	13.84063114	11.11311666	.15780E+00	.30195E+02	.61991E-03	13.59	2.72	
.63255148E+01	.32468202E+01	4.2401023	.58524033E-01	14.31354213	28.00018866	.11376E+00	.22046E+02	.45261E-03	12.70	6.83	
.12081033E+01	.30170727E+01	4.5561987	.55517134E-01	14.91969734	45.34500773	.77408E+01	.15321E+02	.31454E-03	10.61	10.71	
.22664129E+01	.28074301E+01	4.7705603	.50998056E-01	15.45497728	59.46456577	.56764E+01	.11500E+02	.23610E-03	8.00	13.39	
.31260502E+01	.20764533E+01	4.9044262	.47121327E-01	15.74299546	71.11017791	.45400E+01	.93995E+01	.19297E-03	5.21	14.93	
.36889106E+01	.11040547E+01	4.9667372	.44204069E-01	15.84234371	81.03921897	.39640E+01	.83357E+01	.17113E-03	2.53	15.66	
.38848609E+01	-.22887734E-11	4.9836407	.43134643E-01	15.85947158	90.00000000	.37899E+01	.80117E+01	.16448E-03	0.00	15.86	
FIELD POINTS											
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	--PSI--DEG--	-----CP-----	-----P/P0-----	-----P/PT0-----	OUTWASH	SHIPWASH	
-.31351451E+01	-.30659467E-11	3.4733950	.68179800E-01	10.47699753	-90.00000000	.31228E+00	.58776E+02	.12067E-02	0.00	10.48	
-.29713223E+01	.10425048E+01	3.5470307	.70598330E-01	10.78636306	-57.80054023	.29604E+00	.55938E+02	.11484E-02	5.80	-9.14	
-.25023870E+01	.19809951E+01	3.7633794	.77823781E-01	11.51956714	-29.11273550	.25613E+00	.48424E+02	.99413E-03	10.10	-5.66	
-.17933179E+01	.27409980E+01	4.1003025	.88867509E-01	12.35586870	-5.02107111	.20315E+00	.38621E+02	.79289E-03	12.31	-1.10	
-.91347484E+00	.32749428E+01	4.4957342	.10116011E+00	13.17438674	14.38342325	.15464E+00	.29593E+02	.60753E-03	12.78	3.33	
.64156103E+01	.35600466E+01	4.8916615	.11230892E+00	13.87056066	29.43056490	.11709E+00	.22664E+02	.46528E-03	12.14	6.92	
.13713641E+01	.35955241E+01	5.2997805	.11960076E+00	14.90520563	45.10801612	.85693E+01	.16854E+02	.34601E-03	10.64	10.68	
.26015704E+01	.31784251E+01	5.5966917	.12265760E+00	15.93036388	57.97844304	.67517E+01	.13495E+02	.27705E-03	8.61	11.60	
.36159074E+01	.23736922E+01	5.7875031	.12294628E+00	16.72504138	69.18231674	.57311E+01	.11403E+02	.23421E-03	6.10	15.65	
.42882936E+01	.12700193E+01	5.8910988	.12182711E+00	17.23176789	79.71300680	.51874E+01	.10597E+02	.21756E-03	3.17	16.97	
.45239423E+01	-.23904963E-11	5.9236406	.12123819E+00	17.40828270	90.00000000	.50170E+01	.10282E+02	.21109E-03	0.00	17.41	
SHOCK POINTS											
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	--PSI--DEG--	-----CP-----	-----P/P0-----	-----P/PT0-----	OUTWASH	SHIPWASH	
-.33755736E+01	-.30335538E-11	3.6197884	.71476644E-01	8.39261285	-90.00000000	.27652E+00	.52160E+02	.10708E-02	0.00	-8.39	
-.32009045E+01	.11265813E+01	3.7110667	.75753007E-01	8.90781522	-53.85789166	.26447E+00	.49930E+02	.10251E-02	5.28	-7.21	
-.27003179E+01	.21450391E+01	3.9770099	.89203236E-01	10.10834147	-23.80404442	.23297E+00	.44102E+02	.90541E-03	9.26	-4.12	
-.19431837E+01	.29804246E+01	4.3874689	.11294150E+00	11.49100404	-4.44116181	.19310E+00	.38726E+02	.75347E-03	11.49	-1.09	
-.99957110E+00	.35848801E+01	4.8511827	.14423618E+00	12.90737422	17.36666876	.15783E+00	.30200E+02	.62000E-03	12.34	3.91	
.55381788E+01	.39350575E+01	5.2953026	.17872129E+00	14.13077835	30.48329774	.13124E+00	.25282E+02	.51903E-03	12.24	7.28	
.15389353E+01	.40362166E+01	5.7528929	.21882447E+00	15.86885527	44.64861526	.10913E+00	.21228E+02	.43580E-03	11.43	11.30	
.29424946E+01	.34054105E+01	6.0922807	.25147079E+00	17.49489797	57.29123861	.95877E+01	.18735E+02	.38462E-03	9.87	17.45	
.41491131E+01	.27127502E+01	6.3029156	.27292136E+00	18.71557603	68.47196915	.88448E+01	.17368E+02	.35656E-03	7.09	17.45	
.49421380E+01	.14580109E+01	6.4300267	.28624909E+00	19.47717631	79.28847527	.84376E+01	.16601E+02	.34082E-03	3.76	19.14	
.52211780E+01	-.22729670E-11	6.4719569	.29076667E+00	19.73873885	90.00000000	.83008E+01	.16357E+02	.33582E-03	0.00	19.74	

TO USE AS IVS, PUNCH THE 3 CARDS, PLACE BEFORE BODY PT CARDS

50 5 0 0 0 0 0 11
 0. 1.00000000E+01 0. 1.00000000E+01
 .19505687E+00 .50000000E-01 .69602455E+01

FIGURE 17. NORMAL DATA SURFACE

DATA SURFACE NO 47

***TO USE THIS AS AN INITIAL VALUE SURFACE, KEY PUNCH FIRST 6 COLUMNS OF DATA AS INPUT CARDS

SURFACE NO 47, STATION Y = .64024979E+01

BODY POINTS									
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	-----PSI, DEG-----	-----CP-----	-----P/P0-----	-----P/P10-----	OUTWASH P/WASH
-.24828711E+01	-.20385704E-11	1.6974006	-.67039950E-02	14.99999998	-90.00000000	.32241E+00	.60686E+02	.12459E+02	0.00-15.00
-.23472154E+01	.80935275E+00	1.7327764	-.67039950E-02	15.35006741	-58.42099998	.30638E+00	.57665E+02	.11839E+02	8.18-13.16
-.19580005E+01	.15266859E+01	1.8362326	-.67039950E-02	16.21000179	-29.17418670	.26307E+00	.64971E+02	.10197E+02	14.25-11.07
-.13647476E+01	.20740173E+01	2.0023023	-.67039950E-02	17.18056230	-3.41336958	.20613E+00	.79131E+02	.80345E+03	17.15-11.05
-.63910506E+00	.21991367E+01	2.2134315	-.67039950E-02	17.84895448	18.76855390	.15148E+00	.29026E+02	.59589E+03	16.98-15.92
.13903661E+00	.24788412E+01	2.4490684	-.67039950E-02	18.64852226	37.89843248	.10789E+00	.20940E+02	.43611E+03	14.42-11.32
.89418079E+00	.23161535E+01	2.6982275	-.67039950E-02	17.82957909	54.69630300	.75789E+01	.15022E+02	.30440E+03	10.53-14.71
.15517372E+01	.19382250E+01	2.9066942	-.67039950E-02	17.10118700	68.11550318	.56632E+01	.11478E+02	.23563E+03	6.54-15.93
.20573989E+01	.13896798E+01	3.0472019	-.67039950E-02	16.13565204	78.17381887	.46604E+01	.96223E+01	.19754E+03	3.41-15.81
.23748018E+01	.72441611E+00	3.1161477	-.67039950E-02	15.31914894	85.03319850	.42346E+01	.88381E+01	.18145E+03	1.16-15.28
.24828711E+01	-.12742267E-11	3.1341602	-.67039950E-02	14.99999998	90.00000000	.41324E+01	.86456E+01	.17749E+03	0.00-15.00

BASE POINT 4 VIOLATES CFL

FIELD POINTS									
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	-----PSI, DEG-----	-----CP-----	-----P/P0-----	-----P/P10-----	OUTWASH P/WASH
-.26400132E+01	-.30111226E-11	2.5875106	-.23911452E-01	13.26371613	-90.00000000	.32989E+00	.62034E+02	.12736E+02	0.00-13.26
-.24999425E+01	.86298769E+00	2.6147700	-.23640485E-01	13.48844578	-60.57985591	.31135E+00	.58956E+02	.12103E+02	5.72-11.80
-.20979703E+01	.16344544E+01	2.7124572	-.23088619E-01	14.06340431	-33.03622715	.26906E+00	.50779E+02	.10425E+02	11.25-11.78
-.14449242E+01	.22407143E+01	2.8620830	-.22049761E-01	14.77556676	-8.43636271	.21057E+00	.37995E+02	.80633E+02	14.82-11.22
-.72619610E+00	.26305927E+01	3.0445390	-.20574100E-01	15.43905604	13.01129891	.15477E+00	.29934E+02	.60837E+03	15.06-11.56
.10295106E+00	.27794250E+01	3.2397245	-.18959378E-01	15.89371207	31.36373017	.11049E+00	.21515E+02	.44171E+03	13.67-11.43
.10241345E+01	.22807015E+01	3.4766576	-.17695570E-01	16.13595393	48.55356021	.76738E+01	.15198E+02	.31200E+03	10.44-12.46
.18520927E+01	.26936112E+01	3.6432330	-.16166468E-01	16.11901111	62.65846552	.56765E+01	.11491E+02	.23541E+03	7.84-12.40
.25081436E+01	.16716112E+01	3.7476611	-.14933445E-01	15.86869620	73.84678621	.45642E+01	.94533E+01	.19408E+03	4.60-15.27
.29294808E+01	.84002236E+00	3.8000842	-.14149829E-01	15.58409797	82.61736639	.40312E+01	.84581E+01	.17344E+03	2.05-15.46
.30747430E+01	-.21824434E-11	3.8143873	-.13871183E-01	15.46520429	90.00000000	.38719E+01	.81635E+01	.16760E+03	0.00-15.47

FIELD POINTS									
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	-----PSI, DEG-----	-----CP-----	-----P/P0-----	-----P/P10-----	OUTWASH P/WASH
-.28021286E+01	-.30296590E-11	3.1747894	-.49358509E-01	11.84594392	-90.00000000	.32293E+00	.60579E+02	.12437E+02	0.00-11.85
-.26542043E+01	.92747647E+00	3.2240174	-.44779010E-01	12.06211318	-60.16296564	.30575E+00	.57567E+02	.11818E+02	6.07-10.56
-.22107021E+01	.17500280E+01	3.3687995	-.50962622E-01	12.59373133	-32.70193043	.26278E+00	.49618E+02	.10108E+02	10.65-10.84
-.15885172E+01	.24226454E+01	3.5899365	-.51984252E-01	13.22931604	-8.68361094	.20645E+00	.39233E+02	.80551E+02	13.68-11.03
-.79251392E+00	.28697990E+01	3.8535545	-.52224181E-01	13.85419687	11.66586173	.15384E+00	.29461E+02	.60484E+03	13.58-11.46
.85348625E+00	.30792678E+01	4.1199944	-.51137351E-01	14.39000576	28.58362890	.11210E+00	.21778E+02	.44707E+03	12.70-11.60
.11654922E+01	.30418848E+01	4.4075313	-.48431157E-01	15.03251952	45.85391532	.78027E+01	.15844E+02	.31849E+03	10.49-10.91
.21590426E+01	.26459277E+01	4.7048467	-.44773297E-01	15.55585604	59.90252974	.58203E+01	.11785E+02	.24194E+03	7.95-11.54
.29619787E+01	.19520712E+01	4.7308801	-.41507129E-01	15.81297638	71.46162585	.47232E+01	.97366E+01	.19989E+03	5.15-15.03
.34857033E+01	.10362417E+01	4.7914261	-.39265847E-01	15.88532346	81.21466489	.41540E+01	.86853E+01	.17831E+03	2.49-15.71
.36676462E+01	-.26286613E-11	4.8046705	-.38411218E-01	15.89205878	90.00000000	.39744E+01	.83623E+01	.17168E+03	0.00-15.89

FIELD POINTS									
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	-----PSI, DEG-----	-----CP-----	-----P/P0-----	-----P/P10-----	OUTWASH P/WASH
-.29643692E+01	-.30531226E-11	3.4676731	-.66153414E-01	10.38914212	-90.00000000	.30488E+00	.57406E+02	.11785E+02	0.00-10.39
-.28074897E+01	.99632412E+00	3.5387749	-.68223333E-01	10.69535899	-57.61186436	.28963E+00	.54566E+02	.11202E+02	5.74-10.06
-.23592482E+01	.18918605E+01	3.7462549	-.74353523E-01	11.42695616	-28.40539119	.24940E+00	.47142E+02	.96782E+03	10.05-10.56
-.16827858E+01	.28153619E+01	4.0626961	-.83371782E-01	12.29412941	-4.71762280	.19833E+00	.37675E+02	.77347E+03	12.25-11.03
-.84401730E+00	.31198113E+01	4.4283853	-.93201451E-01	13.15945414	14.54956285	.15105E+00	.29112E+02	.59767E+03	12.75-11.36
.85120067E+00	.33870576E+01	4.7892901	-.10182513E+00	13.91496331	29.50004859	.11657E+00	.22567E+02	.46331E+03	12.17-11.96
.13200957E+01	.34111311E+01	5.1534052	-.10682459E+00	15.01268720	45.12096764	.86903E+01	.17078E+02	.35011E+03	10.72-10.76
.24778846E+01	.30067362E+01	5.2411190	-.10911270E+00	16.06062072	58.00600394	.69471E+01	.13344E+02	.28421E+03	8.47-13.72
.34292431E+01	.22408891E+01	5.5996477	-.10931398E+00	16.85557265	69.22673671	.59466E+01	.11998E+02	.24532E+03	6.13-15.82
.46583499E+01	.11974472E+01	5.6948031	-.10836608E+00	17.15785299	79.74702311	.54119E+01	.11013E+02	.22609E+03	3.18-17.10
.42785396E+01	-.27498636E-11	5.7272777	-.10787998E+00	17.53171628	90.00000000	.52447E+01	.10703E+02	.21974E+03	0.00-17.54

SHOCK POINTS									
-----Z-----	-----X-----	MACH NO.	-----PT/PT0-----	THETA, DEG	-----PSI, DEG-----	-----CP-----	-----P/P0-----	-----P/P10-----	OUTWASH P/WASH
-.32198064E+01	-.30335538E-11	3.6656068	-.73601792E-01	8.17885552	-90.00000000	.27019E+00	.51025E+02	.10475E+02	0.00-8.18
-.30517155E+01	.10849104E+01	3.7549150	-.77864495E-01	8.71986197	-53.45597205	.25892E+00	.48903E+02	.10040E+02	5.22-7.07
-.25707418E+01	.20647208E+01	4.0125050	-.91111805E-01	9.98197571	-23.38978402	.22913E+00	.43392E+02	.80948E+03	9.18-11.00
-.18439688E+01	.28677876E+01	4.3998031	-.11371193E+00	11.46968586	-22.945551	.19204E+00	.36530E+02	.74995E+03	11.47-11.05
-.93729636E+00	.34452250E+01	4.8271494	-.14249609E+00	12.99360365	17.26918725	.15945E+00	.30500E+02	.62616E+03	12.43-11.92
.73534036E+01	.37766042E+01	5.2317484	-.17351619E+00	14.30242924	30.20142917	.13449E+00	.25920E+02	.53213E+03	12.43-11.92
.14485214E+01	.38634369E+01	5.6409601	-.20858389E+00	16.13727865	44.30570715	.11406E+00	.22140E+02	.45453E+03	11.70-11.43
.28362590E+01	.34402283E+01	5.9546958	-.23796598E+00	17.80305172	57.04705689	.10107E+00	.19699E+02	.40442E+03	9.91-15.08
.39578864E+01	.25830551E+01	6.1511881	-.25738007E+00	19.03689716	68.30124844	.93721E+01	.18340E+02	.37651E+03	7.27-17.77
.47057545E+01	.13865234E+01	6.2708393	-.26959763E+00	19.90133052	79.20398652	.89500E+01	.17568E+02	.30665E+03	3.64-19.48
.49686030E+01	-.24067052E-11	6.3103563	-.27369523E+00	20.06426459	90.00000000	.88219E+01	.17322E+02	.35561E+03	0.00-20.04

TO USE AS IVS. PUNCH THE 3 CARDS. PLACE BEFORE BODY PT CARDS

47 5 0 0 0 0 0 0 11
0. 10000000E+01 0. 10000000E+01
.1965036E+00 -.10000000E+00 .64024979E+01

DATA POINTS WILL BE RE-SPACED FOR SURFACE 48

FIGURE 18. DATA SURFACE WHERE CFL CONDITION IS VIOLATED

[illegible]

FIGURE 19. DATA SURFACE WITH UNDEFINED FLOW ANGLES

DATA SURFACE NO. 5

***TO USE THIS AS AN INITIAL VALUE SURFACE, KEY PUNCH FIRST 6 COLUMNS OF DATA AS INPUT CARDS

SURFACE NO. 5, STATION Y = 8.07101645E-01

BODY POINTS

---Z---	---X---	---Y---	MACH NO.	---PT/PT0---	THETA, DEG	---PSI/DEG---	---CD---	---P/P0---	---P/PT0---	OUTWASHUPWASH
-9.81228551E-01	-1.84653521E-12	1.76642132	3.68284000E-03	11.11905779	-90.00000000	3.79277E-01	2.56679E-01	7.87376E-04	0.00-11.12	
-9.45324351E-01	2.66629438E-01	1.6554499	3.68284000E-03	12.51305080	-54.54695474	3.78250E-01	2.54016E-01	7.85327E-04	7.34-10.25	
-8.40328774E-01	5.13212298E-01	1.6769635	3.68284000E-03	15.77939305	-27.66582158	3.71703E-01	2.49851E-01	7.72449E-04	14.05-7.47	
-6.74253379E-01	7.22161737E-01	1.7063047	3.68284000E-03	19.46817102	-7.33251556	3.55049E-01	2.39050E-01	7.39055E-04	19.32-2.58	
-4.59402261E-01	8.7811732E-01	1.7608553	3.68284000E-03	22.60173159	10.01947099	3.25642E-01	2.20078E-01	6.80402E-04	22.29 4.14	
-2.13582269E-01	9.7016844E-01	1.8504238	3.68284000E-03	24.56732191	26.13547407	2.81955E-01	1.91895E-01	5.93269E-04	22.31 11.39	
4.5304553E-02	9.92932165E-01	1.9736738	3.68284000E-03	25.00873945	41.47269503	2.30347E-01	1.58602E-01	4.90339E-04	19.27 17.17	
2.97373639E-01	9.47233109E-01	2.1208852	3.68284000E-03	23.84907867	55.84664083	1.79978E-01	1.26081E-01	3.89798E-04	13.94 20.09	
5.26269663E-01	8.38919909E-01	2.2722014	3.68284000E-03	21.64987910	69.46770317	1.38735E-01	9.95009E-02	3.07621E-04	7.45 20.22	
7.18143931E-01	6.7320142E-01	2.4220444	3.68284000E-03	18.37633264	81.92463865	1.05467E-01	7.87037E-02	2.43323E-04	2.67 18.21	
8.62124735E-01	4.74641263E-01	2.5658646	3.68284000E-03	15.04289334	91.10298432	8.20619E-02	6.29398E-02	1.94587E-04	-1.30 15.04	
9.51114521E-01	2.44355448E-01	2.6554507	3.68284000E-03	12.24551017	93.84459345	6.95549E-02	5.48738E-02	1.69650E-04	-8.3 12.22	
9.81228551E-01	-2.1279417E-12	2.6824162	3.68284000E-03	11.11905779	90.00000000	6.59822E-02	5.25664E-02	1.62516E-04	0.00 11.12	

FIELD POINTS

---Z---	---X---	---Y---	MACH NO.	---PT/PT0---	THETA, DEG	---PSI/DEG---	---CD---	---P/P0---	---P/PT0---	OUTWASHUPWASH
-1.07775920E+00	-2.0473142E-12	1.7354584	5.04201119E-03	14.98094923	-90.00000000	4.69746E-01	3.13055E-01	9.67855E-04	0.00-17.08	
-1.23372179E+00	2.96479622E-01	1.7485827	5.07835754E-03	15.12438295	-57.23524886	4.63749E-01	3.09187E-01	9.55893E-04	8.32-12.80	
-9.24852294E-01	5.72200721E-01	1.7854764	5.16255436E-03	17.66249977	-30.00269585	4.44816E-01	2.96959E-01	9.18091E-04	15.42-9.05	
-7.44859700E-01	8.08311127E-01	1.8448233	5.24814465E-03	20.00204889	-8.56076772	4.12046E-01	2.75819E-01	8.52733E-04	20.39-3.20	
-5.11972144E-01	9.89391544E-01	1.9272160	5.36487336E-03	23.17282960	9.00343455	3.69348E-01	2.48300E-01	7.67653E-04	22.92 3.30	
-2.64265270E-01	1.18479291E+00	2.0270994	5.46343346E-03	25.04236698	24.12141110	3.20135E-01	2.16525E-01	6.69418E-04	23.09 10.81	
4.76865102E-02	1.18478490E+00	2.1335066	5.53707371E-03	26.17490998	37.32110469	2.71517E-01	1.85161E-01	5.72450E-04	21.35 16.59	
3.54079956E-01	1.11762675E+00	2.2527419	5.62521652E-03	28.42663003	49.44057901	2.27346E-01	1.56667E-01	4.84359E-04	18.20 21.02	
6.2944404E-01	1.00707155E+00	2.3584133	5.68871105E-03	27.07912372	59.74141471	1.92719E-01	1.34327E-01	4.15289E-04	14.45 23.83	
8.01724014E-01	8.25354193E-01	2.4671812	5.73190943E-03	27.04237170	68.83888321	1.67131E-01	1.17813E-01	3.64236E-04	10.53 25.43	
1.04321043E+00	5.85522132E-01	2.5147040	5.77306744E-03	26.85368789	76.43722245	1.50078E-01	1.06818E-01	3.30243E-04	6.77 26.21	
1.20408941E+00	3.03494545E-01	2.5549273	5.74715621E-03	26.72997615	83.41741731	1.40701E-01	1.00769E-01	3.11542E-04	3.30 26.58	
1.2454303E+00	-2.71251019E-12	2.5681889	5.80436809E-03	26.88878839	90.00000000	1.37712E-01	9.88407E-02	3.05580E-04	0.00 26.69	

FIELD POINTS

---Z---	---X---	---Y---	MACH NO.	---PT/PT0---	THETA, DEG	---PSI/DEG---	---CD---	---P/P0---	---P/PT0---	OUTWASHUPWASH
-1.17201951E+00	-2.4809419E-12	1.7247629	8.21024410E-03	15.74755014	-90.00000000	5.75743E-01	3.18143E-01	1.17926E-03	0.00-15.75	
-1.13000869E+00	3.28437204E-01	1.7653135	8.33494379E-03	16.45910707	-58.52985004	5.65936E-01	3.75097E-01	1.15966E-03	8.88-14.32	
-1.00742337E+00	6.2979746E-01	2.0272222	8.67943557E-03	18.94546681	-31.75801510	5.38645E-01	3.57503E-01	1.10527E-03	16.27-10.24	
-8.1350974E-01	8.42286972E-01	2.0904024	9.22261093E-03	21.70605331	-10.35407765	4.97703E-01	3.11363E-01	1.02375E-03	21.38-4.09	
-5.62301697E-01	1.09787115E+00	2.1976071	9.49025786E-03	24.35180453	6.84129057	4.49906E-01	2.60301E-01	9.28426E-04	24.20 3.09	
-2.70364390E-01	1.23573360E+00	2.3143923	1.06585717E-02	26.62142609	21.08871630	4.02340E-01	2.69571E-01	8.33415E-04	25.06 10.22	
4.04537223E-02	1.29938606E+00	2.4339490	1.15015489E-02	28.50563041	33.34984867	3.58643E-01	2.41368E-01	7.46222E-04	24.40 16.62	
4.8718531E-01	1.24066443E+00	2.5616372	1.24420884E-02	30.08446015	45.12792737	3.17342E-01	2.14724E-01	6.63848E-04	22.23 22.32	
7.53422080E-01	1.16575645E+00	2.6724042	1.33265093E-02	31.31154551	55.56728029	2.83979E-01	1.93168E-01	5.97200E-04	18.98 26.64	
1.05427399E+00	9.63156775E-01	2.7642736	1.41517593E-02	32.18607432	64.95987270	2.58524E-01	1.76779E-01	5.46536E-04	14.92 29.69	
1.28819841E+00	6.87057471E-01	2.8354245	1.46941115E-02	32.75701932	73.65148231	2.41678E-01	1.65879E-01	5.12839E-04	10.27 31.69	
1.43495126E+00	3.57651372E-01	2.8740054	1.50288385E-02	33.08659402	81.92146836	2.32473E-01	1.59947E-01	4.96499E-04	5.23 32.83	
1.48801870E+00	-3.10944824E-12	2.8878993	1.51626742E-02	33.19655424	90.00000000	2.29575E-01	1.58103E-01	4.88798E-04	0.00 33.20	

SHOCK POINTS

---Z---	---X---	---Y---	MACH NO.	---PT/PT0---	THETA, DEG	---PSI/DEG---	---CD---	---P/P0---	---P/PT0---	OUTWASHUPWASH
-1.29916536E+00	-2.4489149E-12	2.0167733	2.14998062E-02	17.58265787	-90.00000000	7.33531E-01	4.83248E-01	1.44033E-03	0.00-17.58	
-1.25290101E+00	3.60222346E-01	2.4290929	2.25662477E-02	18.08226563	-65.77963588	7.23307E-01	4.76671E-01	1.47370E-03	7.63-16.58	
-1.12044986E+00	6.4984545E-01	2.5061201	2.46594203E-02	19.48770403	-31.30385732	6.95643E-01	4.58867E-01	1.41800E-03	14.44-13.64	
-9.10158024E-01	9.49445515E-01	2.6251144	2.71145894E-02	21.51788959	-23.47853244	6.54349E-01	4.32133E-01	1.33640E-03	19.88-8.93	
-6.76201933E-01	1.22775314E+00	2.7693005	3.02188664E-02	23.41007501	-6.35850576	6.07732E-01	4.02053E-01	1.24300E-03	23.78-2.81	
-3.15697752E-01	1.39164465E+00	2.9542312	3.48251254E-02	26.26071426	8.82776383	5.53044E-01	3.66780E-01	1.13395E-03	25.99 4.33	
5.00904083E-02	1.49296713E+00	3.1040884	4.53607805E-02	31.79524331	32.05439748	5.10600E-01	3.39431E-01	1.04940E-03	27.72 18.21	
8.41531596E-01	1.47166220E+00	3.2349884	5.13115494E-02	31.59276518	34.96642904	4.78804E-01	3.18921E-01	9.85988E-04	26.75 19.42	
8.70425496E-01	1.35071047E+00	3.4183113	5.11504906E-02	33.54841365	47.20611176	4.36187E-01	2.91393E-01	9.00882E-04	26.25 25.05	
1.23070682E+00	1.12335796E+00	3.5473210	6.49780677E-02	35.27317695	58.55689115	4.08541E-01	2.73585E-01	8.45743E-04	20.25 31.11	
1.51322570E+00	8.05204630E-01	3.6451097	7.94440953E-02	36.50742274	69.33182359	3.88802E-01	2.60824E-01	8.06373E-04	14.64 34.70	
1.69398685E+00	4.20409471E-01	3.7042376	7.95871117E-02	37.25843303	79.74367297	3.77349E-01	2.53435E-01	7.83530E-04	7.71 36.81	
1.75042758E+00	-3.49446749E-12	3.7239540	8.10087962E-02	37.51140104	90.00000000	3.73608E-01	2.51022E-01	7.76068E-04	0.00 37.51	

TO USE AS IVS, PUNCH THESE CARDS, PLACE BEFORE BODY PT CARDS

5 4 0 0 0 0 0 0 13
C. 1.00000000E+00 0. 1.00000000E+00
4.0049605E-02 5.00000000E-02 8.07101645E-01

SURFACE NO. 6, STATION Y = 8.49219854E-01 LOWER CENTERLINE CP = 3.38154772E-01 UPPER CENTERLINE CP = 5.83298728E-02

SURFACE NO. 7, STATION Y = 8.93391473E-01 LOWER CENTERLINE CP = 3.00044858E-01 UPPER CENTERLINE CP = 5.12612274E-02

SURFACE NO. 8, STATION Y = 9.39771673E-01 LOWER CENTERLINE CP = 2.64572959E-01 UPPER CENTERLINE CP = 4.47370131E-02

SURFACE NO. 9, STATION Y = 9.89470883E-01 LOWER CENTERLINE CP = 2.31830062E-01 UPPER CENTERLINE CP = 3.87227024E-02

FIGURE 20. SPECIAL OPTION PRINT

SECTION V

OPERATIONAL ASPECTS

1. CORE AND TIME REQUIREMENTS

The program requires a core size of 60,000, to compile, 1000,000, to load, and 61,300, to execute, all on the CDC 6600 computer.

The program requires approximately 30 seconds of Central Processor Unit (CPU) time to compile on the FTN compiler, using $OPT = 1$. A typical run will require approximately 10 minutes of CPU time for the fuselage of Phase I and one hour for the wing-body of Phase II. There is practically no difference in the execution times generated by the $OPT = 1$ and $OPT = 2$ compiler options. Therefore, $OPT = 1$ is recommended because of its somewhat faster compilation.

2. START OPTIONS

a. Normal Start

Provisions have been made to run both the Initial Value Surface Program and the Three-Dimensional Method of Characteristics Program in one pass. This is done by combining the control cards; putting the Initial Value Surface Program and data before the Three-Dimensional Method of Characteristics Program and data, and setting $ISTART = 0$ and $IFT = 1$.

During execution the 3DMoC program will automatically read the initial value surface from disc file TAPE4 where it was placed by the IVS program. It is also possible to run the IVS program and the 3DMoC program separately, using a physical tape to transfer the IVS information. In this case the IVS data on TAPE4 are recorded on a physical tape through a COPYCF card in the Initial Value Surface Program at the end of the computation. In the Three-Dimensional Method of Characteristics Program, set $IFT = 1$ and $ISTART = 0$ and transfer the IVS data from the physical tape to disc file TAPE4 through a COPYCF card before computation begins. The physical tape (TAPE1) on which all data surfaces will be written, can double up for the job of transferring the IVS data.

b. Restart

Normal output can either be written on a physical tape (TAPE1) or be printed out. When a restart is made from the Nth data surface on the tape, set $ISTART = N$. Be sure that $ISTART \neq 0$, otherwise the data stored on the tape will be ruined.

When the normal output is printed out, a restart can be made by one of the following methods. When the output control KP4 is set to zero, every 10th data surface will be written on TAPE1, which can then be used for a restart by setting $ISTART = m(10)$. A restart can be made from any completed data surface by key-punching the data cards from the listing and making a restart from cards with $ISTART$ set equal to any negative integer. In key-punching the data, ignore any line with literal information; simply key-punch the first six columns of data and stack the last four cards first, as described in Section III. During restart, the number of data rings per data surface can be increased. Set $INCRS = K$ for restarting from cards or set $IFT = -K$ for restarting from tape. The number of data rings N will be increased to $N+K$. It is recommended to limit K to 2 or less.

3. DEFAULT PRINT

A printout option is built into the program to print intermediate results at a particular point, along a particular data ring or on a particular data surface at the lower level $KPRINT = 1$ or at the higher level $KPRINT = 2$. This may be done for check-out purposes when other means have failed to reveal a source of computational trouble. Level 2 gives extensive default print, while level 1 gives a moderate amount of default print. As a rule, up to level 2 is used at a data point, while level 1 is used along a data ring. Otherwise, the amount of printout obtained could be extensive.

In case a failure occurs during a restart from a physical tape, it is useful to keep track of the data that are stored on the tape. For this purpose, $KPRINT(3)$ can be set equal to 3 to print out the first 40 columns of the stored data as they are read in during the restart. Other intermediate results will be printed out at the higher level 2 at point NP, along ring NL, on data surface NS when $KPRINT(3)$ is set to 3.

4. ERROR MESSAGES

If the program runs all the way, it is a fairly good assumption that the results are good. Usually, if something goes wrong, the computation will stop sooner or later with an error message. Default print can be obtained, if necessary, to assist in locating the source of the error. In the case that the normal output is on TAPE1, and the computation stops at a data surface which is not printed out, it will be necessary to restart from the previous data surface and set KP4 = 1 to have the partial data surface printed out. This will locate the troublesome data point and detailed default print may then be obtained for that point.

Error messages, unusual stops and other program messages are summarized below. They are grouped according to the program or subroutine in which they are generated.

Program FUSLAG

ILLNATURED PSI AND DELTA CASE NO __, ROTATE COORDINATES AND RECOMPUTE SURFACE

Whenever the local velocity is aligned with the Y-axis, the angles ψ and δ are undefined. When this happens, the coordinate system is rotated around the Z-axis through an angle of 0.1 radian. The above message is printed out (for the Ith such occurrence) and the Nth data surface is recomputed.

DATA POINTS WILL BE RE-SPACED FOR SURFACE __

This message will appear when (1) the distribution of data points along a body ring becomes noticeably uneven, (2) a data ring is automatically added by the program, (3) a data point computation violates the CFL stability condition

WRONG IVS NO __, NO __ SPECIFIED OR FAIL END FILE

When a restart is made from TAPE1, this message indicates either the program is unable to locate and read from the specified data surface or the arrangement of data on TAPE1 is unusual so that an END OF FILE was encountered. If this happens, the contents of TAPE1 should be printed out. Alternatively, when KPRINT(3) is set to 3, the first 40 columns of each line information on TAPE1 will be printed out as the program FUSLAG is reading TAPE1.

Subroutine BULK

BULK POINT HAS FAILED TO CONVERGE AFTER 25 ITERATIONS

Computation is stopped.

This happens very rarely. A decrease in the magnitude of the convergence criteria may remedy the problem.

Subroutine BASEPT

BASE POINT ____ VIOLATES CFL

This advisory message appears whenever the CFL stability condition is violated at basepoint I. The number following the message is the factor L (see the discussion on basepoint location in Volume I).

INTERSECTION FAILURE, BASEPOINT NO ____

Computation is stopped.

This message indicates that the Mach conoid fails to properly intersect the line joining basepoint I to the center data point. The first three numbers following the message are coefficients A, B, C, of the quadratic equation (see discussion of basepoint location in Volume I) and the last number is $\sqrt{B^2 - AC}$. When this happens at the juncture point of two body sections check the continuity of the body description. If the body description is new, check FIGURE, paying attention to the formula and coding of the body normal. In high gradient areas, this message usually means more data points are required.

MACH CONE CONVERGENCE FAILURE IN BASEPOINT NO ____

Computation is stopped.

This seldom happens. A relaxing of the convergence criterion on Mach angle (increase in the value of EPSLN) helps.

BASE PT ____ EXTRAPOLATES, STEP DECREASED

The number following this message is the factor L (see discussion on basepoint location in Volume I). If this message appears in a series prior to an abnormal termination, an increase in the number of data rings (and in some cases, in the number of data points) may help.

Subroutine COMPAT

CONVERGENCE FAILURE IN COMPAT

Computation is stopped.

This has never happened. If it should occur, try to increase the number of iterations by modifying the source deck. If it should persist, obtain default print for analysis of the problem.

Subroutine GMTRY

CONVERGENCE FAILURE IN GMTRY

Computation is stopped.

Check the body description and subroutine FIGURE.

Subroutine FIGURE

***** YOU HAVE GONE ALL THE WAY--FEELING NICE, I BET *****

This message indicates that the goal has been accomplished

SECTION VI

LOGICAL STRUCTURE

1. INTERDEPENDENCE OF SUBROUTINES

The Calling-Called matrix for the program is shown in Figure 21.

2. LISTINGS

Two complete listings of the Three-Dimensional Method of Characteristics Program are given below, following Figure 21. The first listing is for the computer program developed in Phase I for the calculation of flow fields over a fuselage and canopy configuration. The second listing is for the computer program developed in Phase II for the calculation of flow fields about a fuselage-canopy-wing configuration.

Calling \ Called																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
	FUSLAG	BULK	PICK	BASEPT	COEFS	GMTRY	TRANS	HARNES	TIDYUP	REFORM	FIGURE	CONPIC	CONPIC	FIGURE	REFORM	TIDYUP	HARNES	TRANS	GMTRY	COEFS	BASEPT	COEFS	GMTRY	TRANS	HARNES	TIDYUP	REFORM	KURFTT	KURVE	ROTXY	CONICF	CUBIC	ELIPSE	WINGF	PCRCL	PELIPS	CONPIC	XSUBG	AERO	SETCP	SECOND																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
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FIGURE 21. CALLING-CALLED MATRIX FOR 3DMoC PROGRAM

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*DECK A
PROGRAM FUSLAG(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,PUNCH,TAPE7=
1      PUNCH,TAPE2,TAPF1,TAPE4)
C **** FUSELAGE + CANOPY (PHASE-I CONTRACT)
COMMON /TEST/ LOT(4),ITEST,STEP,KTEST,KPRINT(3)
COMMON /GEOM/ YMAX,YSTOP,INDEX
COMMON /MESH/ K1,K2
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHETA,DPSI,KP4,IOU3
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE,ISURF,Y0,ISTART
COMMON /SENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
1PS,HUB(8)
COMMON /BSPT/ XBS(4),YBS(4),ZBS(4),URS(4),VBS(4),WBS(4),PBS(4),
1PPMBS(4),THBS(4),PSBS(4)
COMMON /STOR/ H(4,8),A(50,8,4)
COMMON /CP/B(50,4,2),DRAG,ALIFT,TORQUE,YMT,ZMT,WINGA
DIMENSION YSET(10),NPSET(30),LIT(18),DUM(10)
C IN A(I,J,K) J=1,8 CORRESPOND TO X,Y,Z,U,V,W,P,PT, K=1,4 CORRESPOND
C TO A(AQUIRE), L(LOWER CLASS), M(MIDDLE CLASS), U(UPPER CLASS)
CALL FTNBIN (1,0,DUM)
IOU5=5
IOU6=6
IOU7=7
IOU3=1
IOU=IOU5
LTAPE=4
NTAPE=2
REWIND LTAPE
REWIND NTAPE
LN=LTAPE+NTAPE
READ (IOU5,52) (LIT(I),I=1,18)
READ (IOU5,55) DP,DTHETA,DPSI,EPSLN,DYC,YSTOP,STEPM
READ (IOU5,56) NSURF,LINE,NPC,NR,IFT,ISTART,KP4,NS,NL,NP,KPRINT
IOU1=IOU3
IF (KP4.LT.0) IOU1=IOU6
KAB=IABS(KP4)
IF (KP4.EQ.0) KAB=10
DO 1 I=1,NR
1 READ (IOU5,53) YSET(I),NPSET(3*I-2),NPSET(3*I-1),NPSET(3*I)
READ (IOU5,55) FMSTR,GF(1),ALFA,Y0
READ (IOU5,55) YA,ZA,SCALE,WINGA
WRITE (IOU6,54) (LIT(I),I=1,18)
WRITE (IOU6,55) DP,DTHETA,DPSI,EPSLN,DYC,YSTOP,STEPM

```

```

A 1
A 2
H0030
A 5
A 6
A 7
A 8
A 9
A 10
A 11
A 12
A 13
A 14
A 15
A 16
A 17
A 18
A 19
A 20
A 21
A 22
A 23
A 24
A 25
A 26
A 27
A 28
A 30
A 31
A 32
A 33
A 34
A 35
A 36
A 37
A 38
A 39

```

```

105 WRITE(1006,56) NSURF,LINE,NPC,NR,IFT,ISTART,KP4,NS,NL,NP,KPRINT
DO 105 I=1,NR
WRITE(1006,53) YSET(I),NPSET(3*I-2),NPSET(3*I-1),NPSET(3*I)
WRITE(1006,55) FMSTR,GF(1),ALFA,YO
WRITE(1006,55) YA,ZA,SCALE,WINGA
WINGA=WINGA*144.0
STEP=0.
MESS=1
INCR=0
GF(2)=.5*(GF(1)-1.)
GF(3)=.5*(GF(1)+1.)
GF(4)=GF(2)/GF(3)
GF(5)=1./GF(1)-1.
GF(6)=GF(1)*GF(5)
GF(7)=1./GF(6)
GFM2=GF(2)*FMSTR*FMSTR
QINF=SQRT(GFM2/(1.+GFM2))
POP=(1.+GFM2)**GF(6)
RAD=57.295779513082
COSA=COS(ALFA/RAD)
SINA=SIN(ALFA/RAD)
ISURF=1
ILL=0
KURE=0
K1=0
K2=0
SINE=0.
COSINE=1.
S2=0.
C2=1.
SN=SIN(.1)
CS=COS(.1)
YMAX=-1.E7
C ISTART,LT,0,RESTART FROM CARDS,ISTART=1,GT,0,RESTART FROM ITH SURFACE
IF (ISTART.NE.0.OR.IFT.NE.1) GO TO 2
IOU=LTAPE
REWIND IOU3
READ (IOU,55) FMSTR,GF(1),ALFA,YI,DRAG $ YO=(YI-1.0)*SCALE+YA
DRAG = DRAG*3.1415927*SCALE**2/WINGA
IF (ISTART.EQ.0) REWIND IOU3
IF (ISTART.NE.0.OR.KP4.LE.0) GO TO 3
WRITE (IOU3,68) (LIT(I),I=1,18),FMSTR,GF(1),ALFA
WRITE (IOU3,62) ISURF,LINE,ILL,KURE,MESS,INCR,K1,K2,NPC

```



```

3      WRITE (IOU3,66) SINE,COSINE,S2,C2,DYC,STEP,Y0,DRAG,ALIFT,TORQUE
4      IF (ISTART) 8,9,4
      DO 6 I=1,ISTART
      READ (IOU3,52) DUM
      IF (KPRINT(3).EQ.3) WRITE (IOU6,52) DUM
      READ (IOU3,65) ISURF,LINE,ILL,KURE,MESS,INCRES,K1,K2,NPC
      IF (KPRINT(3).NE.0) WRITE (IOU6,56) ISURF,LINE,K1,K2,NPC
      READ (IOU3,66) SINE,COSINE,S2,C2,DYC,STEP,Y0,DRAG,ALIFT,TORQUE
      READ (IOU3,52) DUM
      IF (IFT.LT.0) INCRES=-IFT
      IF (IFT.GT.1) INCRES=1-IFT
      IF (ISURF.EQ.ISTART) GO TO 9
      KOUNT=LINE*(NPC+2)+100
      DO 5 J=1,KOUNT
      READ (IOU3,52) DUM
      IF (KPRINT(3).EQ.3) WRITE (IOU6,52) DUM
      IF (EOF(IOU3)) 6,5
5      CONTINUE
6      CONTINUE
7      WRITE (IOU6,64) ISURF,ISTART
      CALL EXIT
8      READ (IOU5,56) ISURF,LINE,ILL,KURE,MESS,INCRES,K1,K2,NPC
9      READ (IOU5,57) SINE,COSINE,S2,C2,DYC,STEP,Y0,DRAG,ALIFT,TORQUE
      N1=ISURF+1
      N2=NPC+1
      N3=NPC+3
      WRITE (IOU6,58) FMSTR,GF(1),ALFA,DRAG,ALIFT,TORQUE
      DO 13 I=1,LINE
      IF (ISTART.GT.0) READ (IOU3,52) DUM
      IND=2
      IF (I.EQ.1) IND=1
      IF (I.EQ.LINE) IND=3
      IF (ISTART.GT.0) READ (IOU3,52) DUM
      DO 12 J=2,N2
      IF (ISTART.LE.0) READ (IOU,59) A(J,3),A(J,1),A(J,7),A(J,8),THETA,
1PSI
      IF (ISTART.GT.0) READ (IOU3,67) A(J,3),A(J,1),A(J,7),A(J,8),THETA,
1PSI
      THETA=THETA/RAD
      PSI=PSI/RAD
      A(J,7)=A(J,8)/(1.+GF(2)*A(J,7)**2)**GF(6)
      IF (ISTART.NE.0) GO TO 10
      A(J,1)=A(J,1)*SCALE

```

```

10      A(J,3)=A(J,3)*SCALE+ZA
        A(J,2)=Y0
        Q=SQRT(1.-(A(J,7)/A(J,8))*GF(7))
        QS=Q*SIN(THETA)
        A(J,4)=QS*CO5(P5I)
        A(J,5)=Q*CO5(THETA)
        A(J,6)=QS*SIN(P5I)
        DO 11 K=1,4,3
          CALL ROTATE (A(J,K),A(J,K+1),SINE,COSINE)
          CALL DATOUT (A,J,IND,KAB,0)
          CALL DATOUT (A,J,IND,KAB,1)
          WRITE (NTAPE) ((A(J,L),L=1,8),J=2,N2)
          IF (ISTART.EQ.0.AND.KP4.GT.0) END FILE IOU3
          IF (ISTART.LE.0) GO TO 14
          READ (IOU3,52) DUM
          IF (EOF(IOU3)) 14,7
          DO 51 I=N1,NSURF
            ITEST=0
            KTEST=0
            ISURF=I
            NLINE=LINE+INCRES
            DYC=(DYC+DYC*STEP)*FLOAT(LINE)/FLOAT(NLINE)
            IF (STEP.LT.0.00) MESS=1
            STEP=.05
            IPRINT=0
            DO 16 K=1,NR
              NPCC=NPSET(3*(K-1)+1)
              L1=NPSET(3*(K-1)+2)
              L2=NPSET(3*(K-1)+3)
              IF (Y0+DYC.LT.YSET(K).OR.NPSET(3*K+1).EQ.0) GO TO 17
              CONTINUE
              IF (NPC.EQ.NPCC.AND.(L1.EQ.K1.AND.L2.EQ.K2)) GO TO 18
              DYC=DYC*FLOAT(NPC-1-(K2-K1)/2)/FLOAT(NPCC-1-(L2-L1)/2)
              K1=L1
              K2=L2
              MESS=1
            REWIND LTAPE
            REWIND NTAPE
            IF ((Y0+DYC.LE.YSTOP).OR.(ABS(YSTOP-Y0).LT.0.0002)) GO TO 181
            DYC=YSTOP-Y0
            KP4=-10000
181      IF (ITEST.EQ.KTEST) GO TO 19
            IF (ITEST.GT.10) CALL EXIT

```

A 118
 A 119
 A 120
 A 121
 A 122
 A 123
 A 124
 A 125
 A 126
 A 127
 A 128
 A 129
 A 130
 A 131
 A 132
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 A 134
 A 135
 A 136
 A 137
 A 138
 A 139
 A 140
 A 141
 A142
 A 143
 A 144
 A 145
 A 146
 A147
 A 148
 A 149
 A 150
 A 151
 A 152
 A 153
 A 154
 A 155

A 157

```

19 KTEST=ITEST
   GO TO 26
   LTAPE=LN-LTAPE
   NTAPE=LN-NTAPE
   IF (MESS.EQ.0.AND.INCRES.EQ.0) GO TO 21
   DO 20 K=1,LINE
   READ (LTAPE) ((A(L,M),M=1,8),L=1,NPC)
   IF (K.EQ.1) AM=.5*(A(1,3)+A(NPC,3))
   CALL TIUYUP (SINE,COSINE,A,NPC,NPCC,AM)
   WRITE (NTAPE) ((A(L,M,2),M=1,8),L=1,NPCC)
   WRITE (IOU6,63) I
   NPC=NPCC
   N2=NPC+1
   N3=NPC+3
   CALL REFORM (A,LTAPE,NTAPE,NPC,LINE,NLINE)
   INCRES=0
   MESS=0
   GO TO 18
21 IF (KURE.NE.ILL) 23,26
22 REWIND LTAPE
   REWIND NTAPE
23 WRITE (IOU6,61) ILL,I
   IF (ILL.GT.16) CALL EXIT
   KURE=ILL
   CALL ROTATE (SINE,COSINE,SN,CS)
   S2=2.*SINE*COSINE
   C2=COSINE*COSINE-SINE*SINE
   DO 25 J=1,LINE
   READ (LTAPE) ((A(L,K),K=1,8),L=2,N2)
   DO 24 K=2,N2
   DO 24 L=1,4,3
   CALL ROTATE (A(K,L),A(K,L+1),SN,CS)
24 WRITE (NTAPE) ((A(L,K),K=1,8),L=2,N2)
25 REWIND LTAPE
   REWIND NTAPE
   LTAPE=LN-LTAPE
   NTAPE=LN-NTAPE
26 IF (KP4.LE.1.OR.I/KP4*KP4.EQ.1) WRITE (IOU6,60) I
   CALL SETCP(LTAPE,1,A,B,SINE,COSINE,POP,GF,FMSTR,N2)
   IF (STEPM.NE.0.) DYC=AMINI(DYC,STEPM)
   DO 45 J=1,LINE
   IND=2
   IF (J.EQ.1) IND=1

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A 158
A 159
A 160
A 161
A 162
A 163
A 164
A 165
A 166
A 167
A 168
A 169
A 170
A 171
A 172
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A 174
A 175
A 176
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A 178
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A 182
A 183
A 184
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A 186
A 187
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A 189
A 190
A 191
A 192
A 193
A 194
A 195

A 196
A 197
A 198

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```

27 IF (J.EQ.LTNE) IND=3
28 IF (IND=2) 27,31,34
DO 28 M=3,4
READ (LTAPE) ((A(K,L,M),L=1,8),K=2,N2)
IF (DYC.GT.1.E-6) GO TO 29
UYC=AMIN1(ABS(A(2,3,3)-A(2,3,4)),ABS(A(3,1,3)-A(2,1,3)))
XM2=(1.*(A(2,8,3)/A(2,7,3))*GF(7)-1.)/GF(2)
DYC=DYC*.6*SQRT(XM2-1.)
CALL MIRROR (A(1,1,3),S2,C2,N2)
DO 30 K=2,NPC
IF (.6*((A(K,1,4)-A(K,1,3))*2+(A(K,2,4)-A(K,2,3))*2+(A(K,3,4)-A(
1K,3,3))*2).LT.(A(K,1,3)-A(K,1,1,3))*2+(A(K,2,3)-A(K,1,2,3))*2+(
2A(K,3,3)-A(K,1,3,3))*2) GO TO 33
CONTINUE
INCR=1
GO TO 33
31 DO 32 K=1,N3
DO 32 L=1,8
A(K,L,2)=A(K,L,3)
A(K,L,3)=A(K,L,4)
READ (LTAPE) ((A(L,K,4),K=1,8),L=2,N2)
CALL MIRROR (A(1,1,4),S2,C2,N2)
GO TO 36
34 DO 35 K=3,4
DO 35 L=1,N3
DO 35 M=1,4,3
YTEMP=SINE*A(L,M,K)+COSINE*A(L,M+1,K)
A(L,M,K-1)=COSINE*A(L,M,K)-SINE*A(L,M+1,K)
A(L,M+1,K-1)=COSINE*YTEMP+SINA*A(L,M+2,K)
A(L,M+2,K-1)=-SINA*YTEMP+COSA*A(L,M+2,K)
A(L,M/4+7,K-1)=A(L,M/4+7,K)
DO 38 K=2,N2
IPRINT=0
IF (I.NE.NS) GO TO 37
IPRINT=KPRINT(1)
IF (J.NE.NL) GO TO 37
IPRINT=KPRINT(2)
IF (K.NE.NP+1) GO TO 37
IPRINT=KPRINT(3)
CALL HULK (K,IND)
IF (ITEST.NE.KTEST) GO TO 15
IF (KURE.NE.ILL) GO TO 22
IF (IND.NE.3) CALL DATOUT (A,K,IND,KAB,0)
37

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```

38      CONTINUE
      IF (IND.NE.3) WRITE (NTAPE) ((A(L,K),K=1,8),L=2,N2)
      IF (IND=2) 42,45,39
39      CALL HARNES (QINF,A,NPC)
      DO 41 K=2,4
      N=K
      IF (K.EQ.4) N=1
      DO 41 L=1,N3
      IF (K.EQ.4.AND.(L.EQ.1.OR.L.EQ.N3)) GO TO 41
      DO 40 M=1,4,3
      A(L,M/4+7,K)=A(L,M/4+7,N)
      YTEMP=COSA*A(L,M+1,N)-SINA*A(L,M+2,N)
      A(L,M+2,K)=SINA*A(L,M+1,N)+COSA*A(L,M+2,N)
      A(L,M+1,K)=-SINE*A(L,M,N)+COSINE*YTEMP
      A(L,M,K)=COSINE*A(L,M,N)+SINE*YTEMP
40      CONTINUE
41      GO TO 45
42      LB=2
      IF (K1.NE.0) LB=K1+1
      LE=NPC
      IF (K2.NE.0) LE=K2
      DO 44 L=LB,LE
      ARC=(A(L+1,1)-A(L,1))*2+(A(L+1,2)-A(L,2))*2+(A(L+1,3)-A(L,3))*2
      IF (L.NE.LB) GO TO 43
      BIG=ARC
      SMALL=ARC
43      BIG=AMAX1(BIG,ARC)
44      SMALL=AMIN1(SMALL,ARC)
      IF (2.*SMALL.LE.BIG) MESS=1
45      CONTINUE
      DO 47 J=2,N2
      DO 46 K=1,8
      A(J,K)=A(J,K,4)
46      CALL DATOUT (A,J,3,KAB,0)
47      CONTINUE
      IF (KP4.GT.0.OR.(KP4.EQ.0.AND.I/10*10.EQ.1)) WRITE (IOU3,60) I
      WRITE (NTAPE) ((A(J,L),L=1,8),J=2,N2)
      CALL SETCP(NTAPE,2,A,8,SINE,COSINE,POP,GF,FMSTR,N2)
      CALL AERO (NPC,SINA,COSA)
      REWIND NTAPE
      READ (NTAPE) A(1),A(2)
      Y0=SINE*A(1)+COSINE*A(2)
      IF (KP4.EQ.0.AND.I/10*10.NE.1) GO TO 48
      A 279
      A 280
      A 281
      A 282

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48      WRITE (IOU1,62) I,LINE,ILL,KURE,MESS,INCRES,K1,K2,NPC
        WRITE (IOU1,66) SINE,COSINE,S2,C2,DYC,STEP,Y0,DRAG,ALIFT,TORQUE
        IF (I/KAB*KAB,NE,I,AND,KP4,NE,0) GO TO 49
        IF (KP4,GE,0) WRITE (IOU6,62) I,LINE,ILL,KURE,MESS,INCRES,K1,K2,
INPC
        IF (KP4,LT,0) WRITE (IOU7,56) I,LINE,ILL,KURE,MESS,INCRES,K1,K2,
INPC
        IF (KP4,GE,0) WRITE (IOU6,66) SINE,COSINE,S2,C2,DYC,STEP,Y0
        * ,DRAG,ALIFT,TORQUE
        IF (KP4,LT,0) WRITE (IOU7,57) SINE,COSINE,S2,C2,DYC,STEP,Y0
        * ,DRAG,ALIFT,TORQUE
        IF (KP4,LT,1,AND,I/KAB*KAB,NE,I) GO TO 51
        REWIND NTAPE
        DO 50 J=1,LINE
        READ (NTAPE) ((A(K,L),L=1,8),K=2,N2)
        IND=2
        IF (J,EQ,1) IND=1
        IF (J,EQ,LINE) IND=3
        DO 50 K=2,N2
        CALL DATOUT (A,K,IND,KAB,1)
50      IF (KP4,GT,0,OR,(KP4,EQ,0,AND,I/10*10,EQ,I)) END FILE IOU3
51      CONTINUE
        CALL EXIT
C
52      FORMAT (18A4)
53      FORMAT (F10.5,12I5)
54      FORMAT (1H140X38HNORTHROP SUPERSONIC FLOW FIELD PROGRAM//30X18A4)
55      FORMAT (7F10.5)
56      FORMAT (16I5)
57      FORMAT (4E15.8)
58      FORMAT (1H039X40H 3-DIMENSIONAL CHARACTERISTICS SOLUTION /1H05X,24
1HFRFESTREAM MACH NUMBER =,F7.3,5X25HRATIO OF SPECIFIC HEATS =,F6.3
2,5X17HANGLE OF ATTACK =,F7.3,8H DEGREES/1H049X21HINITIAL VALUE SUR
3FACE,T2,6HDRAG =,G14.7/T2,6HLIFT =,G14.7/T2,8HMOMENT =,G14.7)
59      FORMAT (2E15.8,F10.7,E15.8,F12.8,F13.8)
60      FORMAT (1H150X15HDATA SURFACE NO,I3/93H0**TO USE THIS AS AN INITI
1AL VALUE SURFACE, KEY PUNCH FIRST 6 COLUMNS OF DATA AS INPUT CARDS
2)
61      FORMAT (33H0ILLNATURED PSI AND DELTA,CASE NO,I3,42H, ROTATE COORDI
INATES AND RECOMPUTE SURFACE,I3)
62      FORMAT (61H0TO USE AS IVS, PUNCH THE 4 CARDS, PLACE BEFORE BODY PT
* CARDS/1X,9(1H0),10(1H1),10(1H2),10(1H3),10(1H4),10(1H5),10(1H6),
* 10(1H7),1H8/1X,8(10H1234567890)//1X,14I5)

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63	FORMAT (42H0DATA POINTS WILL BE RE-SPACED FOR SURFACE,I3)	A 323
64	FORMAT (13H0WRONG IVS NOI4,4H, NOI4,27H SPECIFIED OR FAIL END FILE	A 324
	1)	A 325
65	FORMAT (1X/////1X,14I5)	A 326
66	FORMAT (1X,4E15.8)	A 327
67	FORMAT (1X,2E15.8,F10.7,E15.8,F12.8,F13.8)	A 328
68	FORMAT (1H1,30X18A4,/1H05X24HFREESTREAM MACH NUMBER =F7.3,5X25HRAT	A 329
	110 OF SPECIFIC HEATS =F6.3,5X,17HANGLE OF ATTACK =F7.3,8H DEGREES)	A 330
	END	A 331

```

*DECK B
SUBROUTINE HULK (L,IND)
IND =1 FOR BODY, 2 FOR FIELD, 3 FOR SHOCK
C**** TAKE NOTE THAT SINE,COSINE MUST CORRESPOND TO CURRENT COORDINATES
COMMON /TEST/ LOT(4),ITEST,STEP,KTEST
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DIHETA,DPSI
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE
COMMON /ESENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
1PS,HUB(8)
COMMON /BSPT/ XBS(4),YBS(4),ZBS(4),UBS(4),VBS(4),WBS(4),PBS(4),
1PPMBS(4),THBS(4),PSBS(4)
COMMON /STOR/ H(4,8),XAL(50),YAL(50),ZAL(50),UAL(50),VAL(50),WAL(
150),PAL(50),PPMAL(50)
DIMENSION XYZ(3,7)
EQUIVALENCE (XC,XYZ)
1 IF (IPRINT.GE.1) 2,3
2 IF (IND.EQ.1) WRITE (IOU6,14)
IF (IND.EQ.2) WRITE (IOU6,13)
IF (IND.EQ.3) WRITE (IOU6,15)
N=4-MOD(IND,2)
CALL PICK (L,IND)
3 IF (KURE.NE.ILL) RETURN
C BACK TO MAIN PROGRAM, ROTATE Y AXIS AWAY FROM FLOW FIELD
UC=HUB(4)
VC=HUB(5)
WC=HUB(6)
PC=HUB(7)
PPMC=HUB(8)
THETAC=TH
PSIC=PS
DO 4 I=1,4
LOT(I)=0
DO 11 I=1,25
IF (IPRINT.GE.1) WRITE (IOU6,16) I
IF (IND.NE.3) GO TO 5
Q=SQRT(1.-(PC/PPMC)**GF(7))
CALL NORM (-UC*Q,QINF-VC*Q,-WC*Q,A,B,C)
IF (I.EQ.1) CALL NORM (A,B,C,A1,B1,C1)
CALL NORM (A,A1,B,B1,C,C1,A,B,C)
IF (IPRINT.GE.1) WRITE (IOU6,21) A,B,C,A1,B1,C1
A4=-A*B
B4=1.-B*B

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43      C4=-C*B
44      BM=COSA*B4-SINA*C4
45      AB=(SINA*B4+COSA*C4)/BM
46      XC=HUB(1)+DYC*A4/BM
47      YC=HUB(2)+DYC*(COSA+SINA*AB)
48      ZC=HUB(3)+DYC*(-SINA+COSA*AB)
49      GO TO 6
50
51      A4=UC+HUB(4)
52      B4=VC+HUB(5)
53      C4=WC+HUB(6)
54      BM=SINE*A4+COSINE*B4
55      AB=(COSINE*A4-SINE*B4)/BM
56      XC=HUB(1)+DYC*(SINE+COSINE*AB)
57      YC=HUB(2)+DYC*(COSINE-SINE*AB)
58      ZC=HUB(3)+DYC*C4/BM
59
60      IF (IPRINT,GE.1) WRITE (IOU6,21) A4,B4,C4,BM,AB,XC,YC,ZC
61      IF (IND,NE.1) GO TO 7
62      CALL GMTRY (SINE,COSINE,XC,YC,ZC,A4,B4,C4)
63      IF (IPRINT,GE.1) WRITE (IOU6,21) XC,YC,ZC,A4,B4,C4
64      CALL TRANS (H,XYZ,A4,B4,C4,1,1)
65      CALL BASEPT (IND)
66      IF (ITEST,EQ,KTEST,OR,LOT(4),NE.4) GO TO 75
67      H(4,1) = XA1(L)
68      H(4,2) = YA1(L)
69      H(4,3) = ZA1(L)
70      CALL NORM(UA1(L),VA1(L),WA1(L),H(4,4),H(4,5),H(4,6))
71      H(4,7) = PA1(L)
72      H(4,8) = PPMAL(L)
73      KTEST = ITEST
74      GO TO 7
75
76      IF (KURE,NE,ILL,OR,ITEST,NE,KTEST) RETURN
77      IF (IPRINT,GE.1) WRITE (IOU6,17) (J,XBS(J),YBS(J),ZBS(J),PBS(J),
78      1PPMBS(J),THBS(J),PSBS(J),UBS(J),VBS(J),WBS(J),J=1,N)
79      CALL COEFS (IND)
80      IF (KURE,NE,ILL) RETURN
81      IF (IND,EQ.1) CALL SOL (COF(4),COF(6),COF(5),COF(1),COF(6),COF(9),
82      1COF(8),COF(3),0,0,1,1,5707963267949,PC,PSIC,THETAC)
83      IF (IND,EQ.2) CALL SOL (COF(4),COF(5),COF(6),COF(1),COF(5),COF(7),
84      1COF(8),COF(2),COF(6),COF(8),COF(9),COF(3),PC,THETAC,PSIC)
85      IF (IND,EQ.3) CALL COMPAT
86      SINTH=SIN(THETAC)
87      UC=SINTH*COS(PSIC)
88      VC=COS(THETAC)

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      WC=SINTH*SIN(PASIC)
      IF (IND.EQ.1) CALL TRANS (H,XYZ,A4,B4,C4,-1.,1)
      IF (UC*UC+WC*WC.GE.4.E-06) GO TO 8
      ILL=ILL+1
      RETURN
      IF (IPRINT.GE.1) WRITE (IOU6,18) I,XC,YC,ZC,PC,PPMC,UC,VC,WC,
1 THETAC,PSIC
      IF (L.NE.2.AND.L.NE.NPC+1) GO TO 9
      UT=SINE*UC+COSINE*VC
      IF (IND.NE.3) CALL NORM (SINE*UT,COSINE*UT,WC,UC,VC,WC)
      IF (IND.EQ.3) CALL NORM (0.,VC,WC,UC,VC,WC)
      IF (I.EQ.1) GO TO 10
      IF (ABS(THETAC-TTEMP).GT.DTHETA) GO TO 10
      IF (ABS(PASIC-PSTEMP).GT.DPSI) GO TO 10
      IF (ABS((PC-PTEMP)/PC).LE.DP) GO TO 12
      TTEMP=THETAC
      PSTEMP=PSIC
      PTEMP=PC
      WRITE (IOU6,19)
      CALL EXIT
      LI=L-1
      IF (IPRINT.GE.1) WRITE (IOU6,20) LI
      Q=SQRT(1.-(PC/PPMC)**GF(7))
      XAL(L)=XC
      YAL(L)=YC
      ZAL(L)=ZC
      UAL(L)=Q*UC
      VAL(L)=Q*VC
      WAL(L)=Q*WC
      PAL(L)=PC
      PPMAL(L)=PPMC
      RETURN
      C
      13 FORMAT (18H0***** FIELD *****)
      14 FORMAT (17H0***** BODY *****)
      15 FORMAT (18H0***** SHOCK *****)
      16 FORMAT (1H0,20X,32HBASE POINT PROPERTIES, ITERATION,13)
      17 FORMAT (15H0I,X,Y,Z,P,PPMC=.15,5E18.8/17H THETA,PSI,U,V,W=.3X5E18.8
1)
      18 FORMAT (41H0NEW BULK POINT PROPERTIES, ITERATION NO.,13/1H 21X,2HX
1C,18X,2HVC,18X,2HZC,18X,2HPC,17X,4HPPMC/1H ,10X,5E20.8/1H ,21X,2HU
2C,18X,2HVC,18X,2HWC,16X,6HTHETAC,15X,4HPASIC/1H ,10X,5E20.8)
      19 FORMAT (54H0BULK POINT HAS FAILED TO CONVERGE AFTER 25 ITERATIONS)

```

B 120
B 121
B 122

FORMAT (24H0***** BULK POINT NO..13.23H HAS CONVERGED *****)
FORMAT (8E15.7)
END

20
21

```

*DECK C
SUBROUTINE PICK (L,IND)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSSLN,DP,DTHETA,DPSI
COMMON /ESFNS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
1PS,HUB(8)
COMMON /STOR/ H(4,8),ALMUS(50,8,4)
1 LP=L+1
LM=L-1
N=2
IF (IND.EQ.2) N=4
DO 2 I=1,8
HUB(I)=ALMUS(L,I,3)
IF (IND.NE.3) H(2,I)=ALMUS(L,I,4)
IF (IND.NE.1) H(N,I)=ALMUS(L,I,2)
H(1,I)=ALMUS(LM,I,3)
H(3,I)=ALMUS(LP,I,3)
2 CALL NORM (HUB(4),HUB(5),HUB(6),HUB(4),HUB(5),HUB(6))
IF (HUB(4)**2+HUB(6)**2.GT.4.E-06) GO TO 3
ILL=ILL+1
RETURN
3 TH=ACOS(HUB(5))
PS=ATAN2(HUB(6),HUB(4))
IF (IND.NE.2) N=3
DO 4 I=1,N
4 CALL NORM (H(I,4),H(I,5),H(I,6),H(I,4),H(I,5),H(I,6))
IF (IPRINT.GE.2) WRITE (IOU6,5) HUB,((H(I,J),J=1,8),I=1,N),TH,PS
RETURN
C
5 FORMAT (17H0***** PICK *****/(8E15.7))
END

```



```

*DECK D
SUBROUTINE BASEPT (IND)
COMMON /TEST/ LOT(4),ITEST,STEP,KTEST,KPRINT(3)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTETA,DPSI
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7)
COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE
COMMON /ESENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
1PS,HUH(8)
COMMON /BSPT/ XBS(4),YBS(4),ZBS(4),URS(4),VBS(4),WBS(4),PBS(4),
1PPMBS(4),THBS(4),PSBS(4)
COMMON /STOR/ XH(4),YH(4),ZH(4),UH(4),VH(4),WH(4),PH(4),PPMH(4)
IF (IPRINT.GE.2) WRITE (IOU6,13)
XD=XC-HUB(1)
YD=YC-HUB(2)
ZD=ZC-HUB(3)
B2=XD*XD+YD*YD+ZD*ZD
ROOT = GF(2)/((PPMC/PC)**GF(7)-1.0)
IF (ROOT.GT.0.) GO TO 20
WRITE(IOU6,600) PPMC,PC
CALL EXIT
600 FORMAT(/ / 24H FLOW SUBSONIC, PPMC,PC= ,2G15.7)
20 AMU4=ASIN(SQRT(ROOT))
IF (IPRINT.GE.2) WRITE (IOU6,14) XD,YD,ZD,AMU4
LID=3
IF (IND.EQ.2) LID=4
N = 1
IF (LOT(4).EQ.4) N=4
DO 8 I=N,LID
XD1=XH(I)-HUB(1)
YD1=YH(I)-HUB(2)
ZD1=ZH(I)-HUB(3)
IF (IPRINT.GE.2) WRITE (IOU6,15) I
A2=XD1*XD1+YD1*YD1+ZD1*ZD1
A8=XD*XD1+YD*YD1+ZD*ZD1
IF (IPRINT.GE.2) WRITE (IOU6,14) XD1,YD1,ZD1
DO 5 J=1,50
IF (J.EQ.1) FL=.5
IF (J.EQ.1) GO TO 4
COS2=COS(.5*(AMU0+AMU4))**2
CALL NORM (.5*(URS(I)+UC),.5*(VBS(I)+VC),.5*(WBS(I)+WC),U,V,W)
BV=XD*U+YD*V+ZD*W
AV=XD1*U+YD1*V+ZD1*W
FL=0.

```

```

A=A2*COS2-AV*AV
B=AR*COS2-AV*BV
C=B2*COS2-BV*BV
TERM=B*B-A*C
IF (TERM.LT.0.) GO TO 9
IF (A.LE.0..AND.B.GT.0.) GO TO 9
IF (C) 1,3,1
FL=C/(B-SQRT(TERM))
IF (IPRINT.GE.2) WRITE (IOU6,14) COS2,BV,AV,U,V,W,A,B,C,TERM,FL,A2,AB
IF (LOT(I).NE.0.OR.(FL.GE.0..AND.FL.LE..7)) GO TO 2
IF (I.NE.4).OR.(KPRINT(3).GT.0.) WRITE (IOU6,10) I,FL
LOT(I)=I
IF (I.NE.4) STEP=-.1
IF (FL.GE.0..AND.FL.LE.1.) GO TO 3
IF (I.NE.4).OR.(KPRINT(3).GT.0) WRITE (IOU6,16) I,FL
IF (N.EQ.4) GO TO 3
ITEST = ITEST+1
RETURN
XBS(I)=HUB(1)+FL*XDI
YBS(I)=HUB(2)+FL*YDI
ZBS(I)=HUB(3)+FL*ZDI
UBS(I)=HUB(4)+FL*(UH(I)-HUB(4))
VBS(I)=HUB(5)+FL*(VH(I)-HUB(5))
WBS(I)=HUB(6)+FL*(WH(I)-HUB(6))
PBS(I)=HUB(7)+FL*(PH(I)-HUB(7))
PPMBS(I)=HUB(8)+FL*(PPMH(I)-HUB(8))
CALL NORM (URS(I),VBS(I),WBS(I),UBS(I),PBS(I),PPMBS(I))
AMU=ASIN(SQRT(GF(2)/((PPMBS(I)/PBS(I))*GF(7)-1.)))
IF (IPRINT.GE.2) WRITE (IOU6,14) U,V,W,A,B,C,TERM,FL,AMU
1  ,PBS(I),PPMBS(I),HUB(7),WH(I),HUB(8),PPMH(I)
IF (J.EQ.1) GO TO 5
IF (FL.GT.1.) GO TO 6
IF (ABS(AMU-AMU0).LE.EPSLN) GO TO 6
AMU0=AMU
WRITE (IOU6,12) I
CALL EXIT
IF (UBS(I)**2+WBS(I)**2.GT.4.E-06) GO TO 7
ILL=ILL+1
RETURN
THBS(I)=ACOS(VBS(I))
PSBS(I)=ATAN2(WBS(I),UBS(I))
CONTINUE
IF (N.EQ.4) LOT(4) = 0

```

```

9      RETURN
      WRITE (10U6,11) I,A,B,C,TERM
      IF (I.NE.4.OR.N.EQ.4) CALL EXIT
      LOT(4) = 4
      GO TO 200

C
10     FORMAT (11H BASE POINT,I2,13H VIOLATES CFL,F10.5)
11     FORMAT (31H0INTERSEXTION FAILURE, BASEPT NO,I2,4E18.8)
12     FORMAT (43H0MACH CONE CONVERGENCE FAILURE IN BASEPT NO,I2)
13     FORMAT (19H0***** BASEPT *****)
14     FORMAT (8E15.7)
15     FORMAT (14H0BASE POINT NO,I2)
16     FORMAT (8H BASE PT,I2,13H EXTRAPOLATES,F10.5,16H, STEP DECREASED)
      END
D 74
D 75

D 77
D 78
D 79
D 80
D 81
D 82
D 83
D 84
D 85

```

```

*DECK E
SUBROUTINE COEFS (IND)
  IND = 1 FOR BODY, 2 FOR FIELD, 3 FOR SHOCK
  COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSSLN,DP,DTHTA,DPSI
  COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
  COMMON /CONT/ NPC,DYC,IIL,KURE,SINE,COSINE
  COMMON /ESENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
    1PS,HUB(8)
  COMMON /BSPT/ XBS(4),YBS(4),ZBS(4),UBS(4),VBS(4),WBS(4),PBS(4),
    2IPMB(4),THBS(4),PSBS(4)
  DIMENSION DX(4),DY(4),DZ(4),DTH(4),DPS(4),A(4),B(4),C(4),D(4)
  IF (IPRINT.GE.2) WRITE (IOU6,8)
  N=4
  IF (IND.EQ.2) GO TO 2
  N=3
  DX(4)=XC-HUB(1)
  DY(4)=YC-HUB(2)
  DZ(4)=ZC-HUB(3)
  DTH(4)=THETAC-TH
  DPS(4)=PSIC-PS
  AMUC=ASIN(SQRT(GF(2)/((PPMC/PC)**GF(7)-1.)))
  DO 3 I=1,N
    DX(I)=XC-XBS(I)
    DY(I)=YC-YBS(I)
    DZ(I)=ZC-ZBS(I)
    DTH(I)=THETAC-THBS(I)
    DPS(I)=PSIC-PSBS(I)
    IF (IPRINT.GE.2) WRITE (IOU6,9) DX(I),DY(I),DZ(I),DTH(I),DPS(I)
  CONTINUE
  DO 5 I=1,N
    CALL NORM (.5*(UBS(I)+UC),.5*(VBS(I)+VC),.5*(WBS(I)+WC),UNT,VNT,
    1WNT)
    IF (IPRINT.GE.2) WRITE (IOU6,9) UNT,VNT,WNT
    J=MOD(I,4)+1
    K=MOD(I-5,4)+4
    CALL SOL (DX(I),DY(I),DZ(I),DTH(I),DX(J),DY(J),DZ(J),DTH(J),DX(K),
    1DY(K),DZ(K),DTH(K),DTHDX,DTHDY,DTHDZ)
    CALL SOL (DX(I),DY(I),DZ(I),DPS(I),DX(J),DPS(J),DX(K),
    1DY(K),DZ(K),DPS(K),DPSDX,DPSDY,DPSDZ)
    CALL NORM (VNT*DZ(I)-WNT*DY(I),WNT*DX(I)-UNT*DY(I)-VNT*
    1DX(I),DXDN,DYDN,DZDN)
    DTHDN=DTHDX*DXDN+DTHDY*DYDN+DTHDZ*DZDN
    UPSDN=DPSDX*DXDN+DPSDY*DYDN+DPSDZ*DZDN

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IF (IPRINT.GE.2) WRITE (IOU6,9) DXDN,DYDN,DZDN,DTHDN,DPSDN
VCHEK=SQRT(UNT*UNT+WNT*WNT)
IF (VCHEK.GT.2.E-3) GO TO 4
ILL=ILL+1
RETURN
COSD1=(UNT*DZDN-WNT*DXDN)/VCHEK
IF (ABS(COSD1).GT.1.) COSD1=SIGN(1.,COSD1)
UZWX=UNT*DZ(I)-WNT*DX(I)
SIND1=SIGN(SQRT(1.-COSD1*COSD1),UZWX)
AMUAV=.5*(AMUC+ASIN(SQRT(GF(2)/((PPMBS(I)/PBS(I))*GF(7)-1.))))
SINMU=SIN(AMUAV)
SINTH=SIN(.5*(THETAC+THBS(I)))
DL=SQRT(DX(I)*DX(I)+DY(I)*DY(I)+DZ(I)*DZ(I))
IF (IPRINT.GE.2) WRITE (IOU6,9) AMUAV,SINMU,SINTH,SIND1,COSD1,DL
A(I)=SINMU*COS(AMUAV)/(GF(1)*.5*(PC+PBS(I)))
B(I)=-COSD1
C(I)=SINTH*SIND1
D(I)=A(I)*PBS(I)+B(I)*THBS(I)+C(I)*PSRS(I)-DL*SINMU*(SIND1*DTHDN+
1SINTH*COSD1*DPSDN)
IF (IPRINT.GE.2) WRITE (IOU6,9) A(I),B(I),C(I),D(I)
CONTINUE
DO 6 I=1,9
COF(I)=0.
DO 7 I=1,N
COF(1)=COF(1)+A(I)*D(I)
COF(2)=COF(2)+B(I)*D(I)
COF(3)=COF(3)+C(I)*D(I)
COF(4)=COF(4)+A(I)*A(I)
COF(5)=COF(5)+A(I)*B(I)
COF(6)=COF(6)+A(I)*C(I)
COF(7)=COF(7)+B(I)*B(I)
COF(8)=COF(8)+B(I)*C(I)
COF(9)=COF(9)+C(I)*C(I)
IF (IPRINT.GE.2) WRITE (IOU6,9) (COF(I),I=1,9)
RETURN
FORMAT (18H0***** COEFS *****)
FORMAT (8E15.7)
END

```

```

*DECK F SUBROUTINE COMPAT
C**** Y-AXIS MUST ALIGN WITH FREE STREAM, ROTATE AXES IF NEEDED
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTA,DPSI
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
COMMON /SENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC
IF (IPRINT.GE.2) WRITE (IOU6,4)
GM2=GF(1)*FMSTR*FMSTR
DO 2 I=1,20
XI=PC*POP
DI=XI-1.
D2=GM2-D1
D4=XI+GF(4)
D3=GM2/GF(3)-D4
THETAC=ATAN(SQRT(D3/D4)*D1/D2)
PSIC=(COF(3)-COF(8)*THETAC-COF(6)*PC)/COF(9)
SN2T=.5*SIN(2.*THETAC)
DTHDP=SN2T*(1./D1+1./D2-.5/D3-.5/D4)*POP
DPSDP=- (COF(8)*DTHDP+COF(6))/COF(9)
D2TDP2=COS(2.*THETAC)/SN2T*DTHDP*DTHDP+POP**2*SN2T*(-1./D1**2+1./
102**2-.5/D3**2+.5/D4**2)
C=COF(5)*PC+COF(7)*THETAC+COF(8)*PSIC-COF(2)
H=C*DTHDP+COF(4)*PC+COF(5)*THETAC+COF(6)*PSIC-COF(1)
HP=C*D2TDP2+(COF(7)*DTHDP+COF(8)*DPSDP+2.*COF(5))*DTHDP+COF(6)*
1DPSDP+COF(4)
PC=PC-H/HP
IF (IPRINT.GE.2) WRITE (IOU6,5) PC,THETAC,PSIC,XI,D1,D2,D3,D4,SN2T
1,DTHDP,DPSDP,D2TDP2,C,H,HP
IF (I.EQ.1) GO TO 1
IF (ABS((PC-PCN)/PC).GT.DP) GO TO 1
IF (ABS(THETAC-THCN).GT.DTHETA) GO TO 1
IF (ABS(PSIC-PSCN).LE.DPSI) GO TO 3
PCN=PC
THCN=THETAC
PSCN=PSIC
WRITE (IOU6,6)
CALL EXIT
PPMC=(D4/(GF(4)*XI+1.))*GF(6)/XI**GF(5)
RETURN
1
2
3
C
4
5
6
FORMAT (19H0***** COMPAT *****)
FORMAT (8E15.7)
FORMAT (30H0CONVERGENCE FAILURE IN COMPAT)

```

F 43

END

```

*DECK G
SUBROUTINE GMTRY (SINE,COSINE,XC,YC,ZC,A4,B4,C4)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTETA,DPSI
COMMON/GEOM/ YMAX,YSTOP,INDEX
X1=CO SINE*XC-SINE*YC
YC=SINE*XC+CO SINE*YC
TA=CO SINE*A4-SINE*B4
TB=SINE*A4+CO SINE*B4
XC=X1
ZI=ZC
IND=0
DO 10 J=1,5
INDEX=0
IN=IND
T=0.
DO 1 I=1,20
CALL FIGURE(XC,YC,ZC,F,A,B,C)
IF (INDEX.EQ.IND) GO TO 2
IF (I.GT.1) GO TO 9
B1=TA*B-TB*A
B3=C4*B-TB*C
9 T=T-F/(B1*A+B3*C)
XC=X1+T*B1
ZC=Z1+T*B3
IF (IPRINT.GE.2) WRITE (IOU6,3)
IF (IPRINT.GE.2) WRITE (IOU6,4) T,XC,YC,ZC,F,A,B,C,INDEX,IND,J
IF (ABS(F).LE.1.E-6) GO TO 10
1 CONTINUE
WRITE (IOU6,5)
CALL EXIT
10 IND=INDEX
WRITE (IOU6,6) INDEX,IN
2 CALL ROTATE (XC,YC,SINE,COSINE)
CALL NORM (COSINE*A+SINE*B,-SINE*A+COSINE*B,C ,A4,B4,C4)
RETURN
C
FORMAT(25(2H *),6H GMTRY,25(2H *))
FORMAT (8G15.7,3I3)
FORMAT (29H0CONVERGENCE FAILURE IN GMTRY)
FORMAT (40H0BODY POINT OSCILLATING BETWEEN SECTIONS,12,4H AND,12)
END

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```

*DECK H
SUBROUTINE FIGURE (X,Y,Z,F,A,B,C)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHETA,DPSI
COMMON /GEOM/ YMAX,YSTOP,INDEX
DIMENSION ZX(13),ZXP(13),P(13),Q(13),R(13),S(13),T(13),SG(13)
IF(Y.GT.YSTOP+.0001.AND.ABS(YSTOP).GT.EPSLN) GO TO 7
DO 2 I=1,50
IF (Y.LE.YMAX) GO TO 3
M=7
READ (IOU5,8) YMAX,N
IF(EOF(IOU5)) 7,1
WRITE (IOU6,12) YMAX,N
DO 2 K=1,N
READ (IOU5,10) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
IF(L.GT.7) M=13
WRITE (IOU6,13) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
2 CONTINUE
3 DO 4 I=1,M
CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),ZXP(I))
4 CONTINUE
IF(INDEX.GT.0) GO TO (101,201,301,401,501,601),INDEX
IF(M.EQ.7) GO TO 50
X1=(ZX(12)-ZX(13))*
*      SQRT(1.-((ZX(8)-ZX(11))/(ZX(10)-ZX(11))**2)+ZX(13))
IF((Z.GT.ZX(2)).AND.(X.LT.ZX(13))) GO TO 600
IF((Z.GT.ZX(8)).AND.(X.LT.X1)) GO TO 100
IF((ZX(8)-ZX(9)).LE.0.) GO TO 50
IF(Z.GT.ZX(9)) GO TO 200
50 IF(Z.GT.ZX(2)) GO TO 300
IF(X.GT.ZX(6)) GO TO 400
*****LOWER FLAT SECTION
INDEX=5
501 A=0.0
C=-1.0
B=ZXP(3)
F=- (Z-ZX(3))
GO TO 6
*****CANOPY
100 INDEX=1
101 CALL ELIPSE(X,Z,ZX,ZXP,10,11,13,12,A,B,C,F)
GO TO 6
*****CUBIC SECTION
200 INDEX=2

```

```

43      201 CALL CUHIC(X,Z,ZX,ZXP,A,B,C,F)
44      GO TO 6
45      C***UPPER ELLIPSE SECTION
46      300 INDEX=3
47      301 CALL ELIPSE(X,Z,ZX,ZXP,1,2,4,5,A,B,C,F)
48      GO TO 6
49      C***LOWER CONIC SECTION
50      400 INDEX=4
51      401 CALL KONIC(X,Z,ZX,ZXP,6,3,5,2,7,A,B,C,F)
52      GO TO 6
53      C***CANOPY FLAT SECTION
54      600 INDEX=6
55      601 A=0.0
56      C=-1.0
57      B=ZXP(10)
58      F=- (Z-ZX(10))
59      6 IF (IPRINT.GE.2) WRITE(10U6,9) F,A,B,C,INDEX
60      RETURN
61      WRITE (10U6,11)
62      CALL EXIT
63
64      C
65      FORMAT (F10.5,I5)
66      FORMAT(19H0***** FIGURE *****/4G14.7,21H BODY SECTION INDEX =,I2)
67      FORMAT (I2,SE15.8,F2.0)
68      FORMAT(1H0,60(2H *)/1H0,20X,35H$$$$$ HALLELUJAH, YOU HAVE GONE ALLH
69      1, 35H THE WAY--FEELING NICE, I BET $$$$$/1H0,60(2H *))
70      FORMAT (35H0GEOMETRIC COEFFICIENTS FOR Y UP TO,G15.7,I5,11H NEW CUH
71      IRVES)
72      FORMAT (9H0CURVE NO,I3,5H, P =E16.8,5H Q =E16.8,5H R =E16.8,5H
73      1S =E16.8,5H T =E16.8,6H SG =F4.1)
      END

```

```

*DECK I SUBROUTINE TRANS (H,XYZ,A4,B4,C4,TO,IN)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHETA,DPSI
DIMENSION H(4,8),XYZ(3,7)
IF (A4*A4+C4*C4*LE.1.E-14) RETURN
COSX=-SQRT(1.-C4*C4)
SRT=SQRT(A4*A4+B4*B4)
IF (SRT.GT.1.E-7) GO TO 1
COSZ=0.
SINZ=1.*TO
GO TO 2
1 COSZ=-B4/SRT
SINZ=TO*A4/SRT
DO 5 J=1,7
IF (IN.EQ.0.AND.J.GT.4) GO TO 5
IF (IN.NE.0.AND.J.GT.3) GO TO 4
DO 3 K=1,4,3
IF (TO.GT.0.) CALL ROTATE (H(J,K),H(J,K+1),SINZ,COSZ)
CALL ROTATE (H(J,K+1),H(J,K+2),C4*TO,COSX)
IF (TO.LT.0.) CALL ROTATE (H(J,K),H(J,K+1),SINZ,COSZ)
CONTINUE
3 IF (IN.EQ.0) GO TO 5
IF (J.GT.2.AND.J.LT.6) GO TO 5
IF (TO.GT.0.) CALL ROTATE (XYZ(1,J),XYZ(2,J),SINZ,COSZ)
CALL ROTATE (XYZ(2,J),XYZ(3,J),C4*TO,COSX)
IF (TO.LT.0.) CALL ROTATE (XYZ(1,J),XYZ(2,J),SINZ,COSZ)
CONTINUE
5 IF (IPRINT.GE.2) WRITE (IOU6,6) H,XYZ
IF (TO.LT.0..OR.IN.EQ.0) RETURN
XYZ(3,3)=ACOS(XYZ(2,2))
XYZ(1,4)=ATAN2(XYZ(3,2),XYZ(1,2))
XYZ(2,5)=ACOS(XYZ(2,7))
XYZ(3,5)=ATAN2(XYZ(3,7),XYZ(1,7))
RETURN
C 6 FORMAT (18H0***** TRANS *****/(8E15.7))
END

```

```

1 I
2 I
3 I
4 I
5 I
6 I
7 I
8 I
9 I
10 I
11 I
12 I
13 I
14 I
15 I
16 I
17 I
18 I
19 I
20 I
21 I
22 I
23 I
24 I
25 I
26 I
27 I
28 I
29 I
30 I
31 I
32 I
33 I
34 I
35 I
36 I

```

```
*DECK J
SUBROUTINE ROTATE (X,Y,SINE,COSINE)
TEMP=X
X=COSINE*TEMP+SINE*Y
Y=-SINE*TEMP+COSINE*Y
RETURN
END
```

```
J J J J J J
1 2 3 4 5 6
```



```

*DECK K
SUBROUTINE SOL (A11,A12,A13,D1,A21,A22,A23,D2,A31,A32,A33,D3,X,Y,Z
1)
  IF (ABS(A11).LE.1.E-7) GO TO 1
  B12=A12/A11
  B13=A13/A11
  C1=D1/A11
  B22=A22-B12*A21
  IF (ABS(B22).LE.1.E-7) GO TO 1
  B32=A32-B12*A31
  B23=(A23-B13*A21)/B22
  C2=(D2-A21*C1)/B22
  B33=(A33-A31*B13-B23*B32)
  IF (ABS(B33).LE.1.E-7) GO TO 1
  Z=(D3-C1*A31-C2*B32)/B33
  Y=C2-B23*Z
  X=C1-B12*Y-B13*Z
  RETURN
1 D=A11*(A22*A33-A23*A32)+A21*(A13*A32-A12*A33)+A31*(A12*A23-A13*A22
1)
  X=(A13*(D2*A32-A22*D3)+A23*(A12*D3-D1*A32)+A33*(D1*A22-A12*D2))/D
  Y=(A11*(D2*A33-A23*D3)+A21*(A13*D3-D1*A33)+A31*(D1*A23-A13*D2))/D
  Z=(A12*(D2*A31-A21*D3)+A22*(A11*D3-D1*A31)+A32*(D1*A21-A11*D2))/D
  RETURN
END

```

```

*DECK L
SUBROUTINE HARNES (QINF,A,N)
DIMENSION A(50,8,4)
DO 1 L=3,N
VN=SQRT(A(L,4)**2+(QINF-A(L,5))**2+A(L,6)**2)
CALL NORM (-A(L,4),QINF-A(L,5),-A(L,6),A0,B0,C0)
A1=(A(L+1,3)-A(L,3))**2+(A(L+1,1)-A(L,1))**2
C1=(A(L+3)-A(L-1,3))**2+(A(L,1)-A(L-1,1))**2
CALL NORM (C1*(A(L+1,3)-A(L,3))+A1*(A(L,3)-A(L-1,3)),0,C1*(A(L+1,
11)-A(L,1))+A1*(A(L,1)-A(L-1,1)),A1,B1,C1)
B=SQRT(1.-B0*B0)
CALL NORM (SIGN(A1*B,A0)+A0*0.,SIGN(C1*B,C0)+C0,A1,B1,C1)
A(L,4)=-A1*VN*B
A(L,6)=-C1*VN*B
RETURN
END

```

1

```

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15

```

```

*DECK M
SUBROUTINE MIRROR (A,SIN2A,COS2A,N)
DIMENSION A(50,8)
I=1
J=3
DO 2 L=1,2
DO 1 K=1,4,3
A(I,K)=-COS2A*A(J,K)+SIN2A*A(J,K+1)
A(I,K+1)=SIN2A*A(J,K)+COS2A*A(J,K+1)
A(I,K+2)=A(J,K+2)
A(I,K/4+7)=A(J,K/4+7)
I=N+L
J=N-L
RETURN
END

```

1

2

```

M M M M M M M M M M M M M M M
1 2 3 4 5 6 7 8 9 10 11 12 13 14

```

```
*DECK N
SUBROUTINE NORM (X,Y,Z,A,B,C)
T=SQRT(X*X+Y*Y+Z*Z)
A=X/T
B=Y/T
C=Z/T
RETURN
END
```

```
1
2
3
4
5
6
7

N
N
N
N
N
N
N
```



```

*DECK 0
SUBROUTINE DATOUT (A,I,IND,KAB,IO)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSI,N,UP,DIHETA,DPSI,KP4,IOU3
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP
COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE,N,Y,IS
DIMENSION A(50,8)
IF (N.EQ.IS.AND.IO.NE.0) RETURN
IF (KP4.LE.0.AND.(IO.EQ.1.AND.N/KAB*KAB.NE.N)) RETURN
IF ((KP4.GT.0.AND.IO.EQ.0).AND.(N/KAB*KAB.NE.N.AND.(IND.NE.1.OR.(
1I.NE.2.AND.I.NE.NPC+1)))) RETURN
RAD=57.2957795130823
P=A(I,7)*POP
PI=A(I,7)/A(I,8)
CP=2.*(P-1.)/(GF(1)*FMSTR*FMSTR)
XM=SQRT(1./PI*GF(7)-1.)/GF(2))
X=COSINE*A(I,1)-SINE*A(I,2)
U=COSINE*A(I,4)-SINE*A(I,5)
V=SINE*A(I,4)+COSINE*A(I,5)
OW=ATAN(U/V)*RAD
UW=ATAN(A(I,6)/V)*RAD
PS=0.
TH=0.
IF (ABS(A(I,6)).LE.1.E-07.AND.ABS(U).LE.1.E-07) GO TO 1
PS=ATAN2(A(I,6),U)*RAD
TH=ACOS(V/SQRT(U*U+V*V+A(I,6)*A(I,6)))*RAD
IF (IO.EQ.0.OR.KP4.GE.0) GO TO 2
WRITE (IOU7,12) A(I,3),X,XM,A(I,8),TH,PS
RETURN
1 IOU=IOU6
IF (KP4.GE.0.AND.IO.EQ.1) IOU=IOU3
IF (I.GT.2) GO TO 3
Y=SINE*A(I,1)+COSINE*A(I,2)
IF (IND.EQ.1) WRITE (IOU,11) N,Y
IF (KP4.GT.1.AND.(IO.EQ.0.AND.N/KAB*KAB.NE.N)) GO TO 4
IF (IND.EQ.1) WRITE (IOU,6)
IF (IND.EQ.2) WRITE (IOU,7)
IF (IND.EQ.3) WRITE (IOU,8)
WRITE (IOU,9)
IF (KP4.GT.1.AND.(IO.EQ.0.AND.N/KAB*KAB.NE.N)) GO TO 5
WRITE (IOU,10) A(I,3),X,XM,A(I,8),TH,PS,CP,P,A(I,7),OW,UW
RETURN
4 WRITE (IOU6,13) CP
5 IF (I.EQ.NPC+1) WRITE (IOU6,14) CP

```



```

*DECK P
SUBROUTINE TIDYUP (SINE,COSINE,A,NP,NPP,AM)
COMMON /MESH/ K1,K2
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHEA,DPSI
DIMENSION A(50,8,4)
DO 1 I=1,NP
CALL ROTATE (A(I,1),A(I,2),-SINE,COSINE)
CALL ROTATE (A(I,4),A(I,5),-SINE,COSINE)
A(I,1,4)=0.
DO 2 I=2,NP
IF (A(I,3).LT.AM) J=I
A(I,1,4)=A(I-1,1,4)+SQRT((A(I,1)-A(I-1,1))**2+(A(I,2)-A(I-1,2))**2)
1+(A(I,3)-A(I-1,3))**2)
IM=(A(J+1,1,4)*(AM-A(J,3))+A(J,1,4)*(A(J+1,3)-AM))/(A(J+1,3)-A(J,3)
1))
NT=2*NPP-2*K1-K2
N=0
DO 3 M=2,NPP
N=N+1
IF (M.LE.K1.OR.M.GT.K2) N=N+1
IF (N.GE.NT/2) GO TO 4
CONTINUE
DT1=(A(NP,1,4)-IM)/FLOAT(NT-N)
DO 5 I=1,8
DT=TM/FLOAT(N)
L=1
IF (I.EQ.1.OR.I.EQ.4) L=2
CALL KURFIT (A(1,1,4),A(1,1),A(1,1,3),NP,0.0,0.0,L,L)
PT=-DT-DT
DO 5 J=1,NPP
IF (J.GT.M) DT=DT1
PT=PT+DT
IF (J.LE.K1.OR.J.GT.K2) PT=PT+DT
CALL KURVE (A(1,1,3),A(1,1,4),A(1,1),PT,A(J,1,2),NP,0)
CONTINUE
IF (IPRINT.GE.2) WRITE (IOU6,7) ((A(I,J,2),J=1,3),I=1,NPP)
DO 6 I=1,NPP
CALL ROTATE (A(I,1,2),A(I,2,2),SINE,COSINE)
CALL ROTATE (A(I,4,2),A(I,5,2),SINE,COSINE)
RETURN
FORMAT (14H0***** TIDYUP *****/(9E14.6))
END

```

```

*DECK 0
SUBROUTINE REFORM (A,L,TAPE,NTAPE,NPC,LINE,NLINE)
DIMENSION A(50,8,4),X(3)
REWIND LTAPE
ALINE=NLINE-1
DO 8 I=1,NPC
REWIND NTAPE
DO 4 J=1,LINE
READ (NTAPE) ((A(L,K,2),K=1,8),L=1,NPC)
IF (I.NE.1.OR.J.NE.1) GO TO 2
DO 1 K=1,3
X(K)=.5*(A(1,K,2)+A(NPC,K,2))
DO 3 K=1,8
A(J,K)=A(I,K,2)
A(J,8)=ALOG10(-ALOG10(A(J,8)))
A(1,1,4)=SQRT((A(1,1)-X(1))**2+(A(1,2)-X(2))**2+(A(1,3)-X(3))**2)
DO 5 J=2,LINE
A(J,1,4)=A(J-1,1,4)+SQRT((A(J,1)-A(J-1,1))**2+(A(J,2)-A(J-1,2))**2
1+(A(J,3)-A(J-1,3))**2)
DA=(A(LINE,1,4)-A(1,1,4))/ALINE
DO 6 K=1,8
CALL KURFIT (A(1,1,4),A(1,K),A(1,1,3),LINE,0.,0.,2,2)
DO 6 J=1,NLINE
PA=A(1,1,4)+DA*FLOAT(J-1)
CALL KURVE (A(1,1,3),A(1,1,4),A(1,K),PA,A(J,K,2),LINE,K)
DO 7 J=1,NLINE
A(J,8,2)=10.**(-10.**A(J,8,2))
WRITE (LTAPE) ((A(M,K,2),K=1,8),M=1,NLINE)
REWIND NTAPE
DO 10 J=1,NLINE
REWIND LTAPE
DO 9 I=1,NPC
READ (LTAPE) ((A(M,K,2),K=1,8),M=1,NLINE)
DO 9 K=1,8
A(I,K)=A(J,K,2)
WRITE (NTAPE) ((A(L,K),K=1,8),L=1,NPC)
LINE=NLINE
RETURN
END

```



```

*DECK S
SUBROUTINE KURVE (A,X,Y,XP,YP,N,L)
DIMENSION A(1),X(1),Y(1)
DO 3 I=2,N
  IF ((XP-X(1))*(X(2)-X(1))) 4,4,2
  IF ((XP-X(1))*(XP-X(1))) 4,3,3
CONTINUE
K=2*I-3
C1=XP-X(I-1)
C2=X(I)-XP
IF (L.EQ.8) C2=0.
SLOPE=(Y(I)-Y(I-1))/(X(I)-X(I-1))
YP=Y(I-1)+(SLOPE+A(K)*C2+A(K+1)*C1*C2)*C1
RETURN
END

```

```

1 2 3 4 5 6 7 8 9 10 11 12 13 14
S S S S S S S S S S S S S S

```

```

*DECK T
SUBROUTINE CONICF (P,Q,R,S,T,SG,X,Y,YP)
ROOT=SG*SQRT((R*X+S)*X+T)
Y=P*X+Q+ROOT
IF ((SG.NE.0.).AND.(ROOT.NE.0.)) GO TO 10
YP=P
GO TO 20
10 YP=P+(R*X+S/2.0)/ROOT
20 RETURN
END

```

T0010
T0020
T0030

T0050
T0060
T0070
T0080
T0090

```

*DECK U
SUBROUTINE CUBIC(X,Z,ZX,ZXP,A,B,C,F)
DIMENSION ZX(1),ZXP(1)
DZ1=ZX(8)-ZX(11)
DZ2=ZX(9)-ZX(2)
DZC=ZX(10)-ZX(11)
DZU=ZX(1)-ZX(2)
DZ21=ZX(9)-ZX(8)
X1=(ZX(12)-ZX(13))*SQRT(1.0-(DZ1/DZC)**2)+ZX(13)
X2=(ZX(5)-ZX(4))*SQRT(1.0-(DZ2/DZU)**2)+ZX(4)
DX21=X2-X1
IF(X1.GT.ZX(13)) GO TO 20
10 Z1P=0.0
X1Y=0.0
Z1PY=0.0
GO TO 30
20 Z1P=-X1/DZ1*(DZC/(ZX(12)-ZX(13)))*2
X1P=1.0/Z1P
X1Y=X1*((ZX(12)-ZXP(13))/(ZX(12)-ZX(13)))+(ZXP(8)-(ZX(8)-ZX(10))
* ZXP(11)-DZ1*ZXP(10))/DZC/Z1P+ZXP(13)
* +2.0*((ZX(12)-ZXP(13))/(ZX(12)-ZX(13))-(ZXP(10)-ZXP(11))/DZC))
X1PY=X1P*((ZXP(8)-ZXP(11))/DZ1-X1Y/X1
Z1PY=-X1PY*Z1P/X1P
30 Z2P=-X2/DZ2*(DZU/(ZX(4)-ZX(5)))*2
X2P=1.0/Z2P
X2Y=X2*((ZX(5)-ZXP(4))/(ZX(5)-ZX(4)))+(ZXP(9)-(ZX(9)-ZX(1))
* ZXP(2)-DZ2*ZXP(1))/DZU/Z2P+ZXP(4)
X2PY=X2P*((ZXP(9)-ZXP(2))/DZ2-X2Y/X2
* +2.0*((ZX(4)-ZXP(5))/(ZX(4)-ZX(5))-(ZXP(1)-ZXP(2))/DZU))
Z2PY=-X2PY*Z2P/X2P
ZY21=ZXP(9)-ZXP(8)
DX21Y=X2Y-X1Y
IF((Z1P.LT.-4.0).OR.(Z2P.LT.-4.0).OR.(Z1P.GT.0.01)) GO TO 40
CA=3.0*DZ21-(Z2P+2.0*Z1P)*DX21
CB=-2.0*DZ21+(Z2P+Z1P)*DX21
CAY=3.0*ZY21-(Z2PY+2.0*Z1PY)*DX21-(Z2P+2.0*Z1P)*DX21Y
CBY=-2.0*ZY21+(Z2PY+Z1PY)*DX21+(Z2P+Z1P)*DX21Y
DX1=X-X1
DX2=X-X2
T=DX1/DX21
A=-Z1P-(2.0*CA+3.0*CB*T)*T/DX21
B=-ZXP(8)-Z1PY*DX1+Z1P*X1Y-(CAY+CBY*T)*T*T
* -(A+Z1P)*(X2Y*DX1-X1Y*DX2)/DX21

```


00001030
00001040
00001050

```

C=1.0
F=Z-ZX(8)-Z1P*DX1-(CA+CB*T)*T*T
RETURN
40 CA=3.0*DX21-(X2P+2.0*X1P)*DZ21
CB=-2.0*DX21+(X2P+X1P)*DZ21
CAY=3.0*DX21Y-(X2PY+2.0*X1PY)*DZ21-(X2P+2.0*X1P)*ZY21
CBY=-2.0*DX21Y+(X2PY+X1PY)*DZ21+(X2P+X1P)*ZY21
DZ1=Z-ZX(8)
DZ2=Z-ZX(9)
T=DZ1/DZ21
A=1.0
C=-X1P-(2.0*CA+3.0*CB*T)*T/DZ21
B=-X1Y-X1PY*DZ1+X1P*ZXP(8)-(CAY+CBY*T)*T*T
* -(C+X1P)*(ZXP(9)*DZ1-ZXP(8)*DZ2)/DZ21
F=X-X1-X1P*DZ1-(CA+CB*T)*T*T
RETURN
END

```

00001060

```

*DECK V
SUBROUTINE ELLIPSE (X,Z,ZX,ZXP,IZK,IZM,IXK,IXM,A,B,C,F)
DIMENSION ZX(1),ZXP(1)
FF=-ABS(Z-ZX(IZK))
DX=X-ZX(IXK)
DXK=ZX(IXM)-ZX(IXK)
DZ=Z-ZX(IZM)
DZK=ZX(IZK)-ZX(IZM)
A=2.0*DX/DXK**2
C=2.0*DZ/DZK**2
B=C*(ZXP(IZM)*FF-ZXP(IZK)*DZ)/DZK+A*(ZXP(IXK)*(X-ZX(IXM))
* -ZXP(IXM)*DX)/DXK
F=(DZ/DZK)**2+(DX/DXK)**2-1.0
RETURN
END

```

```

V0010
V0020
V0030
V0040
V0050
V0060
V0070
V0080
V0090
V0100
V0110
V0120
V0130
V0140

```

```

*DECK W SUBROUTINE KONIC(X,Z,ZX,ZXP,ICX,ICZ,ISX,ISZ,IB,A,B,C,F)
DIMENSION ZX(1),ZXP(1)
SIG = SIGN(1.,ZX(ICZ))-ZX(ISZ))
H = SIG*(1.414213562*ZX(IB)-ZX(ISX))-ZX(ISZ)
HY = SIG*(1.414213562*ZXP(IB)-ZXP(ISX))-ZXP(ISZ)
ZZ = Z-ZX(ISZ)
XX = X-ZX(ISX)
Z1 = ZX(ICZ)-ZX(ISZ)
Z1Y = ZXP(ICZ)-ZXP(ISZ)
X1 = ZX(ICX)-ZX(ISX)
X1Y = ZXP(ICX)-ZXP(ISX)
CK = (H-Z1)**2/(4.*H*X1*Z1*(H-SIG*X1-Z1))
CKY = CK*(2.*(HY-Z1Y)/(H-Z1)-HY/H-X1Y/X1-Z1Y/Z1-
1 (HY-SIG*X1Y-Z1Y)/(H-SIG*X1-Z1))
XZX = X1*ZZ-Z1*XX
F = CK*XZX*XZX+XX*(ZZ-Z1)
A = -2.*CK*Z1*XZX+ZZ-Z1
C = 2.*CK*X1*XZX+XX
B = -A*ZXP(ISX)-C*ZXP(ISZ)+XZX*XZX*CKY+2.*CK*ZZ*XZX*X1Y
1 -(2.*CK*XZX+1.)*XX*Z1Y
RETURN
END

```

```

00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001750
00001760

```

```

*DECK X
SUBROUTINE AERO(NPC,SINA,COSA)
COMMON /CP/B(50,4,2),DRAG,ALIFT,TORQUE,YMT,ZMT,WINGA
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTA,DPSI,KP4,IOU3
DO 10 I=1,2
DO 10 J=2,NPC
DO 10 K=1,2
L=J+K-1
M=(3-K)*I+(3-I)*K-3
CPA=(B(L,4,M)+B(J+1,4,I)+B(J,4,3-I))/(6.0*WINGA)
YA=(B(L,2,M)+B(J+1,2,I)+B(J,2,3-I))/3.0
ZA=(B(L,3,M)+B(J+1,3,I)+B(J,3,3-I))/3.0
IF(I.NE.K) CPA=-CPA
DARY=CPA*(B(J+1,3,I)-B(L,3,M))*B(J,1,3-I)-B(L,1,M))-
*      (B(J+1,1,I)-B(L,1,M))*B(J,3,3-I)-B(L,3,M))
DARZ=CPA*(B(J+1,1,I)-B(L,1,M))*B(J,2,3-I)-B(L,2,M))-
*      (B(J+1,2,I)-B(L,2,M))*B(J,1,3-I)-B(L,1,M))
DRAG=DRAG+DARY*COSA+DARZ*SINA
ALIFT=ALIFT+DARZ*COSA-DARY*SINA
10 TORQUE=TORQUE+DARY*(ZA-ZMT)-DARZ*(YA-YMT)
FY=DRAG*COSA-ALIFT*SINA
FZ=DRAG*SINA+ALIFT*COSA
WRITE(IOU6,600) DRAG,ALIFT,TORQUE,YMT,ZMT,FY,FZ
600 FORMAT(1H0,T7,4H0RAG,T22,4HLIFT,T35,6HMOMENT,T47,
$ 13HPIVOT POINT Y,T68,1HZ,T80,7HY-FORCE,T95,7HZ-FORCE/7G15.6)
RETURN
END

```



```
*DECK Y
SUBROUTINE SETCP (LNTAPE,IB,A,B,SINE,COSINE,DUMMY,GF,FMSTR,N2)
  DIMENSION A(50,8),B(50,4,2)
  REWIND LNTAPE
  READ (LNTAPE) ((A(L,M),M=1,8),L=2,N2)
  DO 10 I=2,N2
    B(I,1,IB) = COSINE*A(I,1)-SINE*A(I,2)
    B(I,2,IB) = SINE*A(I,1)+COSINE*A(I,2)
    B(I,3,IB) = A(I,3)
    10 B(I,4,IB) = 2.0*(A(I,7)*DUMMY-1.0)/(GF*FMSTR*FMSTR)
  REWIND LNTAPE
  RETURN
END
```

```

PROGRAM FUSLAG(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,PUNCH,TAPE7=
1PUNCH,TAPE2,TAPE1,TAPE4,TAPE3)
COMMON /MESH/ K1(8),AL,Z2L,ZX23,ZX7,SIDEP,X2L
COMMON /TEST/ LOT(4),ITEST,STEP,KTEST,KPRINT(3)
COMMON /GEOM/ YMAX,YSTOP,UNIL,INDEX,DBLNL,NCQ,CQ(8,10)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTA,DPSI,KP4,IOU3
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE,ISURF,YO,ISTART,WINGST
COMMON /ESENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
IPS,HUB(8)
COMMON /BSPT/ XBS(4),YBS(4),ZBS(4),UBS(4),VBS(4),WBS(4),PBS(4),
1PPMBS(4),THBS(4),PSBS(4)
COMMON /STOR/ H(4,8),A(99,8,4)
COMMON /CP/ B(99,4,2),DRAG,ALIFT,TORQUE,YMT,ZMT,WINGA
DIMENSION YSET(20),NPSET(180),LIT(18),DUM(10),LI(8)
IN A(I,J,K) J=1,8 CORRESPOND TO X,Y,Z,U,V,W,P,PT, K=1,4 CORRESPOND
TO A(ACQUIRER), L(LOWER CLASS), M(MIDDLE CLASS), U(UPPER CLASS)
CALL FTNBIN (1,0,DUM)
IOU5=5
INCASE=3
IOU6=6
IOU7=7
IOU3=1
IOU=IOU5
LTAPE=4
NTAPE=2
REWIND LTAPE
REWIND NTAPE
LN=LTAPE+NTAPE
READ (IOU5,640) (LIT(I),I=1,18)
READ (IOU5,670) DP,DTHTA,DPSI,EPSLN,DYC,YSTOP,STEPM,WINGST
READ (IOU5,680) NSURF,LINE,NPC,NR,IFT,ISTART,KP4,NS,NL,NP,KPRINT
IOU1=IOU3
IF (KP4.LT.0) IOU1=IOU6
KAB=IABS(KP4)
IF (KP4.EQ.0) KAB=10
DO 10 I=1,NR
  READ (IOU5,650) YSET(I),NPSET(9*I-8),NPSET(9*I-7),NPSET(9*I-6),
  1NPSET(9*I-5),NPSET(9*I-4),NPSET(9*I-3),NPSET(9*I-2),NPSET(9*I-1),
  2NPSET(9*I)

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C C

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20 READ (IOU5,670) FMSTR,GF(1),ALFA,YO
   READ (IOU5,670) YA,ZA,SCALE,WINGA,DBLNL
   READ (IOU5,680) NCQ
   DO 20 J=1,NCQ
   READ (IOU5,810) IC,(CQ(I,J),I=1,2)
   READ (IOU5,810) IC,(CQ(I,J),I=3,8)
   CONTINUE
   WRITE (IOU6,660) (LIT(I),I=1,18)
   WRITE (IOU6,670) DP,DTHETA,UPSI,EPSLN,DYC,YSTOP,STEPM,WINGST
   WRITE (IOU6,680) NSURF,LINE,NPC,NR,IFT,ISTART,KP4,NS,NL,NP,KPRINT
   DO 30 I=1,NR
   WRITE (IOU6,650) YSET(I),NPSET(9*I-8),NPSET(9*I-7),NPSET(9*I-6),
1NPSET(9*I-5),NPSET(9*I-4),NPSET(9*I-3),NPSET(9*I-2),NPSET(9*I-1),
2NPSET(9*I)
   WRITE (IOU6,670) FMSTR,GF(1),ALFA,YO
   WRITE (IOU6,670) YA,ZA,SCALE,WINGA,DBLNL
   WRITE (IOU6,680) NCQ
   JJ=22
   DO 40 J=1,NCQ
   IC=CQ(8,J)
   WRITE (IOU6,820) J,(CQ(I,J),I=1,2)
   WRITE (IOU6,820) JJ,(CQ(I,J),I=3,7),IC
   CONTINUE
   WINGA=WINGA*144.0
   STEP=0.
   MESS=1
   INCRES=0
   GF(2)=-5*(GF(1)-1.)
   GF(3)=-5*(GF(1)+1.)
   GF(4)=GF(2)/GF(3)
   GF(5)=1./(GF(1)-1.)
   GF(6)=GF(1)*GF(5)
   GF(7)=1./GF(6)
   GFM2=GF(2)*FMSTR*FMSTR
   QINF=SQRT(GFM2/(1.+GFM2))
   POP=(1.+GFM2)*GF(6)
   RAD=57.295779513082
   COSA=COS(ALFA/RAD)
   SINA=SIN(ALFA/RAD)
   ISURF=1
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      ILL=0
      KURE=0
      DO 50 I=1,8
      K1(I)=0
      SINE=0.
      COSINE=1.
      S2=0.
      C2=1.
      SN=SIN(.1)
      CS=COS(.1)
      YMAX=-1.E7
      C ISTART,LT,0,RESTART FROM CARDS,ISTART=1,GT,0,RESTART FROM ITH SURFACE
      IF (ISTART.NE.0.OR.IFT.NE.1) GO TO 60
      IOU=LTAPE
      REWIND IOU3
      READ (IOU,670) FMSTR,GF(1),ALFA,YI,DRAG,YO=(YI-1.0)*SCALE+YA
      DRAG=DRAG*3.1415927*SCALE**2/WINGA
      IF (ISTART.EQ.0) REWIND IOU3
      IF (ISTART.NE.0.OR.KP4.LE.0) GO TO 70
      WRITE (IOU3,800) (LIT(I),I=1,18),FMSTR,GF(1),ALFA
      WRITE (IOU3,740) ISURF,LINE,ILL,KURE,MESS,INCRES,NPC,K1
      WRITE (IOU3,780) SINE,COSINE,S2,C2,DYC,STEP,YO,DRAG,ALIFT,TORQUE
      IF (ISTART) 120,130,80
      DO 100 I=1,ISTART
      READ (IOU3,640) DUM
      IF (KPRINT(3).EQ.3) WRITE (IOU6,640) DUM
      READ (IOU3,770) ISURF,LINE,ILL,KURE,MESS,INCRES,NPC,K1
      IF (KPRINT(3).NE.0) WRITE (IOU6,680) ISURF,LINE,NPC,K1
      READ (IOU3,780) SINE,COSINE,S2,C2,DYC,STEP,YO,DRAG,ALIFT,TORQUE
      READ (IOU3,640) DUM
      IF (IFT.LT.0) INCRES=-IFT
      IF (IFT.GT.1) INCRES=1-IFT
      IF (ISURF.EQ.1) GO TO 130
      KOUNT=LINE*(NPC+2)+100
      DO 90 J=1,KOUNT
      READ (IOU3,640) DUM
      IF (KPRINT(3).EQ.3) WRITE (IOU6,640) DUM
      IF (EOF(IOU3)) 100,90
      CONTINUE
      CONTINUE
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110 WRITE (IOU6,760) ISURF,ISTART
120 CALL EXIT
130 READ (IOU5,680) ISURF,LIME,ILL,KURE,MESS,INCRES,NPC,K1
    READ (IOU5,690) SINE,COSINE,S2,C2,DYC,STEP,Y0,DRAG,ALIFT,TORQUE
    N1=ISURF+1
    N2=NPCT+1
    N3=NPCT+3
    WRITE (IOU6,700) FMSTR,GF(1),ALFA,DRAG,ALIFT,TORQUE
    DO 170 I=1,LIME
    IF (ISTART.GT.0) READ (IOU3,640) DUM
    IMO=2
    IF (I.EQ.1) IMO=1
    IF (I.EQ.LIME) IMO=3
    IF (ISTART.GT.0) READ (IOU3,640) DUM
    DO 160 J=2,N2
    IF (ISTART.LE.0) READ (IOU,710) A(J,3),A(J,1),A(J,7),A(J,8),THETA,
1PSI
    IF (ISTART.GT.0) READ (IOU3,790) A(J,3),A(J,1),A(J,7),A(J,8),THETA
1,PSI
    THETA=THETA/RAD
    PSI=PSI/RAD
    A(J,7)=A(J,8)/(1.+GF(2)*A(J,7)**2)**GF(6)
    IF (ISTART.NE.0) GO TO 140
    A(J,1)=A(J,1)*SCALE
    A(J,3)=A(J,3)*SCALE+ZA
    A(J,2)=Y0
    Q=SQRT(1.-(A(J,7)/A(J,8))**GF(7))
    QS=Q*SIN(THETA)
    A(J,4)=Q*COS(PSI)
    A(J,5)=Q*COS(THETA)
    A(J,6)=Q*SIN(PSI)
    DO 150 K=1,4,3
    CALL ROTATE (A(J,K),A(J,K+1),SINE,COSINE)
    CALL DATOUT (A,J,IMO,KAB,0)
    CALL DATOUT (A,J,IMO,KAB,1)
    WRITE (NTAPE) ((A(J,L),L=1,8),J=2,N2)
    IF (ISTART.EQ.0.AND.KP4.GT.0) END FILE IOU3
    IF (ISTART.LE.0) GO TO 180
    READ (IOU3,640) DUM
    IF (EOF(IOU3)) 180,110
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180 DO 630 I=N1,NSURF
    ITEST=0
    KTEST=0
    ISURF=I
    NLINE=LINE+INCRES
    DYC=(DYC+DYC*STEP)*FLOAT(LINE)/FLOAT(NLINE)
    IF(YO.LE.WINGST-.5.AND.(WINGST.LE.YO+DYC.AND.YO+DYC.LE.WINGST
1      +1.)) DYC=WINGST-.01-YO
    IF (STEP.LT.0.00) MESS=1
    STEP=.05
    IPRINT=0
    IF (1.EQ.NS) IPRINT=KPRINT(3)
    DO 210 K=1,NR
        NPCC=NPSET(9*(K-1)+1)
        DO 200 J=1,8
            L1(J)=NPSET(9*(K-1)+J+1)
            IF (YO+DYC.LT.YSET(K).OR.NPSET(9*K+1).EQ.0) GO TO 220
        CONTINUE
        IF (NPC.EQ.NPCC.AND.(L1(1).EQ.K1(1).AND.L1(2).EQ.K1(2))) 230,250
        IF (L1(3).EQ.K1(3).AND.(L1(4).EQ.K1(4).AND.L1(5).EQ.K1(5))) 240,
1250
        IF (L1(6).EQ.K1(6).AND.(L1(7).EQ.K1(7).AND.L1(8).EQ.K1(8))) 290,
1250
        DYC=DYC+FLOAT(2*NPCC-2+K1(1)-K1(2)+K1(3)-K1(4)+K1(5)-K1(6)+K1(7)-K1
1(8))/FLOAT(2*NPCC-2+L1(1)-L1(2)+L1(3)-L1(4)+L1(5)-L1(6)+L1(7)-L1(8
2))
        IF (K1(5).EQ.0.AND.L1(5).NE.0) DYC=DYC/FLOAT(K8+1)
        IF (YO+DYC.GE.YSET(K-1)) GO TO 270
        NPCC=NPSET(9*(K-2)+J+1)
        DO 260 J=1,8
            L1(J)=NPSET(9*(K-2)+J+1)
        DO 280 K=1,8
            K1(K)=L1(K)
        IF (YO.GT.WINGST-0.5.AND.(WINGST.LE.YO+DYC.AND.YO+DYC.LE.WINGST
1      +1.)) DYC=WINGST+1.-YO
        MESS=1
        REWIND LTape
        REWIND NTape
        INDEX=-1
        CALL FIGURE (O.,YO,O.,F,A1,81,C1)
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INDEX=-2
IF ((Y0+DYC.LE.YSTOP).OR.(ABS(YSTOP-Y0).LT.0.0002)) GO TO 300
DYC=YSTOP-Y0
KP4=-10000
CALL FIGURE (O.,Y0+DYC,O.,F,A1,B1,C1)
IF (ITEST.EQ.KTEST) GO TO 310
IF (ITEST.GT.10) CALL EXIT
KTEST=ITEST
GO TO 380
300  LTAPE=LN-LTAPE
      NTAPE=LN-NTAPE
      IF (MESS.EQ.O.AND.INCRES.EQ.O) GO TO 330
      DO 320 K=1,LINE
      READ (LTAPE) ((A(L,M),M=1,8),L=1,NPC)
      IF (K.EQ.1) AM=.5*(A(1,3)+A(NPC,3))
      CALL TIDYUP (SINE,COSINE,A,NPC,NPCC,AM,K)
      WRITE (NTAPE) ((A(L,M,2),M=1,8),L=1,NPCC)
      WRITE (IOU6,750) I
      NPC=NPCC
      N2=NPCC+1
      N3=NPCC+3
      CALL REFORM (A,LTAPE,NTAPE,NPC,LINE,NLINE)
      INCRES=0
      MESS=0
      GO TO 290
330  IF (KURE.NE.ILL) 350,380
340  REWIND LTAPE
      REWIND NTAPE
350  WRITE (IOU6,730) ILL,I
      IF (ILL.GT.16) CALL EXIT
      KURE=ILL
      CALL ROTATE (SINE,COSINE,SN,CS)
      S2=2.*SINE*COSINE
      C2=COSINE*COSINE-SINE*SINE
      DO 370 J=1,LINE
      READ (LTAPE) ((A(L,K),K=1,8),L=2,N2)
      DO 360 K=2,N2
      DO 360 L=1,4,3
      CALL ROTATE (A(K,L),A(K,L+1),SN,CS)
      WRITE (NTAPE) ((A(L,K),K=1,8),L=2,N2)
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380 REWIND LTAPE
    REWIND NTAPE
    LTAPE=LN-LTAPE
    NTAPE=LN-NTAPE
    IF (KP4.LE.1.OR.1/KP4*KP4.EQ.1) WRITE (IOU6,720) 1
    CALL SETCP (LTAPE,1,A,8,SINE,COSINE,POP,GF,FMSTR,N2)
    IF (STEPH.NE.0.) DYC=AMINI (DYC,STEPH)
    DO 570 J=1,LINE
    REWIND INCASE
    WRITE (INCASE,830)
    IND=2
    IF (J.EQ.1) IND=1
    IF (J.EQ.LINE) IND=3
    IF (IND=2) 390,430,460
    DO 400 M=3,4
    READ (LTAPE) ((A(K,L,M),L=1,8),K=2,N2)
    IF (DYC.GT.1.E-6) GO TO 410
    DYC=AMINI (ABS(A(2,3,3)-A(2,3,4)),ABS(A(3,1,3)-A(2,1,3)))
    XM2=(1.*(A(2,8,3)/A(2,7,3))*GF(7)-1.)/GF(2)
    DYC=DYC+.6*SORT(XM2-1.)
    CALL MIRROR (A(1,1,3),S2,C2,N2)
    DO 420 K=2,NPC
    IF (.6*(A(K,1,4)-A(K,1,3))*2+(A(K,2,4)-A(K,2,3))*2+(A(K,3,4)-A(
    K,3,3))*2).LT.(A(K,1,3)-A(K+1,1,3))*2+(A(K,2,3)-A(K+1,2,3))*2+(
    2A(K,3,3)-A(K+1,3,3))*2) GO TO 450
    CONTINUE
    INCRES=1
    GO TO 450
430 DO 440 K=1,N3
    DO 440 L=1,8
    A(K,L,2)=A(K,L,3)
    A(K,L,3)=A(K,L,4)
    READ (LTAPE) ((A(L,K,4),K=1,8),L=2,N2)
    CALL MIRROR (A(1,1,4),S2,C2,N2)
    GO TO 480
440 DO 470 K=3,4
    DO 470 L=1,N3
    DO 470 M=1,4,3
    YTEMP=SINE*A(L,M,K)+COSINE*A(L,M+1,K)
    A(L,M,K-1)=COSINE*A(L,M,K)-SINE*A(L,M+1,K)

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470 A(L,M+1,K-1)=COSA*YTEMP+SINA*A(L,M+2,K)
480 A(L,M+2,K-1)=-SINA*YTEMP+COSA*A(L,M+2,K)
      A(L,M/4+7,K-1)=A(L,M/4+7,K)
      DO 500 K=2,MZ
      IPRINT=0
      IF (I.NE.NS) GO TO 490
      IPRINT=KPRINT(1)
      IF (J.NE.NL) GO TO 490
      IPRINT=KPRINT(2)
      IF (K.NE.MP+1) GO TO 490
      IPRINT=KPRINT(3)
      CALL BULK (K,IND)
      IF (ITEST.NE.KTEST) GO TO 190
      IF (KURE.NE.ILL) GO TO 340
      IF (IND.NE.3) CALL DATOUT (A,K,IND,KAB,0)
      KAY=K-1
      WRITE (INCASE,840) KAY,J
      CONTINUE
500 IF (IND.NE.3) WRITE (NTAPE) ((A(L,K),K=1,8),L=2,N2)
      IF (IND-2) 540,570,510
510 CALL HARNES (QINF,A,NPC)
      REWIND INCASE
      END FILE INCASE
      DO 530 K=2,4
      N=K
      IF (K.EQ.4) N=1
      DO 530 L=1,N3
      IF (K.EQ.4.AND.(L.EQ.1.OR.L.EQ.N3)) GO TO 530
      DO 520 M=1,4,3
      A(L,M/4+7,K)=A(L,M/4+7,N)
      YTEMP=COSA*A(L,M+1,N)-SINA*A(L,M+2,N)
      A(L,M+2,K)=SINA*A(L,M+1,N)+COSA*A(L,M+2,N)
      A(L,M+1,K)=-SINE*A(L,M,N)+COSINE*YTEMP
      A(L,M,K)=COSINE*A(L,M,N)+SINE*YTEMP
      CONTINUE
520 GO TO 570
530 LB=2
540 IF (K1(1).NE.0) LB=K1(1)+1
      LE=NPIC
      IF (K1(2).NE.0) LE=K1(2)

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DO 560 L=LB,LE
ARC=(A(L+1,1)-A(L,1))*2+(A(L+1,2)-A(L,2))*2+(A(L+1,3)-A(L,3))*2
IF (L.NE.LB) GO TO 550
BIG=ARC
SMALL=ARC
BIG=AMAX1(BIG,ARC)
SMALL=AMIN1(SMALL,ARC)
IF (2.*SMALL.LE.BIG) MESS=1
CONTINUE
DO 590 J=2,N2
DO 580 K=1,8
A(J,K)=A(J,K,4)
CALL DATOUT (A,J,3,KAB,0)
CONTINUE
IF (KP4.GT.0.OR.(KP4.EQ.0.AND.I/10*10.EQ.1)) WRITE (10U3,720) I
WRITE (10TAPE) ((A(J,L),L=1,8),J=2,N2)
CALL SETCP (10TAPE,2,A,B,SINE,COSINE,POP,GF,FMSTR,N2)
CALL AERO (NPC,SINA,COSA)
REWIND 10TAPE
READ (10TAPE) A(1),A(2)
YO=SINE*A(1)+COSINE*A(2)
IF (KP4.EQ.0.AND.I/10*10.NE.1) GO TO 600
WRITE (10U1,740) I,LINE,ILL,KURE,MESS,INCRS,NPC,K1
WRITE (10U1,780) SINE,COSINE,S2,C2,DYC,STEP,YO,DRAG,ALIFT,TORQUE
IF (1/KAB*KAB.NE.1.AND.KP4.NE.0) GO TO 610
IF (KP4.GE.0) WRITE (10U6,740) I,LINE,ILL,KURE,MESS,INCRS,NPC,K1
IF (KP4.LT.0) WRITE (10U7,680) I,LINE,ILL,KURE,MESS,INCRS,NPC,K1
IF (KP4.GE.0) WRITE (10U6,780) SINE,COSINE,S2,C2,DYC,STEP,YO,DRAG,
1ALIFT,TORQUE
IF (KP4.LT.0) WRITE (10U7,690) SINE,COSINE,S2,C2,DYC,STEP,YO,DRAG,
1ALIFT,TORQUE
IF (KP4.LT.1.AND.1/KAB*KAB.NE.1) GO TO 630
REWIND 10TAPE
DO 620 J=1,LINE
READ (10TAPE) ((A(K,L),L=1,8),K=2,N2)
IND=2
IF (J.EQ.1) IND=1
IF (J.EQ.LINE) IND=3
DO 620 K=2,N2
CALL DATOUT (A,K,IND,KAB,1)

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630 IF (KP4.GT.0.OR.(KP4.EQ.0.AND.1/10*10.EQ.1)) END FILE IOU3
      CONTINUE
      CALL EXIT
      C
      C
      C
640 FORMAT (18A4)
650 FORMAT (F10.5,12I5)
660 FORMAT (1M140X36NORTHROP SUPERSONIC FLOW FIELD PROGRAM//30X18A4)
670 FORMAT (8F10.5)
680 FORMAT (16I5)
690 FORMAT (4E15.8)
700 FORMAT (1M039X40M 3-DIMENSIONAL CHARACTERISTICS SOLUTION /1M05X,24
      1MFREESTREAM MACH NUMBER =,F7.3,5X25HRATIO OF SPECIFIC HEATS =,F6.3
      2,5X17HANGLE OF ATTACK =,F7.3,8H DEGREES/1M049X21INITIAL VALUE SUR
      3FACE,I2,6MORAG =,G14.7/T2,6HLIFT =,G14.7/T2,8HMOMENT =,G14.7)
710 FORMAT (2E15.8,F10.7,E15.8,F12.8,F13.8)
720 FORMAT (1M150X15HDATA SURFACE NO,I3/93H0**TO USE THIS AS AN INITI
      1AL VALUE SURFACE, KEY PUNCH FIRST 6 COLUMNS OF DATA AS INPUT CARDS
      2)
730 FORMAT (13M011NATURED PSI AND DELTA,CASE NO,I3,42H, ROTATE COORDI
      1NATES AND RECOMPUTE SURFACE,I3)
740 FORMAT (61MOTO USE AS IVS, PUNCH THE 4 CARDS, PLACE BEFORE BODY PT
      1 CARDS/1X,9(1M0),10(1M1),10(1M2),10(1M3),10(1M4),10(1M5),10(1M6),
      210(1M7),1M8/1X,8(10M1234567890)//1X,20I5)
750 FORMAT (42M0DATA POINTS WILL BE RE-SPACED FOR SURFACE,I3)
760 FORMAT (13M0WRONG IVS NOI4,4H, NOI4,27H SPECIFIED OR FAIL END FILE
      1)
770 FORMAT (1X/////1X,20I5)
780 FORMAT (1X,4E15.8)
790 FORMAT (1X,2E15.8,F10.7,E15.8,F12.8,F13.8)
800 FORMAT (1M1,30X18A4,/1M05X24HFREESTREAM MACH NUMBER =F7.3,5X25HRAT
      110 OF SPECIFIC HEATS =F6.3,5X,17HANGLE OF ATTACK =F7.3,8H DEGREES)
810 FORMAT (12,5E15.8,F2.0)
820 FORMAT (1X,I2,1P5E15.8,I2)
830 FORMAT (1M1,40X,41M* * * * * * * * * * * * * * * * * /41X,
      141H* * /41X,41M* * * * * * * * * * * * * * * * * IN THE
      2EVENT OF FAILURE * /41X,41H* * * * * * * * * * * * * * * * * HE
      3 * /41X,41H* I WAS DOING O. K. * /41X,41H* HE GOOFS I
      4H* NOT SO--THE NEXT GUY.

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5N EVERY POSSIBLE WAY. */41X,41H* I WAS DOING O. K. A 397
 6 */41X,41H* BUT THINGS WENT ASTRAY. */41X,41H* A 398
 7 NOW THE LISTING CAN TESTIFY: */41X,41H* I WAS DOING O. A 399
 8 K. */41X,41H* NOT SO--THE NEXT GUY. A 400
 9 */41X,41H* */41X,41H* A 401
 A * A 402
 * A 403
 840 FORMAT (41X,17H I AM POINT NO,13,11H OF LINE NO,13) A 404
 END


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C      SUBROUTINE BULK (L,IND)
C      IND = 1 FOR BODY, 2 FOR FIELD, 3 FOR SHOCK
C****  TAKE NOTE THAT SINE,COSINE MUST CORRESPOND TO CURRENT COORDINATES
COMMON /TEST/ LOT(4),ITEST,STEP,KTEST
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DIHETA,DPSI
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
COMMON /CONT/ NPC,DVC,ILL,KURE,SINE,CGSINE
COMMON /ESENS/ XC,YC,ZC,UC,VC,WG,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
      IPS,HUB(8)
COMMON /BSPT/ XBS(4),YBS(4),ZBS(4),UBS(4),VBS(4),WBS(4),PBS(4),
      IPPBS(4),TPBS(4),PSBS(4)
COMMON /STOR/ H(4,8),XAL(99),YAL(99),ZAL(99),UAL(99),VAL(99),WAL(
      99),PAL(99),PPMAL(99)
      DIMENSION XYZ(3,7)
      EQUIVALENCE (XC,XYZ)
      IF (IPRINT.GE.1) 20,30
      IF (IND.EQ.1) WRITE (IOU6,150)
      IF (IND.EQ.2) WRITE (IOU6,140)
      IF (IND.EQ.3) WRITE (IOU6,160)
      N=4-MOD(IND,2)
      CALL PICK (L,IND)
      IF (KURE.NE.ILL) RETURN
      C      BACK TO MAIN PROGRAM, ROTATE Y AXIS AWAY FROM FLOW FIELD
      UC=HUB(4)
      VC=HUB(5)
      WC=HUB(6)
      PC=HUB(7)
      PPMC=HUB(8)
      THETAC=TH
      PSIC=PS
      DO 40 I=1,4
      LOT(I)=0
      DO 120 I=1,25
      IF (IPRINT.GE.1) WRITE (IOU6,170) I
      IF (IND.NE.3) GO TO 50
      Q=SQRT(1.-(PC/PPMC)**GF(7))
      CALL NORM (-UC*Q,QINF-VC*Q,-WG*Q,A,B,C)
      IF (I.EQ.1) CALL NORM (A,B,C,A1,B1,C1)
      CALL NORM (A+A1,B+B1,C+C1,A,B,C)
      IF (IPRINT.GE.1) WRITE (IOU6,220) A,B,C,A1,B1,C1

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      A4=-A*B      41
      B4=1.-B*B    42
      C4=-C*B      43
      BM=COSA*B4-SINA*C4 44
      AB=(SINA*B4+COSA*C4)/BM 45
      XC=HUB(1)+DYC*A4/BM 46
      YC=HUB(2)+DYC*(COSA+SINA*AB) 47
      ZC=HUB(3)+DYC*(-SINA+COSA*AB) 48
      GO TO 60      49
50      A4=UC+HUB(4) 50
      B4=VC+HUB(5) 51
      C4=WC+HUB(6) 52
      BM=SINE*A4+COSINE*B4 53
      AB=(COSINE*A4-SINE*B4)/BM 54
      XC=HUB(1)+DYC*(SINE+COSINE*AB) 55
      YC=HUB(2)+DYC*(COSINE-SINE*AB) 56
      ZC=HUB(3)+DYC*C4/BM 57
60      IF (IPRINT-GE.1) WRITE (IOU6,220) A4,B4,C4,BM,AB,XC,YC,ZC 58
      IF (IND-NE.1) GO TO 70 59
      CALL GENTRY (SINE,COSINE,XC,YC,ZC,A4,B4,C4) 60
      IF (IPRINT-GE.1) WRITE (IOU6,220) XC,YC,ZC,A4,B4,C4 61
      CALL TRANS (H,X,Y,Z,A4,B4,C4,1.,1) 62
      CALL BASEPT (IND) 63
      IF (ITEST-EQ.KTEST-OR.LOT(4)-NE.5) GO TO 80 64
      H(4,1)=XAL(L) 65
      H(4,2)=YAL(L) 66
      H(4,3)=ZAL(L) 67
      CALL NORM (UAL(L),VAL(L),WAL(L),M(4,4),M(4,5),H(4,6)) 68
      H(4,7)=PAL(L) 69
      H(4,8)=PPMAL(L) 70
      KTEST=ITEST 71
      GO TO 70      72
80      IF (KURE-NE.ILL-OR.ITEST-NE.KTEST) RETURN 73
      IF (IPRINT-GE.1) WRITE (IOU6,180) (J,XBS(J),YBS(J),ZBS(J),PBS(J), 74
      1PPMBS(J),THBS(J),PSBS(J),UBS(J),VBS(J),WBS(J),J=1,N) 75
      CALL COEFS (IND) 76
      IF (KURE-NE.ILL) RETURN 77
      IF (IND-EQ.1) CALL SOL (COF(4),COF(6),COF(5),COF(1),COF(6),COF(9), 78
      1COF(8),COF(3),0.,0.,1.,1.5707963267949,PC,PSIC,THETAC) 79
      IF (IND-EQ.2) CALL SOL (COF(4),COF(5),COF(6),COF(1),COF(5),COF(7), 80

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1COF(8),COF(2),COF(6),COF(8),COF(9),COF(3),PC,THETAC,PSIC)
IF (IND.EQ.3) CALL COMPAT
SINTH=SIN(THETAC)
UC=SINTH*COS(PSIC)
VC=COS(THETAC)
WC=SINTH*SIN(PSIC)
IF (IND.EQ.1) CALL TRANS (H,XYZ,A4,B4,C4,-1.,1)
IF (UC*UC+WC*WC.GE.4.E-06) GO TO 90
ILL=ILL+1
RETURN
90 IF (IPRINT.GE.1) WRITE (IOU6,190) I,XC,YC,ZC,PC,PPMC,UC,VC,WC,
1THETAC,PSIC
IF (L.NE.2.AND.L.NE.NPC+1) GO TO 100
UT=SINE*UC+COSINE*VC
IF (IND.NE.3) CALL NORM (SINE*UT,COSINE*UT,WC,UC,VC,WC)
IF (IND.EQ.3) CALL NORM (O.,VC,WC,UC,VC,WC)
IF (1.EQ.1) GO TO 110
IF (ABS(THETAC-THTEMP).GT.DTHETA) GO TO 110
IF (ABS(PSIC-PSTEMP).GT.OPSI) GO TO 110
IF (ABS((PC-PTEMP)/PC).LE.DP) GO TO 130
THTEMP=THETAC
PSTEMP=PSIC
PTEMP=PC
WRITE (IOU6,200)
CALL EXIT
L1=L-1
130 IF (IPRINT.GE.1) WRITE (IOU6,210) L1
Q=SQRT(1.--(PC/PPMC)*GF(7))
XAL(L)=XC
YAL(L)=YC
ZAL(L)=ZC
UAL(L)=Q*UC
VAL(L)=Q*VC
WAL(L)=Q*WC
PAL(L)=PC
PPMAL(L)=PPMC
RETURN
C
C
C

```

| | | |
|-----|---|-------|
| 140 | FORMAT (18H0***** FIELD *****) | B 121 |
| 150 | FORMAT (17H0***** BODY *****) | B 122 |
| 160 | FORMAT (18H0***** SHOCK *****) | B 123 |
| 170 | FORMAT (1H0,20X,32HBASE POINT PROPERTIES, ITERATION,I3) | B 124 |
| 180 | FORMAT (15H0I,X,Y,Z,P,PPM=,15,5E18.8/17H THETA,PSI,U,V,W=,3X5E18.8 | B 125 |
| | 1) | B 126 |
| 190 | FORMAT (41H0NEW BULK POINT PROPERTIES, ITERATION NO.,I3/1H 21X,2HX | B 127 |
| | 1C,18X,2HVC,18X,2HZC,18X,2HPC,17X,4HPPMC/1H ,10X,5E20.8/1H ,21X,2MU | B 128 |
| | 2C,18X,2HVC,18X,2HWC,16X,6HTHETAC,15X,4HPSIC/1H ,10X,5E20.8) | B 129 |
| 200 | FORMAT (54H0BULK POINT HAS FAILED TO CONVERGE AFTER 25 ITERATIONS) | B 130 |
| 210 | FORMAT (24H0***** BULK POINT NO.,I3,23H HAS CONVERGED *****) | B 131 |
| 220 | FORMAT (8E15.7) | B 132 |
| | END | B 133 |

| | | |
|----|---|--|
| 1 | C | |
| 2 | C | |
| 3 | C | |
| 4 | C | |
| 5 | C | |
| 6 | C | |
| 7 | C | |
| 8 | C | |
| 9 | C | |
| 10 | C | |
| 11 | C | |
| 12 | C | |
| 13 | C | |
| 14 | C | |
| 15 | C | |
| 16 | C | |
| 17 | C | |
| 18 | C | |
| 19 | C | |
| 20 | C | |
| 21 | C | |
| 22 | C | |
| 23 | C | |
| 24 | C | |
| 25 | C | |
| 26 | C | |
| 27 | C | |
| 28 | C | |
| 29 | C | |
| 30 | C | |
| 31 | C | |


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SUBROUTINE PICK (L,IND)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHETA,DPSI
COMMON /ESENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
1PS,HUB(8)
COMMON /STOR/ H(4,8),ALMUS(99,8,4)
LP=L+1
LM=L-1
N=2
IF (IND.EQ.2) N=4
DO 20 I=1,8
HUB(I)=ALMUS(L,I,3)
IF (IND.NE.3) H(2,I)=ALMUS(L,I,4)
IF (IND.NE.1) H(N,I)=ALMUS(L,I,2)
H(1,I)=ALMUS(LM,I,3)
H(3,I)=ALMUS(LP,I,3)
CALL NORM (HUB(4),HUB(5),HUB(6),HUB(4),HUB(5),HUB(6))
IF (HUB(4)**2+HUB(6)**2.GT.4.E-06) GO TO 30
ILL=ILL+1
RETURN
TH=ACOS(HUB(5))
PS=ATAN2(HUB(6),HUB(4))
IF (IND.NE.2) N=3
DO 40 I=1,N
CALL NORM (H(I,4),H(I,5),H(I,6),H(I,4),H(I,5),H(I,6))
IF (IPRINT.GE.2) WRITE (IOU6,50) HUB,((H(I,J),J=1,8),I=1,N),TH,PS
RETURN
50
FORMAT (17H0***** PICK *****/(8E15.7))
END

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SUBROUTINE BASEPT (IND)
COMMON /TEST/ LOT(4),ITEST,STEP,KTEST,KPRINT(3)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTA,DPSI
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7)
COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE,ISURF,YO,ISTART,WINGST
COMMON /ESENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
1PS,HUB(8)
COMMON /BSPT/ XBS(4),YBS(4),ZBS(4),UBS(4),VBS(4),WBS(4),PBS(4),
2LPPMBS(4),TPBS(4),PSBS(4)
COMMON /STOR/ XH(4),YH(4),ZH(4),UH(4),VH(4),WH(4),PH(4),PPMH(4)
3IF (IPRINT.GE.2) WRITE (IOU6,160)
4XD=XC-HUB(1)
5YD=YC-HUB(2)
6ZD=ZC-HUB(3)
7B2=XD*XD+YD*YD+ZD*ZD
8ROOT=GF(2)/((PPMC/PC)**GF(7)-1.0)
9IF (ROOT.GT.0.) GO TO 10
10WRITE (IOU6,120) PPMC,PC
11CALL EXIT
12AMU4=ASIN(SQRT(ROOT))
13IF (IPRINT.GE.2) WRITE (IOU6,170) XD,YD,ZD,AMU4
14LID=3
15IF (IND.EQ.2) LID=4
16N=1
17IF (LOT(4).EQ.5) N=4
18DO 100 I=N,LID
19XD1=XH(1)-HUB(1)
20YD1=YH(1)-HUB(2)
21ZD1=ZH(1)-HUB(3)
22IF (IPRINT.GE.2) WRITE (IOU6,180) I
23A2=XD1*XD1+YD1*YD1+ZD1*ZD1
24AB=XD*XD1+YD*YD1+ZD*ZD1
25IF (IPRINT.GE.2) WRITE (IOU6,170) XD1,YD1,ZD1
26DO 70 J=1,50
27IF (J.EQ.1) FL=0.
28IF (J.EQ.1) GO TO 60
29COS2=COS(.5*(AMU4+AMU4))**2
30CALL NORM (.5*(UBS(1)+UC),.5*(VBS(1)+VC),.5*(WBS(1)+WC),U,V,W)
31BV=XD*U+YD*V+ZD*W
32AV=XD1*U+YD1*V+ZD1*W
33
34
35
36
37
38
39
40

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10

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41 FL=0.
42 A=A2*CO52-AV*AV
43 B=AB*CO52-AV*BV
44 C=C2*CO52-BV*BV
45 TERM=B*B-A*C
46 IF (TERM.LT.0.) GO TO 110
47 IF (A.LE.0..AND.B.GT.0.) GO TO 110
48 IF (C) 20,50,20
49 FL=C/(B-SQRT(TERM))
50 IF (IPRINT.GE.2) WRITE (IOU6,170) COS2,BV,AV,U,V,W,A,B,C,TERM,FL,
51 1A2,AB
52 IF (LOT(1),NE.0.OR.(FL.GE.0..AND.FL.LE..7)) GO TO 30
53 IF (KPRINT(3).GT.0) WRITE (IOU6,130) I,FL
54 LOT(I)=I
55 IF (I.NE.4) STEP=-.1
56 IF (FL.GE.-0.1..AND.FL.LE.1.1) GO TO 50
57 IF (I.NE.4).OR.(KPRINT(3).GT.0) WRITE (IOU6,190) I,FL
58 IF (N.EQ.4.OR.(WINGST.LE.VO..AND.VO.LE.WINGST+1.)) GO TO 50
59 ITEST=ITEST+1
60 IF (I.EQ.4) LOT(4)=5
61 RETURN
62 XBS(1)=HUB(1)+FL*XD1
63 YBS(1)=HUB(2)+FL*YD1
64 ZBS(1)=HUB(3)+FL*ZD1
65 UBS(1)=HUB(4)+FL*(UM(1)-HUB(4))
66 VBS(1)=HUB(5)+FL*(VM(1)-HUB(5))
67 WBS(1)=HUB(6)+FL*(WM(1)-HUB(6))
68 PBS(1)=HUB(7)+FL*(PM(1)-HUB(7))
69 PPMBS(1)=HUB(8)+FL*(PPMH(1)-HUB(8))
70 CALL NORM (UBS(1),VBS(1),WBS(1),PBS(1),UBS(1),VBS(1),WBS(1))
71 AMU=ASTN(SQRT(GF(2)/(PPMBS(1)/PBS(1))*GF(7)-1.))
72 IF (IPRINT.GE.2) WRITE (IOU6,170) U,V,W,A,B,C,TERM,FL,AMU,PBS(1),
73 1PPMBS(1),HUB(7),WM(1),HUB(8),PPMH(1)
74 IF (J.EQ.1) GO TO 70
75 IF (FL.GT.1.) GO TO 80
76 IF (ABS(AMU-AMU0).LE.EPSLN) GO TO 80
77 AMU0=AMU
78 WRITE (IOU6,150) I
79 CALL EXIT
80 IF (UBS(1)*2+WBS(1)*2.GT.4.E-06) GO TO 90

```

| | | |
|-----|---|-----|
| 90 | ILL=ILL+1 | 81 |
| | RETURN | 82 |
| | THS(I)=ACOS(VBS(I)) | 83 |
| | PSBS(I)=ATAN2(MBS(I),UBS(I)) | 84 |
| | IF (PSBS(I).LT.-3.) PSBS(I)=PSBS(I)+6.2831853072 | 85 |
| 100 | CONTINUE | 86 |
| | IF (N.EQ.4) LOT(4)=0 | 87 |
| | RETURN | 88 |
| 110 | WRITE (10U6,140) I,A,B,C,TERM | 89 |
| | IF (I.NE.4.OR.N.EQ.4) CALL EXIT | 90 |
| | GO TO 40 | 92 |
| C | | 93 |
| C | | 94 |
| C | | 95 |
| 120 | FORMAT (//24H FLOW SUBSONIC, PPMC,PC=,2G15.7) | 96 |
| 130 | FORMAT (11H BASE POINT,12,13H VIOLATES CFL,F10.5) | 97 |
| 140 | FORMAT (31H0INTERSECTION FAILURE, BASEPT NO,12,4E18.8) | 98 |
| 150 | FORMAT (43H0MACH CONE CONVERGENCE FAILURE IN BASEPT NO,12) | 99 |
| 160 | FORMAT (19H0***** BASEPT *****) | 100 |
| 170 | FORMAT (8E15.7) | 101 |
| 180 | FORMAT (14H0BASE POINT NO,12) | 102 |
| 190 | FORMAT (0H BASE PT,12,13H EXTRAPOLATES,F10.5,16H, STEP DECREASED) | 103 |
| | END | 104 |


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C
SUBROUTINE COEFS (IND)
  IND = 1 FOR BODY, 2 FOR FIELD, 3 FOR SHOCK
  COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTA,DPSI
  COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
  COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE
  COMMON /ESENS/ XC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC,A4,B4,C4,TH,
    IPS,HUB(8)
  COMMON /BSP/ XBS(4),YBS(4),ZBS(4),UBS(4),VBS(4),WBS(4),PBS(4),
    LPPMBS(4),THBS(4),PSBS(4)
  DIMENSION DX(4),DY(4),DZ(4),DTH(4),DPS(4),A(4),B(4),C(4),D(4)
  IF (IPRINT.GE.2) WRITE (IOU6,80)
10  N=4
    IF (IND.EQ.2) GO TO 20
    N=3
    DX(4)=XC-HUB(1)
    DY(4)=YC-HUB(2)
    DZ(4)=ZC-HUB(3)
    DTH(4)=THETAC-TH
    DPS(4)=PSIC-PS
    AMUC=ASIN(SQRT(GF(2)/(1+PPMC/PC)*GF(7)-1.))
    DO 30 I=1,N
      DX(I)=XC-XBS(I)
      DY(I)=YC-YBS(I)
      DZ(I)=ZC-ZBS(I)
      DTH(I)=THETAC-THBS(I)
      DPS(I)=PSIC-PSBS(I)
      IF (IPRINT.GE.2) WRITE (IOU6,90) DX(I),DY(I),DZ(I),DTH(I),DPS(I)
      CONTINUE
    DO 50 I=1,N
      CALL NORM (.5*(UBS(I)+UC),.5*(VBS(I)+VC),.5*(WBS(I)+WC),UNT,VNT,
        1WNT)
      IF (IPRINT.GE.2) WRITE (IOU6,90) UNT,VNT,WNT
      J=MOD(I,4)+1
      K=MOD(I-5,4)+4
      CALL SOL (DX(I),DY(I),DZ(I),DTH(I),DX(J),DY(J),DZ(J),DTH(J),DX(K),
        1DY(K),DZ(K),DTH(K),DTHDX,DTHDY,DTHDZ)
      CALL SOL (DX(I),DY(I),DZ(I),DPS(I),DX(J),DY(J),DZ(J),DPS(J),DX(K),
        1DY(K),DZ(K),DPS(K),DPSDX,DPSDY,DPSDZ)
      CALL NORM (WNT*DZ(I)-WNT*DY(I),WNT*DX(I)-UNT*DZ(I),UNT*DY(I)-VNT*
        1DX(I),DXDN,DYDN,DZDN)
20
30

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41 DTHDN=DTHDX*DXDN+DTHDY*DYDN+DTHDZ*DZDN
42 DPSON=DP SDX*DXDN+DP SDY*DYDN+DP SDZ*DZDN
43 IF (IPRINT.GE.2) WRITE (IOU6,90) DXDN,DYDN,DZDN,DTHDN,DPSON
44 VCHEK=SQRT(UNT*UNT+WNT*WNT)
45 IF (VCHEK.GT.2.E-3) GO TO 40
46 ILL=ILL+1
47 RETURN
48 COSDI=(UNT*DZDN-WNT*DXDN)/VCHEK
49 IF (ABS(COSDI).GT.1.) COSDI=SIGN(1.,COSDI)
50 UZWX=UNT*DX(1)-WNT*DY(1)
51 SINDI=SIGN(SQRT(1.-COSDI*COSDI),UZWX)
52 AMUAV=-5*(AMUC+ASIN(SQRT(GF(2)/(PPMBS(1)/PBS(1))*GF(7)-1.)))
53 SINMU= SIN(AMUAV)
54 SINTH= SIN(.5*(THETAC+THBS(1)))
55 DL=SQRT(DX(1)*DX(1)+DY(1)*DY(1)+DZ(1)*DZ(1))
56 IF (IPRINT.GE.2) WRITE (IOU6,90) AMUAV,SINMU,SINTH,SINDI,COSDI,DL
57 A(1)=SINMU*COS(AMUAV)/(GF(1)*.5*(PC+PBS(1)))
58 B(1)=-COSDI
59 C(1)=SINTH*SINDI
60 D(1)=A(1)*PBS(1)+B(1)*THBS(1)+C(1)*PSBS(1)-DL*SINMU*(SINDI*DTHDN+
61 1SINTH*COSDI*DPSON)
62 IF (IPRINT.GE.2) WRITE (IOU6,90) A(1),B(1),C(1),D(1)
63 CONTINUE
64 DO 60 I=1,9
65 COF(I)=0.
66 DO 70 I=1,M
67 COF(1)=COF(1)+A(I)*D(I)
68 COF(2)=COF(2)+B(I)*D(I)
69 COF(3)=COF(3)+C(I)*D(I)
70 COF(4)=COF(4)+A(I)*B(I)
71 COF(5)=COF(5)+A(I)*B(I)
72 COF(6)=COF(6)+A(I)*C(I)
73 COF(7)=COF(7)+B(I)*B(I)
74 COF(8)=COF(8)+B(I)*C(I)
75 COF(9)=COF(9)+C(I)*C(I)
76 IF (IPRINT.GE.2) WRITE (IOU6,90) (COF(I),I=1,9)
77 RETURN
78 C
79 C
80 C

```

E 81
E 82
E 83

FORMAT (18H0***** COEFS *****)
FORMAT (8E15.7)
END

80
90

```

C**** SUBROUTINE COMPAT
Y-AXIS MUST ALIGN WITH FREE STREAM, ROTATE AXES IF NEEDED
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHETA,DPSI
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP,COF(9)
COMMON /ESENS/ MC,YC,ZC,UC,VC,WC,PC,PPMC,THETAC,PSIC
IF (IPRINT.GE.2) WRITE (IOU6,40)
GM2=GF(1)*FMSTR*FMSTR
DO 20 I=1,20
XI=PC*POP
D1=XI-1.
D2=GM2-D1
D4=XI+GF(4)
D3=GM2/GF(3)-D4
THETAC=ATAN(SQRT(D3/D4))*D1/D2
PSIC=(COF(3)-COF(8))*THETAC-COF(6)*PC/COF(9)
SN2T=.5*SIN(2.*THETAC)
DTHDP=SN2T*(1./D1+1./D2-.5/D3-.5/D4)*POP
DPSDP=-((COF(8)*DTHDP+COF(6))/COF(9)
D2TDP2=COF(2.*THETAC)/SN2T*DTHDP+POP**2*SN2T*(-1./D1**2+1./
D2**2-.5/D3**2+.5/D4**2)
C=COF(5)*PC+COF(7)*THETAC+COF(8)*PSIC-COF(2)
H=C*DTHDP+COF(4)*PC+COF(5)*THETAC+COF(6)*PSIC-COF(1)
HP=C*D2TDP2+(COF(7)*DTHDP+COF(8)*DPSDP+2.*COF(5))*DTHDP+COF(6)*
DPSDP+COF(4)
PC=PC-H/HP
IF (IPRINT.GE.2) WRITE (IOU6,50) PC,THETAC,PSIC,XI,D1,D2,D3,D4,
ISN2T,DTHDP,DPSDP,D2TDP2,C,H,HP
IF (I.EQ.1) GO TO 10
IF (ABS((PC-PCN)/PC).GT.DP) GO TO 10
IF (ABS(THETAC-THCN).GT.DTHETA) GO TO 10
IF (ABS(PSIC-PSCN).LE.DPSI) GO TO 30
PCN=PC
THCN=THETAC
PSCN=PSIC
WRITE (IOU6,60)
CALL EXIT
PPMC=(D4/(GF(4)*XI+1.))*GF(6)/XI**GF(5)
RETURN
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20
30
C
C

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F 41
F 42
F 43
F 44
F 45

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C
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60
FORMAT (19H0***** COMPAT *****)
FORMAT (8E15.7)
FORMAT (30H0CONVERGENCE FAILURE IN COMPAT)
END

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SUBROUTINE GMTRY (SINE,COSINE,XC,YC,ZC,A4,B4,C4)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,OP,OTHETA,OPSI
COMMON /GEOM/ YMAX,YSTOP,UNIL,INDEX,ZBLNU(4),YBLNU(4),DBLNL
UNIL=AMAX1(1.,UNIL)
X1=COSINE*XC-SINE*YC
YC=SINE*XC+COSINE*YC
TA=COSINE*A4-SINE*B4
TB=SINE*A4+COSINE*B4
XC=X1
Z1=ZC
IND=0
DO 40 J=1,5
INDEX=0
IN=IND
T=0.
DO 30 I=1,30
CALL FIGURE (XC,YC,ZC,F,A,B,C)
IF (INDEX.EQ.IND) GO TO 50
IF (I.GT.1) GO TO 10
B1=TA*B-TB*A
B3=C4*B-TB*C
T=T-F/(B1*A+B3*C)
XC=X1+T*B1
ZC=Z1+T*B3
IF (IPRINT.GE.2) WRITE (IOU6,60)
IF (IPRINT.GE.2) WRITE (IOU6,70) T,XC,YC,ZC,F,A,B,C,INDEX,IND,J
IF (I.EQ.1) GO TO 20
IF (ABS(XC-X0)+ABS(ZC-Z0).LE.UNIL*1.E-6) GO TO 40
X0=XC
Z0=ZC
CONTINUE
WRITE (IOU6,80)
CALL EXIT
IND=INDEX
WRITE (IOU6,90) INDEX,IN
CALL ROTATE (XC,YC,SINE,COSINE)
CALL NORM (COSINE*A+SINE*B,-SINE*A+COSINE*B,C,A4,B4,C4)
RETURN
C
C

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| 40 | |
| 50 | |
| C | |
| C | |

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G 42
G 43
G 44
G 45
G 46

C 60
70
80
90

FORMAT (25(2H *),6H GMTRY,25(2H *))
 FORMAT (8G15.7,3I3)
 FORMAT (29HCONVERGENCE FAILURE IN GMTRY)
 FORMAT (40H000Y POINT OSCILLATING BETWEEN SECTIONS,12,4H AND,12)
 END

```

SUBROUTINE FIGURE (X,Y,Z,F,A,B,C)
COMMON /MESH/ K1(8),AL,ZZL,ZX23,ZX7,SP,XXL
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTA,DPSI
COMMON /GEOM/ YMAX,YSTOP,UNIL,INDEX,DBLNL,NCQ,CQ(8,10)
DIMENSION ZX(23),ZXP(23),P(23),Q(23),R(23),S(23),T(23),SG(23)
DIMENSION AU(2),SU(3)
IF ((Y.EQ.YI).AND.(MOLD.LT.3)) GO TO 80
IF ((Y.EQ.YI).AND.(MOLD.GT.2)) GO TO 70
YI=Y
IF ((Y.GT.YSTOP+.0001).AND.(ABS(YSTOP).GT.EPSLN)) GO TO 380
DO 30 I=1,50
IF (Y.LE.YMAX) GO TO 40
READ (IOU5,400) YMAX,N,MOD,RATIO
IF (EOF(IOU5)) 380,10
IF (MOD.NE.0) MOLD=MOD
WRITE (IOU6,440) YMAX,N,MOLD,RATIO
DO 20 K=1,M
READ (IOU5,420) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
WRITE (IOU6,450) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
CONTINUE
IF (MOLD.EQ.1) M=7
IF (MOLD.EQ.2) M=13
IF (MOLD.GT.2) M=21
CONTINUE
DO 50 I=1,M
IF ((RATIO.GT.0.)AND.((I.EQ.19).OR.(I.EQ.20))) GO TO 50
IF (MOLD.EQ.3.AND.(I.GT.7.AND.I.LT.14)) GO TO 50
CALL CONICF (P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),ZXP(I))
IF (IPRINT.GE.2) WRITE (IOU6,390) I
CONTINUE
AL=ZX(18)
IF (MOLD.LT.3) ZX7 = ZX(7)
IF (MOLD.LT.3) GO TO 80
IF (RATIO.GT.0.) CALL XSUBG (ZX,ZXP,RATIO)
CALL CONPIC (CQ,NCQ,Y,ZX(22),ZXP(22),INQ)
IF (INDEX.LT.-1) GO TO 60
ZX(23)=ZX(15)-DBLNL
ZXP(23)=ZXP(15)
ZX23=ZX(23)
UNIL=ABS(ZX(5))

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|-----|--|------|
| 60 | ZX7=AMIN1(ZX(23),ZX(7)) | H 40 |
| | CALL PCRCL (ZX,ZXP,-2.,Y,Z,14,16,19,1,4,2,5,22,A,8,C,F,X2U,Z2U) | H 41 |
| | CALL PCRCL (ZX,ZXP,-2.,Y,Z,15,17,20,3,6,7,5,23,A,8,C,F,X2L,Z2L) | H 42 |
| | IF (INDEX.EQ.-1) XXL=XL | H 43 |
| | IF (INDEX.EQ.-1) ZL=ZL | H 44 |
| | CALL ROTXY (X2U,Z2U,X2U,ZX(19),ZX(16),X2UP,Z2UP) | H 45 |
| | CALL ROTXY (X2U,Z2U,X2U,ZX(16),X2U,ZX(19),ZX(16),ZX(19),ZX(16)) | H 46 |
| | CALL ROTXY (X2L,Z2L,X2L,ZX(20),ZX(17),X2LP,Z2LP) | H 47 |
| | CALL ROTXY (X2L,Z2L,X2L,ZX(20),ZX(17),X2LP,Z2LP) | H 48 |
| | IF (INDEX.LT.0) RETURN | H 49 |
| 70 | CALL ROTXY (X,Z,X2U,Z2U,ZX(19),ZX(16),XUP,ZUP) | H 50 |
| | CALL ROTXY (X,Z,X2L,Z2L,ZX(20),ZX(17),XLP,ZLP) | H 51 |
| 80 | IF (INDEX.GT.0) GO TO (140,160,180,200,220,240,260,280,300,320,340 | H 52 |
| | 1,360,120), INDEX | H 53 |
| | IF ((MOLD.EQ.1).OR.(MOLD.EQ.3)) GO TO 90 | H 54 |
| | IF ((Z.GE.ZX(10)).AND.(X.LE.ZX(13))) GO TO 130 | H 55 |
| | IF (Z.GE.ZX(8)) GO TO 150 | H 56 |
| | IF (Z.GT.ZX(9)) GO TO 170 | H 57 |
| 90 | IF ((MOLD.LT.3).AND.(Z.GT.ZX(2))) GO TO 190 | H 58 |
| | IF ((MOLD.GT.2).AND.(Z.GT.ZX(22)).AND.(Z.GT.ZX(2)).AND.(X.LT.X2U) | H 59 |
| | 1.AND.(ZX(14).LE.ZX(16))) GO TO 190 | H 60 |
| | IF ((MOLD.GT.2).AND.(Z.GT.ZX(22)).AND.(Z.GT.ZX(2)).AND.(ZX(14) | H 61 |
| | 1.GT.ZX(16))) GO TO 190 | H 62 |
| | IF (MOLD.LT.3) GO TO 110 | H 63 |
| | IF ((Z.GE.ZX(22)).AND.(X.LT.X2U).AND.(ZX(14).LE.ZX(16))) GO TO 210 | H 64 |
| | IF ((Z.GE.ZX(22)).AND.(ZX(14).GT.ZX(16))) GO TO 210 | H 65 |
| | IF (Z.LT.ZX(18)) GO TO 100 | H 66 |
| | IF (XUP.LT.X2UP) GO TO 230 | H 67 |
| | IF (XUP.LT.ZX(19)) GO TO 250 | H 68 |
| | GO TO 270 | H 69 |
| 100 | IF ((Z.LE.ZX(23)).AND.(X.LT.X2L).AND.(ZX(15).GE.ZX(17))) GO TO 110 | H 70 |
| | IF ((Z.LE.ZX(23)).AND.(ZX(15).LT.ZX(17))) GO TO 110 | H 71 |
| | IF (XLP.LT.X2LP) GO TO 290 | H 72 |
| | IF (XLP.LT.ZX(20)) GO TO 310 | H 73 |
| | GO TO 330 | H 74 |
| 110 | IF (Z.GE.ZX(7)) GO TO 210 | H 75 |
| | IF (X.GT.ZX(6)) GO TO 350 | H 76 |
| | C***BOTTOM FLAT SECTION | H 77 |
| | INDEX=13 | H 78 |
| 120 | A=0.0 | H 79 |

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H 118
H 119

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      B=ZXP(3)
      C=-1.0
      F=-(2-ZX(3))
      GO TO 370
*****CANOPY FLAT SECTION
130  INDEX=1
140  A=0.0
      B=-ZXP(10)
      C=1.0
      F=Z-ZX(10)
      GO TO 370
*****CANOPY SECTION
150  INDEX=2
160  CALL ELIPSE (X,Z,ZX,ZXP,10,11,13,12,A,B,C,F)
      GO TO 370
*****CUBIC SECTION
170  INDEX=3
180  CALL CUBIC (X,Y,Z,ZX,ZXP,A,B,C,F)
      GO TO 370
*****UPPER FUSELAGE ELLIPSE SECTION
190  INDEX=4
200  CALL ELIPSE (X,Z,ZX,ZXP,1,2,4,5,A,B,C,F)
      GO TO 370
*****VERTICAL STRAIGHT SECTION
210  INDEX=5
220  A=1.0
      B=-ZXP(5)
      C=0.
      F=X-ZX(5)
      GO TO 370
*****UPPER WING BLENDING SECTION
230  INDEX=6
240  CALL PCRCL (ZX,ZXP,X,Y,Z,14,16,19,1,4,2,5,22,A,B,C,F,D,D)
      GO TO 370
*****UPPER WING STRAIGHT SECTION
250  INDEX=7
260  CALL WINGF (ZX,ZXP,X,Y,Z,19,5,16,14,A,B,C,F)
      GO TO 370
*****UPPER WING TIP SECTION
270  INDEX=8

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280 CALL PELIPS (ZX,ZXP,X,Y,Z,14,16,19,5,18,21,A,B,C,F)
GO TO 370
C***LOWER WING BLENDING SECTION
290 INDEX=9
300 CALL PCRL (ZX,ZXP,X,Y,Z,15,17,20,3,6,7,5,23,A,B,C,F,D,D)
GO TO 370
C***LOWER WING STRAIGHT SECTION
310 INDEX=10
320 CALL WINGF (ZX,ZXP,X,Y,Z,20,5,17,15,A,B,C,F)
GO TO 370
C***LOWER WING TIP SECTION
330 INDEX=11
340 CALL PELIPS (ZX,ZXP,X,Y,Z,15,17,20,5,18,21,A,B,C,F)
GO TO 370
C***LOWER FUSELAGR ELLIPSE SECTION
350 INDEX=12
360 CALL ELIPSE (X,Z,ZX,ZXP,3,7,6,5,A,B,C,F)
370 IF (IPRINT.GE.2) WRITE (IOU6,410) F,A,B,C,INDEX
RETURN
380 WRITE (IOU6,430)
CALL EXIT
C
C
390 FORMAT (10H CURVE NO ,I3,5H OK)
400 FORMAT (F10.5,2I5,F10.5)
410 FORMAT (19H0**** FIGURE ****/4G14.7,21H BODY SECTION INDEX =,I2)
420 FORMAT (I2,5E15.8,F2.0)
430 FORMAT (1H0,60(2H *)/1H0,20X,35H$$$$ HALLELUJAH, YOU HAVE GONE AL
1L,35H THE WAY--FEELING NICE, I BET $$$$1H0,60(2H *)
440 FORMAT (35HGEOMETRIC COEFFICIENTS FOR Y UP TO,G15.7,15,11H NEW CU
IRVES,2X,5HMOID=,I2,2X,6HRTIO=,F7.3)
450 FORMAT (9HOCURVE NO,I3,5H, P =E16.8,5H Q =E16.8,5H R =E16.8,5H
1S =E16.8,5H T =E16.8,6H SG =F4.1)
END
H 120
H 121
H 122
H 123
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| 10 | 1 |

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SUBROUTINE ROTXY (X,Y,X1,Y1,X2,Y2,XP,YP)
  DY=Y2-Y1
  DX=X2-X1
  R=SQRT(DX**2+DY**2)
  SINP=DY/R
  COSP=DX/R
  XP=COSP*X+SINP*Y
  YP=-SINP*X+COSP*Y
  RETURN
END

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SUBROUTINE TRANS (H,XYZ,A4,B4,C4,TO,IN)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DIHETA,DPSI
DIMENSION H(4,8),XYZ(3,7)
IF (A4+A4+C4+C4.LE.1.E-14) RETURN
COSX=-SQRT(1.-C4*C4)
SRT=SQRT(A4*A4+B4*B4)
IF (SRT.GT.1.E-7) GO TO 10
COSZ=0.
SINZ=1.*TO
GO TO 20
10 COSZ=-B4/SRT
SINZ=TO*A4/SRT
20 DO 50 J=1,7
IF (IN.EQ.0.AND.J.GT.4) GO TO 50
IF (IN.NE.0.AND.J.GT.3) GO TO 40
DO 30 K=1,4,3
IF (TO.GT.0.) CALL ROTATE (H(J,K),H(J,K+1),SINZ,COSZ)
CALL ROTATE (H(J,K+1),H(J,K+2),C4*TO,COSX)
IF (TO.LT.0.) CALL ROTATE (H(J,K),H(J,K+1),SINZ,COSZ)
30 CONTINUE
IF (IN.EQ.0) GO TO 50
IF (J.GT.2.AND.J.LT.6) GO TO 50
40 IF (TO.GT.0.) CALL ROTATE (XYZ(1,J),XYZ(2,J),SINZ,COSZ)
CALL ROTATE (XYZ(2,J),XYZ(3,J),C4*TO,COSX)
IF (TO.LT.0.) CALL ROTATE (XYZ(1,J),XYZ(2,J),SINZ,COSZ)
50 CONTINUE
IF (IPRINT.GE.2) WRITE (IOU6,60) H,XYZ
IF (TO.LT.0..OR.IN.EQ.0) RETURN
XYZ(3,3)=ACOS(XYZ(2,2))
XYZ(1,4)=ATAN2(XYZ(3,2),XYZ(1,2))
XYZ(2,5)=ACOS(XYZ(2,7))
XYZ(3,5)=ATAN2(XYZ(3,7),XYZ(1,7))
IF (XYZ(1,4).LT.-3.) XYZ(1,4)=XYZ(1,4)+6.2831853072
IF (XYZ(3,5).LT.-3.) XYZ(3,5)=XYZ(3,5)+6.2831853072
RETURN
60
C
C
C
C
FORMAT (18H0**** TRANS ****/(8E15.7))
END

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SUBROUTINE ROTATE (X,Y,SINE,COSINE)
TEMP=X
X=COSINE*TEMP+SINE*Y
Y=-SINE*TEMP+COSINE*Y
RETURN
END

| | | |
|--|---|----|
| SUBROUTINE SOL (A11,A12,A13,D1,A21,A22,A23,D2,A31,A32,A33,D3,X,Y,Z | L | 1 |
| 1) | L | 2 |
| IF (ABS(A11).LE.1.E-7) GO TO 10 | L | 3 |
| B12=A12/A11 | L | 4 |
| B13=A13/A11 | L | 5 |
| C1=D1/A11 | L | 6 |
| B22=A22-B12*A21 | L | 7 |
| IF (ABS(B22).LE.1.E-7) GO TO 10 | L | 8 |
| B32=A32-B12*A31 | L | 9 |
| B23=(A23-B13*A21)/B22 | L | 10 |
| C2=(D2-A21*C1)/B22 | L | 11 |
| B33=(A33-A31*B13-B23*B32) | L | 12 |
| IF (ABS(B33).LE.1.E-7) GO TO 10 | L | 13 |
| Z=(D3-C1*A31-C2*B32)/B33 | L | 14 |
| Y=C2-B23*C2 | L | 15 |
| X=C1-B12*Y-B13*Z | L | 16 |
| RETURN | L | 17 |
| 10 | L | 18 |
| Q=A11*(A22*A33-A23*A32)+A21*(A13*A32-A12*A33)+A31*(A12*A23-A13*A22 | L | 19 |
| 1) | L | 20 |
| X=(A13*(D2*A32-A22*D3)+A23*(A12*D3-D1*A32)+A33*(D1*A22-A12*D3))/D | L | 21 |
| Y=(A11*(D2*A33-A23*D3)+A21*(A13*D3-D1*A33)+A31*(D1*A23-A13*D2))/D | L | 22 |
| Z=(A12*(D2*A31-A21*D3)+A22*(A11*D3-D1*A31)+A32*(D1*A21-A11*D2))/D | L | 23 |
| RETURN | L | 24 |
| END | | |

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SUBROUTINE HARNES (QINF,A,N)
DIMENSION A(99,8,4)
DO 10 L=3,N
VN=SQRT(A(L,4)**2+(QINF-A(L,5))**2+A(L,6)**2)
CALL NORM (-A(L,4),QINF-A(L,5),-A(L,6),A0,B0,C0)
A1=(A(L+1,3)-A(L,3))**2+(A(L+1,1)-A(L,1))**2
C1=(A(L,3)-A(L-1,3))**2+(A(L,1)-A(L-1,1))**2
CALL NORM (C1*(A(L+1,3)-A(L,3))+A1*(A(L,3)-A(L-1,3)),0.,C1*(A(L+1,
11)-A(L,1))+A1*(A(L,1)-A(L-1,1)),A1,B1,C1)
B=SQRT(1.-B0*B0)
CALL NORM (SIGN(A1*B,A0)+A0,0.,SIGN(C1*B,C0)+C0,A1,B1,C1)
A(L,4)=-A1*VN*B
A(L,6)=-C1*VN*B
RETURN
END

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| N | N | N | N | N | N | N | N | N | N | N | N | N | N |

```

SUBROUTINE MIRROR (A,SIN2A,COS2A,N)
  DIMENSION A(99,8)
  I=1
  J=3
  DO 20 L=1,2
  DO 10 K=1,4,3
    A(I,K)=-COS2A*A(J,K)+SIN2A*A(J,K+1)
    A(I,K+1)=SIN2A*A(J,K)+COS2A*A(J,K+1)
    A(I,K+2)=A(J,K+2)
    A(I,K/4+7)=A(J,K/4+7)
  I=N+L
  J=N-L
  RETURN
  END

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0 0 0 0 0 0 0

SUBROUTINE NORM (X,Y,Z,A,B,C)
T=SQR(X²+Y²+Z²)
A=X/T
B=Y/T
C=Z/T
RETURN
END

```

SUBROUTINE DATOUT (A,I,IND,KAB,IO)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHTA,DPS1,KP4,IOU3
COMMON /FSTR/ COSA,SINA,FMSTR,QINF,GF(7),POP
COMMON /CONT/ NPC,DYC,ILL,KURE,SINE,COSINE,N,Y,IS
DIMENSION A(99,8)
IF (N.EQ.IS.AND.IO.NE.0) RETURN
IF (KP4.LE.0.AND.(IO.EQ.1.AND.N/KAB*KAB.NE.N)) RETURN
IF ((KP4.GT.0.AND.IO.EQ.0).AND.(N/KAB*KAB.NE.N.AND.(IND.NE.1.OR.(I
11.NE.2.AND.I.NE.NPC+1)))) RETURN
RAD=57.2957795130823
P=A(I,7)*POP
P1=A(I,7)/A(I,8)
CP=2.*(P-1.)/(GF(1)*FMSTR*FMSTR)
XM=SQRT((1./P1*GF(7)-1.)/GF(2))
X=COSINE*A(I,1)-SINE*A(I,2)
U=COSINE*A(I,4)-SINE*A(I,5)
V=SINE*A(I,4)+COSINE*A(I,5)
OM=ATAN(U/V)*RAD
UM=ATAN(A(I,6)/V)*RAD
PS=0.
TH=0.
IF (ABS(A(I,6)).LE.1.E-07.AND.ABS(U).LE.1.E-07) GO TO 10
PS=ATAN2(A(I,6),U)*RAD
TH=ACOS(V/SQRT(U*U+V*V+A(I,6)*A(I,6)))*RAD
IF (IO.EQ.0.OR.KP4.GE.0) GO TO 20
WRITE (IOU7,120) A(I,3),X,XM,A(I,8),TH,PS
RETURN
10 IOU=IOU6
IF (KP4.GE.0.AND.IO.EQ.1) IOU=IOU3
IF (I.GT.2) GO TO 30
Y=SINE*A(I,1)+COSINE*A(I,2)
IF (IND.EQ.1) WRITE (IOU,110) N,Y
IF (KP4.GT.1.AND.(IO.EQ.0.AND.N/KAB*KAB.NE.N)) GO TO 40
IF (IND.EQ.1) WRITE (IOU,60)
IF (IND.EQ.2) WRITE (IOU,70)
IF (IND.EQ.3) WRITE (IOU,80)
WRITE (IOU,90)
IF (KP4.GT.1.AND.(IO.EQ.0.AND.N/KAB*KAB.NE.N)) GO TO 50
WRITE (IOU,100) A(I,3),X,XM,A(I,8),TH,PS,CP,P,A(I,7),OM,UM
RETURN
20
30

```

| | | | |
|-----|--|---|----|
| 40 | WRITE (IOU6,130) CP | P | 41 |
| 50 | IF (I.EQ.NPC+1) WRITE (IOU6,140) CP | P | 42 |
| | RETURN | P | 43 |
| C | | P | 44 |
| C | | P | 45 |
| C | | P | 46 |
| 60 | FORMAT (1H054X11H80DY POINTS) | P | 47 |
| 70 | FORMAT (1H054X12MFIELD POINTS) | P | 48 |
| 80 | FORMAT (1H054X12HSMOCK POINTS) | P | 49 |
| 90 | FORMAT (80H -----Z-----X----- MACH NO. ----PI/PIO---- | P | 50 |
| | 1- THETA, DEG --PSI,DEG--,52H ----CP-----P/PO-----P/PIO- | P | 51 |
| | 2--OUTWASHUPWASHI) | P | 52 |
| 100 | FORMAT (1H 2E15.8,F10.7,E15.8,F12.8,F13.8,3E13.5,2F6.2) | P | 53 |
| 110 | FORMAT (11H0SURFACE NO,13,14H, STATION Y = E15.8) | P | 54 |
| 120 | FORMAT (2E15.8,F10.7,E15.8,F12.8,F13.8) | P | 55 |
| 130 | FORMAT (1H+,44X,22MLOWER CENTERLINE CP = E15.8) | P | 56 |
| 140 | FORMAT (1H+,83X,22HUPPER CENTERLINE CP = E15.8) | P | 57 |
| | END | P | 58 |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | |
| | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q | Q |

```

SUBROUTINE TIDYUP (SINE,COSINE,A,NP,NPP,AN,LINE)
COMMON /MESH/ K1,K2,K3,K4,K5,K6,K7,K8,ZL(6)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,DP,DTHEA,DPSI
DIMENSION A(99,8,4),L(5),TM(5),ZT(99),XT(99)
IF (K5.EQ.0) ZL(1)=AN
DO 10 I=1,NP
IF (I.LE.5) L(I)=0
CALL ROTATE (A(I,1,1),A(I,2,1),-SINE,COSINE)
CALL ROTATE (A(I,4,1),A(I,5,1),-SINE,COSINE)
A(I,1,4)=0.
REFL=1.E10
IF (LINE.EQ.1) GO TO 30
NO=NP-K7
DO 20 I=1,NO
XT(I)=A(I,K7,1,1)
ZT(I)=A(I,K7,3,1)
CALL ROTATE (XT(I),ZT(I),-7071067812,7071067812)
XP=X0
CALL SECOND (XT,ZT,NO,XP,ZL(5),DYP,0)
CALL ROTATE (XP,ZL(5),7071067812,7071067812)
DO 60 I=2,NP
DO 50 KK=1,5
IF (L(KK).NE.0.OR.KK.EQ.2) GO TO 40
IF (A(I,3,1)-LT.ZL(KK)-AND.A(I+1,3,1)-GE.ZL(KK)) L(KK)=I
IF (REFL.LT.(A(I,3,1)-ZL(2))*2+(A(I,1,1)-ZL(6))*2) GO TO 50
L(2)=I
REFL=(A(I,3,1)-ZL(2))*2+(A(I,1,1)-ZL(6))*2
CONTINUE
A(I,1,4)=A(I-1,1,4)+SQRT((A(I,1,1)-A(I-1,1,1))*2+(A(I,2,1)-A(I-1,
12,1))*2+(A(I,3,1)-A(I-1,3,1))*2)
DO 70 I=1,5
IF (LINE.EQ.1.AND.I.EQ.5) GO TO 80
IF (K5.EQ.C.AND.I.GT.1) GO TO 80
TM(I)=(A(L(I)+1,1,4)*(ZL(I)-A(L(I),3,1))+A(L(I),1,4)*(A(L(I)+1,3,1
1)-ZL(I)))/(A(L(I)+1,3,1)-A(L(I),3,1))
NT=2*NPP-6+K1-K2+2*(K3-K4)+4*(K4-K5+K6-K7)-2*(K4-K5+K6-K7)/(K8+1)
IF (K6-K5.LT.2) NT=NT+4+2*(K5-K6)
IF (K5.EQ.0) NT=2*NPP-2+K1-K2+K3-K4
K9=2*K7-K6
K10=2*K7-K5

```

```

K11=2*K7-K4
K12=2*K7-K3
N=0
DO 90 M=2,NPP
N=N+1
IF (M.LE.K1.OR.M.GT.K2) N=N+1
IF (N.GE.NT/2) GO TO 100
CONTINUE
IF (K5.NE.0) M=K12
IF (K5.NE.0) N=(NT-K1+K2)/2+K3-1+K12-NPP
DT0=TM(1)/FLOAT(N)
IF (LINE.EQ.1) RATIO=TM(4)/TM(1)
IF (K5.NE.0) DT05=TM(1)*(1.-RATIO)/(FLOAT(N-2*K3))
IF (K5.NE.0) DT0=(TM(1)*RATIO-2.*DT05)/FLOAT(2*K3-2)
DT1=(A(NP,1,4)-TM(1))/FLOAT(NT-N)
DT07=(TM(5)-TM(1))/FLOAT(N-2*K3+2)
TOP=2*(NPP-K12)+K1-K2
IF (K5.NE.0.AND.K5.EQ.K6) DT1=DT05+(DT1-DT05)*FLOAT(NT-N)/TOP
IF (K5.NE.K6.AND.LINE.NE.1) DT1=DT07+(DT1-DT07)*FLOAT(NT-N)/TOP
IF (K3.NE.0.AND.K5.EQ.0) DT0=A(NP,1,4)/FLOAT(NT)
IF (K3.NE.0.AND.K5.EQ.0) DT1=DT0
IF (K5.EQ.K6) K=0
IF (K5.EQ.K6.OR.LINE.NE.1) GO TO 110
DT1=DT05*(DT1-DT05)*FLOAT(NT-N)/TOP
SHIFT=DT05*(FLOAT(K4-K3)+FLOAT((K5-K4)/(K8+1))/2.)
MOVE=((TM(2)+TM(3))/2.-SHIFT-DT0*FLOAT(2*K3-2))*FLOAT(K8+1)/DT05
MOVE=MAX0(MOVE,1-(K4-K3)*(K8+1))
K=MOVE/(K8+1)
IF (MOVE.LT.0) K=K-1
INC=MOVE-K*(K8+1)-1
IF (MOVE.EQ.0) INC=0
IF (MOVE.GE.4) INC=INC+1
IF (I.PRINT.GE.2) WRITE (10U6,150) MOVE,K,INC
DO 130 I=1,8
DT=DT0
LL=1
IF (1.EQ.1.OR.1.EQ.4) LL=2
CALL KURFIT (A(1,1,4),A(1,1,1),A(1,1,3),NP,0.,0.,LL,LL)
PT=-DT-DT
DO 130 J=1,NPP

```

```

IF (K5.NE.0.AND.J.GT.K3) DT=DT05
IF (K5.NE.K6.AND.(LINE.NE.1.AND.J.GT.K7)) DT=DT07
IF (J.GT.M) DT=DT1
PT=PT+DT
IF (J.LE.K1.OR.J.GT.K2) PT=PT+DT
IF (J.GT.K3.AND.J.LE.K4).OR.(J.GT.K4.AND.J.LE.K12)) PT=PT-DT
IF ((J.GT.K5+1.AND.J.LT.K6).OR.(J.GT.K9+1.AND.J.LT.K10)) PT=PT+DT
IF ((J.GT.K4+K.AND.J.LE.K5+K).OR.((J.GT.K6.AND.J.LE.K9).OR.(
1J.GT.K10-K.AND.J.LE.K11-K))) PT=PT-DT*FLOAT(K8)/FLOAT(K8+1)
IF (K5.EQ.K6) GO TO 120
IF (J.EQ.K4+K+1.OR.J.EQ.K11-K) PT=PT+FLOAT(INC)*DT/FLOAT(K8+1)
IF (J.EQ.K5+K+1.OR.J.EQ.K10-K) PT=PT-FLOAT(INC)*DT/FLOAT(K8+1)
CALL KURVE (A(1,1,3),A(1,1,4),A(1,1,1),PT,A(J,1,2),NP,LL)
CONTINUE
IF (LINE.EQ.1) X0=A(M,1,2)
IF (LINE.EQ.1) Z0=A(M,3,2)
IF (LINE.EQ.1) CALL ROTATE (X0,Z0,-.7071067812,.7071067812)
IF (IPRINT.GE.2) WRITE (IQU6,160) ((A(I,J,2),J=1,8),I=1,NPP)
DO 140 I=1,NPP
CALL ROTATE (A(I,1,2),A(I,2,2),SINE,COSINE)
CALL ROTATE (A(I,4,2),A(I,5,2),SINE,COSINE)
RETURN
120
130
140
C
C
C
150
160
FORMAT (6I10)
FORMAT (19M0**** TIDYUP ****)/(8E14.6)
END

```

1
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4
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25

R R

```

SUBROUTINE SECOND (X,Y,N,XP,YP,DYP,IT)
DIMENSION X(1),Y(1)
M=N-1
ARROW=XP-X(1)
NI=N/2+1
IF ((X(NI)-X(1))*ARROW) 10,10,20
IP=2
GO TO 40
DO 30 I=2,M
IP=I
IF ((XP-X(I))*ARROW) 40,40,30
CONTINUE
A=XP-X(IP-1)
B=XP-X(IP)
C=XP-X(IP+1)
D=X(IP-1)-X(IP)
E=X(IP-1)-X(IP+1)
G=X(IP)-X(IP+1)
T1=Y(IP-1)/(D+E)
T2=-Y(IP)/(D+G)
T3=Y(IP+1)/(E+G)
YP=T1*B+C+T2*A+C+T3*A*B
IF (IT.GT.0) DYP=T1*(B+C)+T2*(A+C)+T3*(A+B)
RETURN
END
10
20
30
40

```


| | |
|---|----|
| T | 1 |
| T | 2 |
| T | 3 |
| T | 4 |
| T | 5 |
| T | 6 |
| T | 7 |
| T | 8 |
| T | 9 |
| T | 10 |
| T | 11 |
| T | 12 |
| T | 13 |
| T | 14 |
| T | 15 |
| T | 16 |
| T | 17 |
| T | 18 |
| T | 19 |
| T | 20 |
| T | 21 |
| T | 22 |
| T | 23 |
| T | 24 |
| T | 25 |
| T | 26 |
| T | 27 |
| T | 28 |
| T | 29 |
| T | 30 |
| T | 31 |
| T | 32 |

```

SUBROUTINE KURFIT (X,Y,A,N,DY1,DY2,K1,K2)
DIMENSION X(1),Y(1),A(1),B(200)
N1=N-2
A(1)=-DY1/2.
B(1)=X(1)-X(2)
IF (K1.EQ.2) GO TO 10
A(1)=- (DY1+(Y(2)-Y(1))/B(1))/B(1)
B(1)=0.0
J=1
DO 20 I=1,N1
K=I+1
J=J+1
C1=X(K)-X(I)
C2=X(K+1)-X(K)
C3=Y(K)-Y(I)
C4=Y(K+1)-Y(K)
C5=C3/C1-C4/C2
C6=C1/C2
C7=C1*C2
B(J)=1.0/(C6*(C1-B(J-1)))
A(J)=(C5/C2-C6*A(J-1))*B(J)
J=J+1
B(J)=1.0/((-C1-C2)/C7-C6*B(J-1))
A(J)=(-C5/C7-C6*A(J-1))*B(J)
A(J+1)=(DY2-C4/C2+C2*A(J))/(C2*(B(J)-C2))
IF (K2.EQ.2) A(J+1)=(DY2/2.+A(J))/(-2.*C2+B(J))
J=2*(N-1)
J=J-1
IF (J.LE.0) RETURN
A(J)=A(J)-B(J)*A(J+1)
GO TO 30
END

```

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| U | U | U | U | U | U | U | U | U | U | U | U | U | U |

```

SUBROUTINE KURVE (A,X,Y,XP,YP,N,L)
DIMENSION A(1),X(1),Y(1)
DO 30 I=2,N
  IF ((XP-X(1))*(X(2)-X(1))) 40,40,20
  IF ((XP-X(1))*(XP-X(1))) 40,30,30
CONTINUE
K=2*I-3
C1=XP-X(I-1)
C2=X(I)-XP
IF (L.EQ.8) C2=0.
SLOPE=(Y(I)-Y(I-1))/(X(I)-X(I-1))
YP=Y(I-1)+(SLOPE+A(K)*C2+A(K+1)*C1*C2)*C1
RETURN
END
10
20
30
40

```

1
2
3
4
5
6
7
8
9

V
V
V
V
V
V
V
V
V

```

SUBROUTINE CONICF (P,Q,R,S,I,SG,X,Y,YP)
  ROOT=SG*SQRT((R*X+S)*X+T)
  Y=P*X+Q+ROOT
  IF ((SG.NE.0.).AND.(ROOT.NE.0.)) GO TO 10
  YP=P
  GO TO 20
  YP=P+(R*X+S/2.0)/ROOT
  RETURN
  END

```

10
20


```

1  SUBROUTINE CUBIC (X,YI,Z,ZX,ZXP,A,B,C,F)
2  DIMENSION ZX(1),ZXP(1)
3  IF (Y.EQ.YI) GO TO 30
4  Y=YI
5  DZ1=ZX(8)-ZX(11)
6  DZ2=ZX(9)-ZX(2)
7  DZC=ZX(10)-ZX(11)
8  DZU=ZX(1)-ZX(2)
9  DZ21=ZX(9)-ZX(8)
10 X1=(ZX(12)-ZX(13))*SQRT(1.0-(DZ1/DZC)**2)+ZX(13)
11 X2=(ZX(5)-ZX(4))*SQRT(1.0-(DZ2/DZU)**2)+ZX(4)
12 DX21=X2-X1
13 IF (X1.GT.ZX(13)) GO TO 10
14 Z1P=0.0
15 X1Y=0.0
16 Z1PY=0.0
17 GO TO 20
18
19
20 Z1P=-X1/DZ1*(DZC/(ZX(12)-ZX(13))**2
21 X1P=1.0/Z1P
22 X1Y=X1*((ZX(12)-ZX(13))/(ZX(12)-ZX(13)))+(ZXP(8)+((ZX(8)-ZX(10))
23 1*(ZXP(11)-DZ1*ZXP(10))/DZC)/Z1P+ZXP(13)
24 X1PY=X1P*((ZX(8)-ZX(11))/DZ1-X1Y/X1+2.0*((ZXP(12)-ZXP(13))/(ZX(
25 112)-ZX(13))-(ZXP(10)-ZXP(11))/DZC))
26 Z1PY=-X1PY*Z1P/X1P
27 Z2P=-X2/DZ2*(DZU/(ZX(4)-ZX(5))**2
28 X2P=1.0/Z2P
29 X2Y=X2*((ZXP(5)-ZXP(4))/(ZX(5)-ZX(4)))+(ZXP(9)+((ZX(9)-ZX(11))*ZXP(
30 12)-DZ2*ZXP(1))/DZU)/Z2P+ZXP(4)
31 X2PY=X2P*((ZXP(9)-ZXP(2))/DZ2-X2Y/X2+2.0*((ZXP(4)-ZXP(5))/(ZX(4)-
32 1ZX(5))-(ZXP(1)-ZXP(2))/DZU))
33 Z2PY=-X2PY*Z2P/X2P
34 ZY21=ZXP(9)-ZXP(8)
35 DX21Y=X2Y-X1Y
36 IF ((Z1P.LT.-4.0).OR.(Z2P.LT.-4.0).OR.(Z1P.GT.0.01)) GO TO 40
37 CA=3.0*DZ21-(Z2P+2.0*Z1P)*DX21
38 CB=-2.0*DZ21+(Z2P+Z1P)*DX21
39 CAV=3.0*ZY21-(Z2PY+2.0*Z1PY)*DX21-(Z2P+2.0*Z1P)*DX21Y
40 CBY=-2.0*ZY21+(Z2PY+Z1PY)*DX21+(Z2P+Z1P)*DX21Y
41 DX1=X-X1
42 DX2=X-X2

```

```

41      T=DX1/OX21
42      A=-Z1P-(2.0*CA+3.0*CB*T)*T/OX21
43      B=-ZXP(8)-Z1PY*OX1+Z1P*X1Y-(CAY+CBY*T)*T*(A+Z1P)*(X2Y*OX1-X1Y*
44      1OX2)/OX21
45      C=1.0
46      F=Z-ZX(8)-Z1P*OX1-(CA+CB*T)*T*T
47      INDEX=1
48      RETURN
49
50      CA=3.0*OX21-(X2P+2.0*X1P)*OZ21
51      CB=-2.0*OX21+(X2P+X1P)*OZ21
52      CAY=3.0*OX21Y-(X2PY+2.0*X1PY)*OZ21-(X2P+2.0*X1P)*ZY21
53      CBY=-2.0*OX21Y+(X2PY+X1PY)*OZ21+(X2P+X1P)*ZY21
54      OZ1=Z-ZX(8)
55      OZ2=Z-ZX(9)
56      T=OZ1/OZ21
57      A=1.0
58      C=-X1P-(2.0*CA+3.0*CB*T)*T/OZ21
59      B=-X1Y-X1PY*OZ1+X1P*ZXP(8)-(CAY+CBY*T)*T*(C+X1P)*(ZXP(9)*OZ1-ZXP
60      1(8)*OZ2)/OZ21
61      F=X-X1-X1P*OZ1-(CA+CB*T)*T*T
62      INDEX=2
63      RETURN
      END

```

40

| | |
|---|----|
| X | 1 |
| X | 2 |
| X | 3 |
| X | 4 |
| X | 5 |
| X | 6 |
| X | 7 |
| X | 8 |
| X | 9 |
| X | 10 |
| X | 11 |
| X | 12 |
| X | 13 |
| X | 14 |

```

SUBROUTINE ELIPSE (X,Z,ZX,ZXP,I2K,I2M,I2K,I2M,I2K,I2M,A,B,C,F)
DIMENSION ZX(1),ZXP(1)
FF=Z-ZX(I2K)
DX=X-ZX(I2K)
DZ=Z-ZX(I2M)-ZX(I2K)
DZK=ZX(I2K)-ZX(I2M)
A=2.0*DX/DZK**2
C=2.0*DZ/DZK**2
B=C*(ZXP(I2M)*F-ZXP(I2K)*DZ)/DZK+A*(ZXP(I2K)*F-ZX(I2M))-ZXP(I2M)
1*DX)/DXK
F=(DZ/DZK)**2+(DX/DZK)**2-1.0
RETURN
END

```

```

SUBROUTINE WINGF (ZX,ZXP,X,YI,Z,IXG,IXE,IZG,IZE,A,B,C,F)
DIMENSION ZX(1),ZXP(1)
IF ((Y.EQ.YI).AND.(IZG.EQ. IZGS)) GO TO 10
Y=YI
IZGS=IZG
T1=ZX(IXG)-ZX(IXE)
T2=ZX(IZG)-ZX(IZE)
T3=T1/T2
D=(T2*(ZXP(IXG)-ZXP(IXE))-T1*(ZXP(IZG)-ZXP(IZE)))/T2**2
DZ=Z-ZX(IZE)
F=(X-ZX(IXE))-T3*DZ
A=1.0
B=T3*ZXP(IZE)-DZ*D-ZXP(IXE)
C=-T3
RETURN
END

```

10

```

Y 1
Y 2
Y 3
Y 4
Y 5
Y 6
Y 7
Y 8
Y 9
Y 10
Y 11
Y 12
Y 13
Y 14
Y 15
Y 16

```



```

SUBROUTINE PCRCL (ZX,ZXP,X,YI,Z,IZE,IZG,IXG,IZU,IXU,IZM,IXM,IZI,FX
1,FY,FZ,F,X2,Z2)
COMMON /IO/ IOUS,IOU6,IOU7,IPRINT
DIMENSION ZX(1),ZXP(1)
IT=0
IF ((ZX(IZI).LT.ZX(2)).AND.(ZX(IZI).GT.ZX(7))) IT=1
IF ((Y.EQ.YI).AND.(ITT.EQ.IT).AND.(IZEP.EQ.IZE)) GO TO 50
Y=YI
ITT=IT
IZEP=IZE
XM4=(ZX(IZG)-ZX(IZE))/(ZX(IXG)-ZX(IXM))
IF (IZG.EQ.16) SS=-SIGN(1.0,XM4)
IF (IZG.EQ.17) SS=SIGN(1.0,XM4)
ZUM=ZX(IZU)-ZX(IZM)
XMU=ZX(IXM)-ZX(IXU)
IF (IT.NE.1) GO TO 10
X1=ZX(IXM)
X1Y=ZXP(IXM)
XM1=0.
XM1Y=0.
XM3P=0.
XM3PY=0.
GO TO 20
Z1M=ZX(IZI)-ZX(IZM)
Z1MZUM=Z1M/ZUM
T1=SQRT(1.0-Z1MZUM**2)
X1=ZX(IXU)+XMU*T1
X1U=X1-ZX(IXU)
T2=2.0*Z1MZUM*((ZX(IZI)-ZX(IZM))/ZUM-Z1M*(ZX(IZU)-ZX(IZM))/ZUM
1**2)
X1Y=-XMU**2/X1U*T2/2.0+T1*(ZXP(IXM)-ZXP(IXU))+ZXP(IXU)
XMUZUM=XMU/ZUM
T1=Z1M/X1U
XM1=XMUZUM**2*T1
T2=((ZX(IXM)-ZXP(IXU))/ZUM-XMU*(ZX(IZU)-ZXP(IZM))/ZUM**2)*T1
T3=(ZX(IZI)-ZX(IZM))/X1U-Z1M*(X1Y-ZXP(IXU))/X1U**2
XM1Y=(2.0*T2+XMUZUM*T3)*XMUZUM
XM3=-1.0/XM1
XM3P=-1.0/XM3
XM3Y=XM1Y/XM1**2

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20      XM3PY=XM3Y/XM3**2
      XM4P=-1.0/XM4
      XGE=Z X(IXG)-Z X(IXM)
      ZGE=Z X(IZG)-Z X(IZE)
      XM4Y=(ZXP(IZG)-ZXP(IZE))/XGE-(ZXP(IXG)-ZXP(IXM))*ZGE/XGE**2
      XM4PY=XM4Y/XM4**2
      DTH=(ATAN(XM3P)+SS*ATAN(XM4P))/2.0
      XM5=TAN(DTH)
      T1=(1.0/COS(DTH))**2
      T2=XM3PY/(1.0+XM3P**2)+XM4PY/(1.0+XM4P**2)
      XM5Y=T1*T2/2.0
      IF (IT.NE.1) GO TO 30
      XP=Z X(IXM)
      ZP=Z X(IZE)
      XPY=ZXP(IXM)
      ZPY=ZXP(IZE)
      GO TO 40

30      ZE1=Z X(IZE)-Z X(IZ1)
      XM34=XM3-XM4
      T1=(XM4*Z X(IXM)-XM3*X1)
      XP=(ZE1-T1)/XM34
      T2=ZXP(IZE)-ZXP(IZ1)-XM4*ZXP(IXM)-XM4Y*Z X(IXM)+XM3*X1Y+XM3Y*X1
      XPY=(XM34*T2-(ZE1-T1)*(XM3Y-XM4Y))/XM34**2
      ZP=Z X(IZE)+XM4*(XP-Z X(IXM))
      ZPY=ZXP(IZE)+XM4*(XPY-ZXP(IXM))+(XP-Z X(IXM))*XM4Y
      XM15=XM1-XM5
      T1=(ZP-Z X(IZ1))-(XM5*XP-XM1*X1)
      T2=ZPY-ZXP(IZ1)-XM5*XPY-XM5Y*XP+XM1*X1Y+XM1Y*X1
      XO=T1/XM15
      XOY=(XM15*T2-T1*(XM1Y-XM5Y))/XM15**2
      ZO=Z X(IZ1)+XM1*(XO-X1)
      ZOY=ZXP(IZ1)+XM1*(XOY-X1Y)+XM1Y*(XO-X1)
      ZOZ1=ZO-Z X(IZ1)
      XOZ1=XO-X1
      R2=ZOZ1**2+XOZ1**2
      R=SQRT(R2)
      IF (IPRINT-GE.2) WRITE (10U6,80) X,Y,Z,XO,ZO,R,XP,ZP,IT
      IF (X.LT.-1.) GO TO 60
      RY=(ZOZ1*(ZOY-ZXP(IZ1))+XOZ1*(XOY-X1Y))/R
      XO=X-XO

```

Z 81
Z 82
Z 83
Z 84
Z 85
Z 86
Z 87
Z 88
Z 89
Z 90
Z 91
Z 92
Z 93
Z 94
Z 95
Z 96

```

ZZO=Z-ZO
F=R2-ZZO**2-XXO**2
FX=-2.0*XXO
FY=2.0*(R*RY+XXO*XOY+ZZO*ZOY)
FZ=-2.0*ZZO
GO TO 70
CONTINUE
D=SQRT((X1-XP)**2+(ZX(IZ1)-ZP)**2)
ANG=ATAN(XM4)
X2=XP+D*COS(ANG)
Z2=ZP+XM4*(X2-XP)
RETURN
FORMAT (16H0*****PCRCCL*****/(8G15.7))
END

```

60

70

C

C

80

| | |
|----|----|
| 1 | AA |
| 2 | AA |
| 3 | AA |
| 4 | AA |
| 5 | AA |
| 6 | AA |
| 7 | AA |
| 8 | AA |
| 9 | AA |
| 10 | AA |
| 11 | AA |
| 12 | AA |
| 13 | AA |
| 14 | AA |
| 15 | AA |
| 16 | AA |
| 17 | AA |
| 18 | AA |
| 19 | AA |
| 20 | AA |
| 21 | AA |
| 22 | AA |
| 23 | AA |
| 24 | AA |
| 25 | AA |
| 26 | AA |
| 27 | AA |
| 28 | AA |
| 29 | AA |
| 30 | AA |
| 31 | AA |
| 32 | AA |
| 33 | AA |
| 34 | AA |
| 35 | AA |
| 36 | AA |
| 37 | AA |
| 38 | AA |
| 39 | AA |
| 40 | AA |

```

SUBROUTINE PELIPS (ZX,ZXP,X,YI,Z,IZE,I2G,IXG,IXM,I2I,IXI,FX,FY,FZ,
1F)
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT
DIMENSION ZX(23),ZXP(23)
IF ((YI.EQ.Y).AND.(IZES.EQ.IZE)) GO TO 10
Y=YI
IZES=IZE
DZI=ZX(I2G)-ZX(IZE)
DZB=ZX(IXG)-ZX(IXM)
Z2P=DZI/DZB
Z2PY=(DZB*(ZXP(I2G)-ZXP(IZE))-DZI*(ZXP(IXG)-ZXP(IXM)))/DZB**2
C=ZX(IXI)-ZX(IXG)
CY=ZXP(IXI)-ZXP(IXG)
DZ=ZX(I2G)-ZX(I2I)
DZY=ZXP(I2G)-ZXP(I2I)
T1=C*(C+DZ/Z2P)
T2=2.0*C+DZ/Z2P
A=T1/T2
T1Y=2.0*C*CY+(Z2P*(C*DZY+CY*DZ)-C*DZ*Z2PY)/Z2P**2
T2Y=2.0*CY+(Z2P*DZY-DZ*Z2PY)/Z2P**2
AY=(T2*T1Y-T1*T2Y)/T2**2
AMC=A-C
B2=DZ**2-AMC*DZ*Z2P
B2Y=2.0*DZ*DZY-AMC*(DZ*Z2PY+Z2P*DZY)-DZ*Z2P*(AY-CY)
XO=ZX(IXI)-A
XOY=ZXP(IXI)-AY
IF (SQRT(B2).GT.1.5*ABS(ZX(I2G)-ZX(I2I))) GO TO 20
IF (IPRINT.GT.1) WRITE (IOU6,30) B2,DZ,T1,T2,Z2P,IZE,YI,Z,ZX
D=(X-XO)/A
OY=(-A*XOY-(X-XO)*AY)/A**2
ZM2=Z-ZX(I2I)
F=ZM2**2+B2*(D**2-1.0)
FY=2.0*(B2*D*DY-ZM2*ZXP(I2I))+B2Y*(D**2-1.0)
FX=2.0*D*B2/A
FZ=2.0*ZM2
IF (IPRINT.GT.1) WRITE (IOU6,30) F,FX,FZ,A,B2,D,DY,XO,XOY
RETURN
ZSQ=SQRT(1.-(Z-ZX(I2I))**2/B2)
F=X-XO-A*ZSQ
FX=1.

```

10

20

AA 41
AA 42
AA 43
AA 44
AA 45
AA 46
AA 47

FZ=A/B2*(Z-ZX(IZI))/ZSQ
FY=-XOY-AV*ZSQ-FZ*(ZXP(IZI)+.5*(Z-ZX(IZI)))/B2*B2Y/B2)
RETURN

C
C 30

FORMAT (17H0*****PELIPS**** / (8G15.7))
END

| | | |
|--|----|----|
| | 1 | AB |
| | 2 | AB |
| | 3 | AB |
| | 4 | AB |
| | 5 | AB |
| | 6 | AB |
| | 7 | AB |
| | 8 | AB |
| | 9 | AB |
| | 10 | AB |


```

SUBROUTINE CONPIC (C,NC,XP,YP,DYP,IND)
DIMENSION C(8,4)
IND=0
DO 10 I=1,NC
IF ((XP-GE.C(1,I)).AND.(XP-LE.C(2,I))) GO TO 20
CONTINUE
IND=1
CALL CONICF (C(3,I),C(4,I),C(5,I),C(6,I),C(7,I),C(8,I),XP,YP,DYP)
RETURN
END
10
20

```

| | | |
|----|----|--|
| 1 | AC | |
| 2 | AC | |
| 3 | AC | |
| 4 | AC | |
| 5 | AC | |
| 6 | AC | |
| 7 | AC | |
| 8 | AC | |
| 9 | AC | |
| 10 | AC | |
| 11 | AC | |
| 12 | AC | |


```

SUBROUTINE XSUBG (ZX,ZXP,R)
DIMENSION ZX(11),ZXP(11)
T1=ZX(21)-ZX(5)
T2=ZX(16)-ZX(18)
T3=ZX(14)-ZX(18)
ZX(19)=ZX(21)-T1*T2/(R*T3)
ZXP(19)=ZXP(21)-(T3*(T2*(ZXP(21)-ZXP(5))+T1*(ZXP(16)-ZXP(18)))-T1*
1T2*(ZXP(14)-ZXP(18)))/(R*T3*T3)
ZX(20)=ZX(19)
ZXP(20)=ZXP(19)
RETURN
END

```

| | |
|----|----|
| AD | 1 |
| AD | 2 |
| AD | 3 |
| AD | 4 |
| AD | 5 |
| AD | 6 |
| AD | 7 |
| AD | 8 |
| AD | 9 |
| AD | 10 |
| AD | 11 |
| AD | 12 |
| AD | 13 |
| AD | 14 |
| AD | 15 |
| AD | 16 |
| AD | 17 |
| AD | 18 |
| AD | 19 |
| AD | 20 |
| AD | 21 |
| AD | 22 |
| AD | 23 |
| AD | 24 |
| AD | 25 |
| AD | 26 |
| AD | 27 |
| AD | 28 |

```

SUBROUTINE AERO (NPC,SINA,COSA)
COMMON /CP/ B(99,4,2),DRAG,ALIFT,TORQUE,YMT,ZMT,WINGA
COMMON /IO/ IOU5,IOU6,IOU7,IPRINT,EPSLN,OP,DTHTA,DPS1,KP4,IOU3
DO 10 I=1,2
DO 10 J=2,NPC
DO 10 K=1,2
L=J+K-1
M=(3-K)*I+(3-I)*K-3
CPA=(B(L,4,M)+B(J+1,4,1)+B(J,4,3-I))/(6.0*WINGA)
YA=(B(L,2,M)+B(J+1,2,1)+B(J,2,3-I))/3.0
ZA=(B(L,3,M)+B(J+1,3,1)+B(J,3,3-I))/3.0
IF (I.NE.K) CPA=-CPA
DARY=CPA*(B(J+1,3,1)-B(L,3,M))*(B(J,1,3-I)-B(L,1,M))-(B(J+1,1,I)-
1B(L,1,M))*(B(J,3,3-I)-B(L,3,M)))
DARZ=CPA*(B(J+1,1,1)-B(L,1,M))*(B(J,2,3-I)-B(L,2,M))-(B(J+1,2,I)-
1B(L,2,M))*(B(J,1,3-I)-B(L,1,M)))
DRAG=DRAG+DARY*COSA+DARZ*SINA
ALIFT=ALIFT+DARZ*COSA-DARY*SINA
TORQUE=TORQUE+DARY*(ZA-ZMT)-DARZ*(YA-YMT)
FY=DRAG*COSA-ALIFT*SINA
FZ=DRAG*SINA+ALIFT*COSA
WRITE (IOU6,20) DRAG,ALIFT,TORQUE,YMT,ZMT,FY,FZ
RETURN
10
C
C
20
FORMAT (1H0,T7,4HDRAG,T22,4HLIFT,T35,6HMOMENT,T47,13HPIVOT POINT Y
1,T68,1HZ,T80,7HY-FORCE,T95,7HZ-FORCE/TG15.6)
END

```


| | |
|----|----|
| AE | 1 |
| AE | 2 |
| AE | 3 |
| AE | 4 |
| AE | 5 |
| AE | 6 |
| AE | 7 |
| AE | 8 |
| AE | 9 |
| AE | 10 |
| AE | 11 |
| AE | 12 |

```

SUBROUTINE SETCP (LNTAPE,IB,A,B,SINE,COSINE,DUMMY,GF,FMSTR,N2)
DIMENSION A(99,8),B(99,4,2)
REWIND LNTAPE
READ (LNTAPE) ((A(L,M),M=1,8),L=2,N2)
DO 10 I=2,N2
  B(I,1,IB)=COSINE*A(I,1)-SINE*A(I,2)
  B(I,2,IB)=SINE*A(I,1)+COSINE*A(I,2)
  B(I,3,IB)=A(I,3)
  B(I,4,IB)=2.0*(A(I,7)*DUMMY-1.0)/(GF*FMSTR*FMSTR)
REWIND LNTAPE
RETURN
END

```

10

SECTION VII

FUNCTIONAL DESCRIPTION OF SUBROUTINES

- | | |
|--------|--|
| BULK | - Coordinates the three basic modes of computation: body point, field point, and shock point calculations. It establishes the position of a new point at each iteration and checks to see if the convergence criteria are satisfied. |
| PICK | - Picks the appropriate data points from the last computed data surface for each of the three basic modes of computation. |
| BASEPT | - Determines the location of the base point (the intersection of a line joining two data points with the backward facing Mach conoid) and the flow properties at this point. |
| COEFS | - Computes the values of the coefficients of the compatibility relation in the generalized finite-difference form for each of the three basic computations. |
| COMPAT | - Solves the nonlinear equation resulting from manipulation of the compatibility relations for the shock point computation. |
| GMTRY | - Finds a new body point and the unit normal at that point. |
| FIGURE | - Describes a slab-delta-wing type body through six conic-section curves and provides the unit normal at any specified body point. |
| TRANS | - Transforms to and from a body-normal oriented coordinate system. |
| ROTATE | - Rotates a two-dimensional vector through an angle. |
| SOL | - Solves three simultaneous linear equations. |
| HARNES | - Calculates the average between the locally computed shock normal and the shock normal determined from the shape of the shock surface and recomputes the local velocity behind the shock, using the average normal. |
| MIRROR | - Sets the mirror point properties across the plane of symmetry. |
| NORM | - Normalizes a vector. |
| DATOUT | - Performs all output options. |
| TIDYUP | - Rearranges the data points along the data rings. |
| REFORM | - Rearranges the data rings on a data surface. |
| KURFIT | - Provides the coefficients of a cubic spline for data interpolation. |
| KURVE | - Performs data interpolation through a cubic spline. |
| ROTXY | - Rotates the X-Y coordinates. |
| CONICF | - Computes Y and Y' from conic-section coefficients. |
| CUBIC | - Computes the cubic contour near the fuselage-canopy juncture. |

| | |
|--------|--|
| ELIPSE | - Computes the elliptic contour of the fuselage. |
| WINGF | - Computes the upper or lower wing contour. |
| PCRCL | - Computes the upper blending circular contour. |
| PELIPS | - Computes the partial ellipse contour near the wing leading edge. |
| CONPIC | - Computes the upper limit point of the upper blending contour. |
| XSUBG | - Determines the X abscissa of point G of Figure 15. |
| AERO | - Computes the pressure coefficient and moments. |
| SETCP | - Collects relevant data for AERO. |
| SECOND | - Makes interpolation using the 2nd order Lagrange's formula. |

PART 3: THE SURFACE FIT AND MINIMUM SEARCH PROGRAM

SECTION I

INTRODUCTION

Latin Squares are used to sample configurations for wave drag calculations. Corresponding to each cell of the Square, a configuration exists which can be represented by a set of body describing input data. Both 5 x 5 and 3 x 3 Latin Squares are used: the former is for Phase I study and the latter, Phase II study. Six variables z_1, \dots, z_6 can be treated by a 5 x 5 Latin Square and four variables z_1, \dots, z_4 by a 3 x 3 Latin Square. These reduced variables z_i are related to the physical variables x_i through the formula

$$x_i = \frac{x_{i\max} + x_{i\min}}{2} + \frac{z_i (x_{i\max} - x_{i\min})}{n-2}$$

where $n = 6$ for a 5 x 5 Latin Square and 4 for a 3 x 3 Latin Square. The advantage of the reduced variables is that a program written in terms of them is valid for any physical variables with any ranges of variation.

When the wave drag coefficients C_{DW} have been calculated as input data, the Surface Fit and Minimum Search program is used to obtain the coefficients b_o , b_i , and b_{ij} of the wave drag equation*

$$C_{DW} = b_o + \sum b_i z_i + \sum b_{ij} z_i z_j$$

through a least square procedure; in other words, the program is used to fit a hypersurface in an n dimensional space. When the type of constraints is specified, the program is used to yield a set of values for the z_i that corresponds to a minimum wave drag body subject to the given constraints.

* i and j range from 1 to n ; however, as explained in Volume I, not every possible term is included.

SECTION II

GUIDE TO THE SEARCH PROCEDURE

In the search procedure, wave drag coefficients are computed using the wave drag equation at points covering the entire region bounded by the given ranges of variables in the n -dimensional space. The point which has the least wave drag is taken to define the minimum wave drag configuration. The accuracy of locating the minimum is therefore dependent on the resolution of the numerical network. Accurate location of the minimum can be obtained efficiently by a search-by-steps technique where the search is first conducted using coarser grids to determine an approximate location, and then repeated in a smaller region centered around the location of the previously obtained minimum. This process can be repeated as many times as needed to obtain the desired accuracy. The major advantage is that the given constraints can be satisfied easily by rejecting points which violate the constraints.

1. SEARCH STEPS

The searching procedure is summarized as follows:

- a. Select the ranges of search by specifying the lower and upper limits of each of the n number of reduced variables:*

$$(z_L)_j, (z_u)_j \quad j = 1, n \quad \begin{cases} n = 4 \text{ for } 3 \times 3 \text{ Latin Square} \\ n = 6 \text{ for } 5 \times 5 \text{ Latin Square} \end{cases}$$

- b. Select the resolution for each of the variables by specifying the numbers of grid points N_j ($j = 1, n$) of that variable. The resolution is given by

$$\text{resolution} = \frac{(z_u)_j - (z_L)_j}{N_j - 1}$$

* $(z_L)_j \equiv O(J)$, $(z_u)_j \equiv E(J)$, and $N_j \equiv NP(J)$ in the input data described in Section III.

The total number of points for each search cycle is equal to the product of N_j , i. e.,

$$\text{total points} = \prod_{j=1}^n N_j$$

For example, if 10 points are specified for all variables, the total number of points for $n = 6$ is 10^6 . To keep the searching time within practical limit, N_j must therefore be selected carefully so that the total number of searching points is within reasonable limits.* Using the data of a. and b., the program computes the n tables of variables:

$$(z_i)_j \left\{ \begin{array}{l} i = 1, N_j \\ (z_1)_j = (z_L)_j ; (z_N)_j = (z_u)_j \end{array} \right\} j = 1, n$$

so that all configurations defined by every possible combination of the n variables,

$$(z_i)_1, (z_i)_2, \dots, (z_i)_n$$

can be checked for the given constraints (e. g., the volume). The configuration which has the minimum wave drag coefficient computed by the wave drag equation is considered the minimum wave drag configuration.

- c. If the search is to be repeated, select the new ranges of the n variables by redefining the lower and upper limits as,

$$(z_L)_j = z_j' - \Delta_j, (z_u)_j = z_j' + \Delta_j$$

where z_j' are the variables for the minimum wave drag configuration determined previously, and Δ_j are arbitrary increments of z_j selected to define a smaller region of search. In situations where $(z_L)_j$ or $(z_u)_j$ defined by

*See Section IV for time estimates.

above relations are beyond the ranges of consideration, they are then set equal to the minimum or maximum of the range.

- d. Repeat the procedure from step b, until the desired accuracy is obtained.

2. TYPES OF CONSTRAINTS

Four types of geometric constraints are included in order to satisfy most design needs. These are:

- a. One or more of the six geometric variables take assigned values within the ranges of variation. For instance, the length can be kept the same as that of the baseline or the width can take 90% of the baseline width.
- b. At one or more fuselage stations the configuration cross sections contain geometric curves prescribed by tabulated data of width X versus elevation Z . This type of constraint is useful for the placement of equipment. In the case of the radome constraint, only the radome radius and the elevation of the center need to be specified.
- c. At one or more fuselage stations the configuration cross sections satisfy minimum area requirements. The minimum area can be either a given area or a certain percentage of the baseline cross-sectional area.
- d. The configuration satisfies a minimum volume requirement between two given stations. A given volume or a certain percentage of the baseline volume can be imposed.

SECTION III

INPUT/OUTPUT DESCRIPTION

Two different sizes of Latin Squares are used in Phase I and Phase II; the input and output of these two phases are described in this section.

1. INPUT DESCRIPTION

The input data cards for Phase I program LATIN1 and Phase II program LATIN2 are shown in Figures 22 and 23. The cards are described below:

Phase I Program LATIN1 Input

| Card No | Variable | Format | Description |
|---------|--|--|--|
| ① | $\begin{bmatrix} \text{SYM}(1) \\ \vdots \\ \text{SYM}(6) \end{bmatrix}$ | $\begin{bmatrix} 3 \times \text{A2} \\ \vdots \\ 3 \times \text{2A} \end{bmatrix}$ | Alphanumeric symbols to identify reduced variables z_1, \dots, z_6 in print out |
| ② | $\begin{bmatrix} \text{IOR} \\ \text{IPRINT} \end{bmatrix}$ | 15
15 | Number of terms in the Wave Drag equation
Print out control

IF IPRINT $\begin{cases} = 0, \text{ Minimum Print} \\ = 1, \text{ detail print about surface fit} \end{cases}$ |
| ③ | KIND | 15 | Constraint Control

If KIND $\begin{cases} = 0, \text{ no constraint; or constraints imposed on one or more of the variables} \\ = 1, \text{ local area-ratio constraint} \\ = 2, \text{ local tabulated X-vrs-Z constraint} \\ = 3, \text{ randome constraint} \\ = 4, \text{ volume constraint} \end{cases}$ |

• Use card 4₁ if KIND = 1 or 2

| Card No | Variable | Format | Description |
|--|------------|--------|--|
| ④ ₁ | FS | F9.2 | Fuselage station at which cross-sectional area constraint is imposed |
| | RATIO | F9.2 | Ratio of desired area to baseline cross-sectional area at this F. S. if $0 < \text{RATIO} \leq 2$ |
| | | | Desired cross-sectional area at this F. S. if $\text{RATIO} > 2$ |
| | | | Not used if $\text{KIND} = 2$; may be left blank |
| • Add cards 4 ₂ and 5 ₂ if $\text{KIND} = 2$ | | | |
| ④ ₂ | NPFS | 15 | Number of points in the table |
| ⑤ ₂ | ZFS(1) | F9.2 | Elevation Z(1) of the first point |
| | XFS(1) | F9.2 | Width X(1) of the first point |
| | ⋮ | ⋮ | |
| | ZFS(NPFS) | F9.2 | Elevation Z(NPFS) of the NPFS th point |
| | XFS(NPFS) | F9.2 | Width X(NPFS) of the NPFS th point |
| • Use card 4 ₃ if $\text{KIND} = 3$ | | | |
| ④ ₃ | FS | F9.2 | Fuselage station at which the radome constraint is imposed |
| | FC | F9.2 | Z value of radome center |
| | RD | F9.2 | Radius of Radome |
| • Use cards 4 ₄ and 5 ₄ if $\text{KIND} = 4$ | | | |
| ④ ₄ | FS1 | F10.2 | Fuselage stations between which the volume constraints is imposed. Note that if $\text{FS1} < 50$ the complete nose is included. |
| | FS2 | F10.2 | |
| | ANY | F10.2 | Ratio of desired volume to baseline volume if $0 < \text{ANY} \leq 2$ |
| | | | Desired volume if $\text{ANY} > 2$ |
| | NFSI | 15 | Number of specified fuselage stations at which cross-sectional areas are calculated for volume integration |
| ⑤ ₄ | FS(2) | F9.2 | Fuselage Stations at which cross-sectional areas are calculated for volume integration |
| | FS(NFSI-1) | F9.2 | |
| ⑥ | Blank Card | | Must be present to terminate the input string |

| Card No | Variable | Format | Description |
|--|---|---|---|
| ⑦ | $\begin{bmatrix} J \\ \text{ANY} \end{bmatrix}$ | $\begin{bmatrix} I2 \\ F10.0 \end{bmatrix}$ | <p>Cell number of the Latin Square</p> <p>Wave Drag Coefficient for Jth cell</p> |
| • There follow 24 cards like card 7 | | | |
| ⑧ | $\begin{bmatrix} J \\ \text{ANY} \\ V(1) \\ \vdots \\ V(6) \end{bmatrix}$ | $\begin{bmatrix} I2 \\ F10.0 \\ F10.0 \\ \vdots \\ F10.0 \end{bmatrix}$ | <p>Identification number (starting from 26) for additional input of wave drag coefficient</p> <p>Wave drag coefficient for Jth addition</p> <p>Value of reduced variable z_1 for Jth addition</p> <p>Value of reduced variable z_6 for Jth addition</p> |
| • There follow additional cards like card 8 | | | |
| ⑨ | Blank card | | Must be present to terminate the input string. |
| • If KIND \neq 4, go to card 13 | | | |
| ⑩ | $\begin{bmatrix} J \\ \text{ANY} \end{bmatrix}$ | $\begin{bmatrix} I2 \\ F10.0 \end{bmatrix}$ | <p>Cell number of the Latin Square</p> <p>Nose volume up to F. S. 50 for Jth cell*</p> |
| • There follow 24 cards like card 10 | | | |
| ⑪ | $\begin{bmatrix} J \\ \text{ANY} \end{bmatrix}$ | $\begin{bmatrix} I2 \\ F10.0 \end{bmatrix}$ | <p>Identification number for additional nose volume input</p> <p>Nose volume for Jth addition</p> |
| • There follow additional cards like card 11 | | | |
| ⑫ | Blank card | | Must be present to terminate the input string |
| ⑬ | $\begin{bmatrix} \text{NP}(1) \\ \vdots \\ \text{NP}(6) \end{bmatrix}$ | $\begin{bmatrix} I5 \\ \vdots \\ I5 \end{bmatrix}$ | <p>Number of evenly spaced grid points for reduced variable z_1 for the search process</p> <p>Number of evenly spaced grid points for reduced variable z_6 for the search process</p> |
| ⑭ | $\begin{bmatrix} O(1) \\ \vdots \\ O(6) \end{bmatrix}$ | $\begin{bmatrix} F9.2 \\ \vdots \\ F9.2 \end{bmatrix}$ | <p>Lower limit of the search interval for z_1</p> <p>Lower limit of the search interval for z_6</p> |

*See Section IV for volume calculations.

| Card No | Variable | Format | Description |
|---------|----------|--------|--|
| ⑮ | E(1) | F9.2 | Upper limit of the search interval for z_1 |
| | E(6) | F9.2 | Upper limit of the search interval for z_6 |

Phase II Program LATIN2 Input

| Card No | Variable | Format | Description |
|--|---|--------|---|
| ① | SYM(1) | 3 x A2 | Alphanumeric symbols to identify reduced variables z_1, \dots, z_4 in print out |
| | SYM(4) | 3 x A2 | |
| ② | IOR | I5 | Number of terms in the wave drag equation |
| | IPRINT | I5 | Print out control |
| If IPRINT $\left\{ \begin{array}{l} = 0, \text{ minimum print} \\ = 1, \text{ detail print about surface fit} \end{array} \right.$ | | | |
| ③ | KINDT | I5 | Constraint control |
| | If KINDT $\left\{ \begin{array}{l} = 0, \text{ no constraints; or constraints imposed on one or more of the variables} \\ = 1, \text{ volume constraint} \end{array} \right.$ | | |
| ④ | VOLBIN | F10.0 | Volume increment desired (i. e., the desired volume minus the baseline volume)* |
| | J | I2 | Cell number of the Latin Square |
| ⑤ | ANY | F10.0 | Wave drag coefficient for Jth cell |
| ● There follow 8 cards like card 4 | | | |
| ⑤ | J | I2 | Identification number (starting from 10) for additional input of wave drag coefficients |
| | ANY | F10.0 | Wave drag coefficient for Jth addition |

*See Section IV for volume calculations.

| Card No | Variable | Format | Description |
|---------|----------|--------|--|
| ⑤ | V(1) | F10.0 | Value of reduced variable z_1 for Jth addition |
| | ⋮ | ⋮ | |
| | V(4) | F10.0 | Value of reduced variable z_4 for Jth addition |

• There follow additional cards like card 5

| | | | |
|---|------------|--|--|
| ⑥ | Blank Card | | Must be present to terminate the input string. |
|---|------------|--|--|

• If KINDT = 0, go to card 10

| | | | |
|---|-----|-------|--|
| ⑦ | J | I2 | Cell number of the Latin Square |
| | ANY | F10.0 | Volume increment for Jth cell (i. e., volume of Jth configuration minus the baseline volume) |

• There follow 8 cards like card 7

| | | | |
|---|-----|-------|---|
| ⑧ | J | I2 | Identification number for additional volume increment input |
| | ANY | F10.0 | Volume increment for Jth addition |

• There follow additional cards like card 8

| | | | |
|---|------------|--|---|
| ⑨ | Blank card | | Must be present to terminate the input string |
|---|------------|--|---|

| | | | |
|---|-------|----|---|
| ⑩ | NP(1) | I5 | Number of evenly spaced grid points for reduced variable z_1 for the search process |
| | ⋮ | ⋮ | |
| | NP(4) | I5 | Number of evenly spaced grid points for reduced variable z_4 for the search process |

| | | | |
|---|------|------|--|
| ⑪ | O(1) | F9.2 | Lower limit of the search interval for z_1 |
| | ⋮ | ⋮ | |
| | O(4) | F9.2 | Lower limit of the search interval for z_4 |

| | | | |
|---|------|------|--|
| ⑫ | E(1) | F9.2 | Upper limit of the search interval for z_1 |
| | ⋮ | ⋮ | |
| | E(4) | F9.2 | Upper limit of the search interval for z_4 |

2. OUTPUT DESCRIPTION

Sample printouts of LATIN1 (5 x 5 Latin Square) and LATIN2 (3 x 3 Latin Square) are shown in Figures 24 through 27. Figure 24 shows the results of the drag coefficient surface fit for the 5 x 5 Latin Square. The input data shown in Figure 24 includes the drag coefficient for the basic 25 Latin Square cells plus 7 additional configurations including the baseline (No. 26). With the 7 additional drag coefficients, 6 additional terms were added to the wave drag equation (see Appendix A of Volume 1). Figure 25 shows the 5 x 5 Latin Square surface fit of the nose volume. The printout is similar to that of the drag coefficient. Figure 26 shows the results of a minimum wave drag configuration search with volume constraint. Here the search was made keeping the variable z_1 at a constant value of 0, while the remaining 5 variables z_2, \dots, z_5 were varied through 5 discreet points between -2.0 and 2.0. That is, the resolution of each of the 5 searching variables in this search cycle is equal to 1.0. The minimum wave drag configuration, within the given ranges of variables and resolution is printed along with its cross-sectional areas and volume. The number of configurations which do not satisfy the volume constraint is indicated by the number of points rejected. Figure 27 shows a sample output of the 3 x 3 Latin Square surface fit and the minimum value search results with volume constraint. The printout is similar to that of the 5 x 5 Latin Square results. Here, however, the fitted volume is the complete fuselage canopy and wing, and the numerical values shown are the differences from the baseline.

LATIN SQUARE MINIMUM VALUE SEARCH PROGRAM
 VARIABLES ARE LISTED AS . . . L B F H A
 ORDER OF FIT . . . 23
 CONSTRAINT = 4-VOLUME

ADDITIONAL TERMS ARE . . .

(18) L L
 (19) A A
 (20) L H
 (21) B A
 (22) L B
 (23) H A

INPUT DATA . . . *WAVE DRAG*

1 8.722590
 2 5.970170
 3 5.724920
 4 5.884690
 5 5.952560
 6 7.625800
 7 7.254040
 8 7.105100
 9 5.439380
 10 5.760620
 11 0.526840
 12 0.673050
 13 0.591540
 14 0.861430
 15 7.610590
 16 8.217730
 17 8.688300
 18 6.438170
 19 0.618100
 20 5.939600
 21 7.630460
 22 8.222750
 23 0.625220
 24 7.248460
 25 5.876170
 26 0.694370
 27 0.572600
 28 0.095690
 29 5.955290
 30 5.863430
 31 0.814490
 32 0.118840

COEFFICIENTS OF WAVE DRAG EQUATION

| | | | | |
|---------------------|--------------------|--------------------|---------------------|--------------------|
| (1) 6.589280 | (2) -.3965690 | (3) .1952752 | (4) .2064617E-02 | (5) .4552590 |
| (6) -.2050504E-01 | (7) .2688061 | (8) .3790653E-01 | (9) -.4525385E-03 | (10) .4179457E-01 |
| (11) .2906077E-01 | (12) -.2480445E-01 | (13) .5690592E-01 | (14) .1303170E-01 | (15) -.1453514E-01 |
| (16) -.2082480E-01 | (17) -.4708812E-02 | (18) .4236248E-01 | (19) .1710669E-01 | (20) -.4901643E-01 |
| (21) .2862795E-01 | (22) .1614830E-01 | (23) .1834393E-02 | | |

STD DEV= .71811E-01

FITTED WAVE DRAG

| | | | | |
|----------------|----------------|----------------|----------------|----------------|
| (1) 8.657905 | (2) 5.936778 | (3) 5.756353 | (4) 5.968195 | (5) 5.927520 |
| (6) 7.716832 | (7) 7.130031 | (8) 7.199410 | (9) 5.445890 | (10) 5.702036 |
| (11) 6.609727 | (12) 6.476629 | (13) 6.589280 | (14) 6.947679 | (15) 7.551826 |
| (16) 8.263872 | (17) 8.683826 | (18) 6.355805 | (19) 6.736829 | (20) 5.841928 |
| (21) 7.645751 | (22) 8.136829 | (23) 8.601087 | (24) 7.299810 | (25) 5.939397 |
| (26) 6.782620 | (27) 6.607058 | (28) 6.056381 | (29) 5.948000 | (30) 5.862854 |
| (31) 6.801438 | (32) 6.143416 | | | |

ERROR OF FIT

| | | | | |
|--------------------|---------------------|--------------------|--------------------|---------------------|
| (1) -.646445E-01 | (2) -.3339190E-01 | (3) .3143257E-01 | (4) .8350464E-01 | (5) -.2503977E-01 |
| (6) .9103227E-01 | (7) -.1240094 | (8) .9430971E-01 | (9) .6510390E-02 | (10) -.5858410E-01 |
| (11) .8288685E-01 | (12) -.1964207 | (13) -.2259986E-02 | (14) .8624890E-01 | (15) -.5876402E-01 |
| (16) .4614162E-01 | (17) -.4473969E-02 | (18) -.8236504E-01 | (19) .1187293 | (20) -.9767153E-01 |
| (21) .1529119E-01 | (22) -.8592102E-01 | (23) -.2413316E-01 | (24) .5134994E-01 | (25) .6322689E-01 |
| (26) .8824958E-01 | (27) .3445787E-01 | (28) -.3930931E-01 | (29) -.7290010E-02 | (30) -.5763780E-03 |
| (31) -.1305239E-01 | (32) .2457550E-01 | | | |

FIGURE 24. SURFACE FIT OF WAVE DRAG COEFFICIENTS (5 x 5 LATIN SQUARE)

INPUT DATA.... *VOLUME*

| | | | | | |
|-----------------|-----------|-------|-----------|-------|-----------|
| 1 | 27969.00 | | | | |
| 2 | 24190.00 | | | | |
| 3 | 22492.00 | | | | |
| 4 | 27633.00 | | | | |
| 5 | 31198.00 | | | | |
| 6 | 25953.00 | | | | |
| 7 | 26918.00 | | | | |
| 8 | 31499.00 | | | | |
| 9 | 25273.00 | | | | |
| 10 | 30202.00 | | | | |
| 11 | 22460.00 | | | | |
| 12 | 26212.00 | | | | |
| 13 | 29430.00 | | | | |
| 14 | 34228.00 | | | | |
| 15 | 37811.00 | | | | |
| 16 | 28259.00 | | | | |
| 17 | 33819.00 | | | | |
| 18 | 29035.00 | | | | |
| 19 | 32614.00 | | | | |
| 20 | 30919.00 | | | | |
| 21 | 26603.00 | | | | |
| 22 | 31917.00 | | | | |
| 23 | 35621.00 | | | | |
| 24 | 36351.00 | | | | |
| 25 | 31103.00 | | | | |
| 26 | 25076.00 | | | | |
| 27 | 25055.00 | | | | |
| 28 | 23565.00 | | | | |
| 29 | 21192.00 | | | | |
| 30 | 20452.00 | | | | |
| 31 | 27049.00 | | | | |
| 32 | 27194.00 | | | | |
| (1) | 29697.09 | (2) | 1468.806 | (3) | 854.0985 |
| (6) | -189.2461 | (7) | 1423.439 | (8) | -195.7796 |
| (11) | -184.8959 | (12) | 111.8339 | (13) | -189.0630 |
| (16) | 230.2987 | (17) | 325.6316 | (18) | -54.28646 |
| (21) | 372.5243 | (22) | -251.2878 | (23) | 320.3092 |
| STD DEV= 212.15 | | | | | |
| (1) | 28199.48 | (2) | 23933.67 | (3) | 22326.73 |
| (6) | 25911.69 | (7) | 26861.34 | (8) | 31465.42 |
| (11) | 22483.77 | (12) | 25957.68 | (13) | 29697.09 |
| (16) | 28234.93 | (17) | 33408.26 | (18) | 29127.16 |
| (21) | 26743.74 | (22) | 31698.24 | (23) | 35829.78 |
| (26) | 25439.63 | (27) | 25164.94 | (28) | 23504.00 |
| (31) | 26999.85 | (32) | 27234.34 | (3) | |
| ERROR OF FIT | | | | | |
| (1) | 230.4782 | (2) | -256.3349 | (3) | -165.2720 |
| (6) | -41.31367 | (7) | -56.65509 | (8) | -33.57555 |
| (11) | 23.77196 | (12) | -254.3200 | (13) | 267.0949 |
| (16) | -24.07026 | (17) | -410.7430 | (18) | 92.16195 |
| (21) | 140.7384 | (22) | -218.7605 | (23) | 208.7771 |
| (26) | 363.6349 | (27) | 109.9404 | (28) | -61.00450 |
| (31) | -49.14077 | (32) | 40.34173 | (3) | |
| (4) | -39.72363 | (5) | 1778.234 | (6) | 56.59233 |
| (9) | 260.7751 | (10) | 202.7722 | (11) | 108.9358 |
| (14) | 114.5688 | (15) | -288.7734 | (16) | |
| (19) | | (20) | | (21) | |
| (24) | | (25) | | (26) | |
| (29) | | (30) | | (31) | |
| (32) | | (33) | | (34) | |
| (35) | | (36) | | (37) | |
| (38) | | (39) | | (40) | |
| (41) | | (42) | | (43) | |
| (44) | | (45) | | (46) | |
| (47) | | (48) | | (49) | |
| (50) | | (51) | | (52) | |
| (53) | | (54) | | (55) | |
| (56) | | (57) | | (58) | |
| (59) | | (60) | | (61) | |
| (62) | | (63) | | (64) | |
| (65) | | (66) | | (67) | |
| (68) | | (69) | | (70) | |
| (71) | | (72) | | (73) | |
| (74) | | (75) | | (76) | |
| (77) | | (78) | | (79) | |
| (80) | | (81) | | (82) | |
| (83) | | (84) | | (85) | |
| (86) | | (87) | | (88) | |
| (89) | | (90) | | (91) | |
| (92) | | (93) | | (94) | |
| (95) | | (96) | | (97) | |
| (98) | | (99) | | (100) | |

FIGURE 25. SURFACE FIT OF NOSE VOLUME (5 x 5 LATIN SQUARE)

INPUT NO. OF PTS.
 1 5 5 5 5
 INPUT LOWER LIMITS
 0. -2.0 -2.0 -2.0 -2.0
 INPUT UPPER LIMITS
 2.0 2.0 2.0 2.0 2.0
 1041 POINTS REJECTED
 2064 POINTS ACCEPTED
 AVERAGE = 7.2638

MINIMUM DRAG CONFIGURATION

| CD | L | B | F | H | A# | A |
|---|----------|-----------|----------|-----------|----------|----|
| 6.114940 | 0. | -1.000000 | 2.000000 | -1.000000 | 1.000000 | 0. |
| KIND.FS.ABASE.AMIN | 4 50.000 | 745.94 | 705.32 | | | |
| KIND.FS.ABASE.AMIN | 4 90.000 | 1003.5 | 1005.7 | | | |
| KIND.FS.ABASE.AMIN | 4 150.00 | 1438.0 | 1437.7 | | | |
| KIND.FS.ABASE.AMIN | 4 190.00 | 1641.8 | 1650.0 | | | |
| KIND.FS.ABASE.AMIN | 4 200.00 | 1685.3 | 1697.6 | | | |
| KIND.FS.ABASE.AMIN | 4 205.00 | 1706.5 | 1720.9 | | | |
| KIND.FS.ABASE.AMIN | 4 210.00 | 1747.9 | 1765.1 | | | |
| KIND.FS.ABASE.AMIN | 4 215.00 | 1782.1 | 1801.7 | | | |
| KIND.FS.ABASE.AMIN | 4 220.00 | 1775.4 | 1796.0 | | | |
| KIND.FS.ABASE.AMIN | 4 225.00 | 1768.6 | 1790.1 | | | |
| KIND.FS.ABASE.AMIN | 4 -0. | 272.37 | 256.48 | | | |
| KIND.FS.ABASE.AMIN | 4 230.00 | 1761.8 | 1784.2 | | | |
| VOLUME - BASELINE.MIN. CONF..NOSE... 264920.7 266021.9 26088.12 | | | | | | |

FIGURE 26. MINIMUM VALUE RESULTS WITH VOLUME CONSTRAINT
(5 x 5 LATIN SQUARE)

```

INPUT ORDER OF FIT - 8 THRU 14
10R,IPRINT      10      1

VOLUME CONSTRAINT: VOLUME      116486.8      GREATER THAN BASELINE

ADDITIONAL TERMS ARE. . . .
(10)  H H

INPUT DATA.... *WAVE DRAG*
  1 .1046020E-01
  4 .9455500E-02
  7 .1166290E-01
  2 .1165250E-01
  5 .1040130E-01
  8 .1142970E-01
  3 .1078680E-01
  6 .1283200E-01
  9 .1143090E-01
 10 .9793590E-02

      COEFFICIENTS OF WAVE DRAG EQUATION
( 1) .1040130E-01 ( 2) .2706667E-03 ( 3) .5785167E-03 ( 4) .3638333E-03 ( 5) .7459000E-03
( 6) .2598000E-03 ( 7) .5391000E-03 ( 8) -.1181679E-03 ( 9) .2227321E-03 (10) .6171788E-04
STD DEV= .69843E-15

      FITTED WAVE DRAG
( 1) .1046020E-01 ( 2) .1165250E-01 ( 3) .1078680E-01 ( 4) .9455500E-02 ( 5) .1040130E-01
( 6) .1283200E-01 ( 7) .1166290E-01 ( 8) .1142970E-01 ( 9) .1143090E-01 (10) .9793590E-02

      ERROR OF FIT
( 1) -.2775558E-15 ( 2) -.6661338E-15 ( 3) -.2775558E-15 ( 4) -.6661338E-15 ( 5) -.1609823E-14
( 6) -.6106227E-15 ( 7) -.3845781E-15 ( 8) -.6661338E-15 ( 9) -.1665335E-15 (10) -.4996004E-15
.....

INPUT DATA.... *VOLUME*
  1 -70402.30
  4 -48181.60
  7 32094.00
  2 1265.500
  5 36291.10
  8 83446.10
  3 47920.10
  6 137459.1
  9 154575.0
 10 0.

( 1) 36291.10 ( 2) 44555.30 ( 3) 71074.02 ( 4) 7140.667 ( 5) 14605.67
( 6) 4258.567 ( 7) 2174.267 ( 8) 8759.461 ( 9) 8386.327 (10) -6849.644
STD DEV= .32692E-08
( 1) -70402.30 ( 2) 1265.500 ( 3) 47920.10 ( 4) -48181.60 ( 5) 36291.10
( 6) 137459.1 ( 7) 32094.00 ( 8) 83446.10 ( 9) 154575.0 (10) -.7275958E-09

      ERROR OF FIT
( 1) .2793968E-08 ( 2) 0. ( 3) -.2328306E-08 ( 4) .2095476E-08 ( 5) -.1396984E-08
( 6) -.6519258E-08 ( 7) -.6984919E-09 ( 8) -.3725290E-08 ( 9) -.5587935E-08 (10) -.7275958E-09
.....

INPUT NO. OF PTS.
  21 21 21 21
INPUT LOWER LIMITS
-1.0 -1.0 -1.0 -1.0
INPUT UPPER LIMITS
 1.0  1.0  1.0  1.0
179282 POINTS REJECTED
15199 POINTS ACCEPTED
AVERAGE= .11728E-01

      MINIMUM DRAG CONFIGURATION
      CD      H      A      R1      R2
.1074085E-01 .6000000 -.9000000 -.8000000 .9000000
116486.8     120002.2

```

FIGURE 27. SURFACE FIT AND MINIMUM VALUE SEARCH RESULTS WITH VOLUME CONSTRAINT (3 x 3 LATIN SQUARE)

SECTION IV

OPERATIONAL ASPECTS

1. CORE AND TIME REQUIREMENTS

Both the LATIN1 and LATIN2 can be run on 60,000₈ words of memory. The computer time required for the search is dependent on the total number of search cases. As a guide it takes about 5-10 seconds for the LATIN1 program and 0.05-0.10 seconds for the Latin2 program to compute 1000 search cases. Additional 5 seconds should be allowed for compilation.

2. ERROR MESSAGES

If the number of input data is less than the requested order of Latin Square fit (number of terms in the wave drag equation) the error message,

INSUFFICIENT NO. OF INPUT DATA

will be printed and the job will be terminated.

3. VOLUME DATA PREPARATION

If the volume constraint option is used, the two minimum value search programs require the input of configuration volumes as well as wave drag coefficients. For the LATIN1 program, the input volume is that of the fuselage nose ahead of fuselage station 50, while for the LATIN2 program, the input volume is that of the complete configuration which comprises the fuselage, canopy and wings. Two auxiliary programs, which use the same body description data for the 3DMoC program, can be used to calculate the input volume data. The listings of the two volume calculation programs, one for LATIN1 and the other for LATIN2 programs, are presented below.

One input-data card is required for each of the volume calculation programs. The data required are

KASE, Y, Y2 FORMAT(I5, 2F10.2)

where KASE = an input integer to identify the body configuration (e.g., cell number)

Y1, Y2 = the fuselage stations between which the volume is to be calculated.

The values of Y1 and Y2 used in these two programs are

| | LATIN1 | LATIN2 |
|----|--------|--------|
| Y1 | 0 | 0 |
| Y2 | 50 | 430 |

```

C***FUSELAGE VOLUME CALCULATION PROCEDURE
DIMENSION ZX(13),P(13),Q(13),R(13),S(13),T(13),SG(13),ZXP(13)
DIMENSION AREA(101),YS(101)
REWIND 2
NY=101
M78=10
YMAXL=-100.
YMAX=-100.
10 WRITE(6,600)
600 FORMAT(' INPUT KASE,Y1,Y2,')
READ(5,*) KASE,Y1,Y2
XN=NY-1
DELTAY=(Y2-Y1)/XN
DO 50 LL=1,NY
XLL=LL-1
Y=Y1+DELTAY*XLL
YS(LL)=Y
DO 2 I=1,50
IF((Y.LE.YMAX).AND.(Y.GE.YMAXL)) GO TO 3
IF(Y.LT.YMAXL) REWIND 2
YMAXL=YMAX
READ(2,200) YMAX,N
M=7
DO 2 K=1,N
READ(2,201) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
IF(L.GT.7) M=13
IF((L.EQ.9).OR.(L.EQ.8)) M78=8
2 CONTINUE
200 FORMAT(F10.5,I5)
201 FORMAT(I2,SE15.8,F2.0)
3 DO 4 I=1,7
CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),ZXP(I))
4 CONTINUE
IF(M.EQ.7) GO TO 6
DO 5 I=M78,13
5 CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),ZXP(I))
IF(M78.EQ.10) SG(8) = 99.
6 CALL PLOT(Y,ZX,ZXP,M,SG,AREA(LL))
MODE=1
50 CONTINUE
CALL SIGMA2(NY,0,YS,AREA,VOL)
WRITE(6,700) KASE,VOL
700 FORMAT(I5,F15.6)

```

```

00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000290
00000300
00000310
00000320
00000330
00000340
00000350
00000360
00000370
00000380
00000390
00000400
00000410
00000420
00000430

```

00000440
00000450
00000460
00000470

500 READ(5,500) DUMMY
FORMAT(F20.0)
GO TO 10
END

00000480
00000490
00000500
00000510
00000520
00000530
00000540
00000550
00000560

```

SUBROUTINE CONICF(P,Q,R,S,T,SG,X,Y,YP)
  ROOT=SG*SQRT((R*X+S)*X+T)
  Y=P*X+Q+ROOT
  IF (SG.NE.0.) GO TO 10
  YP=P
  GO TO 20
10 YP=P+(R*X+S/2.0)/ROOT
20 RETURN
  END

```

```

SUBROUTINE PLOT(Y,ZX,ZXP,M,SG,AREA)
COMMON PRINT,NMAX
DIMENSION XP(200),ZP(200)
DIMENSION ZX(1),ZXP(1),SG(1)
N=200
XN=N-1
NM1=N-1
IF(M.EQ.7) Z1=ZX(1)
IF(M.EQ.13) Z1=ZX(10)
Z2=ZX(3)
XP(1)=0.
XP(N)=0.
ZP(1)=Z1
ZP(N)=Z2
DZ=(Z1-Z2)/XN
DO 1000 I=2,NM1
  XI=I-1
  Z=Z1-DZ*XI
  ZP(I)=-Z
  IF((M.EQ.7).OR.(SG(8).EQ.99.)) GO TO 10
  IF(Z.GT.ZX(8)) GO TO 100
  IF(Z.GT.ZX(9)) GO TO 200
  10 IF(Z.GT.ZX(2)) GO TO 300
  IF(Z.GT.ZX(3)) GO TO 400
C**LOWER FLAT
  INDEX=5
  X=ZX(6)
  GO TO 500
C**CANOPY
  100 INDEX=1
  X=XELIPS(ZX(11),ZX(10),ZX(12)-ZX(13),Z)+ZX(13)
  GO TO 500
C**CUBIC
  200 INDEX=2
  IF(SG(8).NE.99.) GO TO 15
  IF(Z.GE.ZX(1)) GO TO 300
  GO TO 400
  15 X1=XELIPS(ZX(11),ZX(10),ZX(12)-ZX(13),ZX(8))+ZX(13)
  X2=XELIPS(ZX(2),ZX(1),ZX(5)-ZX(4),ZX(9))+ZX(4)
  Z1P=XELIPP(ZX(11),ZX(10),X1+ZX(12),ZX(8))
  Z2P=XELIPP(ZX(2),ZX(1),X2+ZX(5)-ZX(4),ZX(9))
  DZ1=Z-ZX(8)
  DZ21=ZX(9)-ZX(8)

```

```

A=3.*DZ21-(Z2P+2.*Z1P)*(X2-X1)
B=-2.*DZ21+(Z2P+Z1P)*(X2-X1)
IF((Z1P.L1.-4.).OR.(Z2P.LT.-4.).OR.(Z1P.GE.0.)) GO TO 22
GO TO 18
22 TX=1
  IF(Z.EQ.ZX(8)) X=X1
  IF(Z.EQ.ZX(9)) X=X2
  IF((Z.EQ.ZX(8)).OR.(Z.EQ.ZX(9))) GO TO 500
  XI=X1
  DO 19 L=1,2
  DO 17 J=1,6
    DXR=(XI-X1)/(X2-X1)
    ZI=ZX(8)+Z1P*(XI-X1)+A*DXR**2+B*DXR**3
    ZIP=Z1P+(2.0*A*DXR+3.0*B*DXR**2)/(X2-X1)
    IF(ZIP.NE.0.) GO TO 16
    X=X1+(X2-X1)/100.
  GO TO 17
16 X=X1-(ZI-Z)/ZIP
  IF(ABS(X-X1).LE.1.E-5) GO TO 500
17 XI=X
  XI=X2
19 CONTINUE
  GO TO 500
18 DX21=X2-X1
  X1P=1.0/Z1P
  X2P=1.0/Z2P
  A=3.0*DX21-(X2P+2.0*X1P)*DZ21
  B=-2.0*DX21+(X2P+X1P)*DZ21
  DZR=(Z-ZX(8))/DZ21
  X=X1+X1P*DZ1+A*DZR**2+B*DZR**3
  GO TO 500
C**UPPER ELLIPSE
300 INDEX=3
  X=XELIPS(ZX(2),ZX(1),ZX(5)-ZX(4),Z) + ZX(4)
  GO TO 500
C**LOWER CONIC
400 INDEX=4
  CALL CONICS(ZX,ZXP,6,3,5,2,7,Z,X)
500 XP(1)=X
1000 CONTINUE
  CALL SIGMA2(N,0,ZP,XP,AREA)
  RETURN
  END
00001000
00001010
00001020
00001030
00001040
00001050
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00001070
00001080
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00001100
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00001120
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00001190
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00001400
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00001420

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00001430
00001440
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00001470

```
FUNCTION XELIPS(Z1,Z2,X,Z)
XELIPS=X*SQRT(1.0-((Z-Z1)/(Z2-Z1))**2)
XELIPS=ABS(XELIPS)
RETURN
END
```


00001480
00001490
00001500
00001510

FUNCTION XELIPP(Z1,Z2,X1,X,Z)
XELIPP=-X1/(Z-Z1)*((Z2-Z1)/X)**2
RETURN
END

00001520
 00001530
 00001540
 00001550
 00001560
 00001570
 00001580
 00001590
 00001600
 00001610
 00001620
 00001630

```

SUBROUTINE CONICS(ZX,ZXP,ICX,ICZ,ISX,ISZ,IB,L,X)
  DIMENSION ZX(1),ZXP(1)
  SIG = SIGN(1.,ZX(ICZ))-ZX(ISZ))
  H = SIG*(1.414213562*ZX(IB)-ZX(ISX))-ZX(ISZ)
  ZZ = Z-ZX(ISZ)
  Z1 = ZX(ICZ)-ZX(ISZ)
  X1 = ZX(ICX)-ZX(ISX)
  CK = (H-Z1)**2/(4.*H*X1*Z1*(H-SIG*X1-Z1))
  A = 2.*X1*Z1*ZZ*CK*Z1-ZZ
  X = ZX(ISX)+(A-SIG*SQR((2.*A-Z1*ZZ)*(Z1-ZZ)))/(2.*Z1*Z1*CK)
  RETURN
END

```

00001640
00001650
00001660
00001670
00001680
00001690
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00001740

```

SUBROUTINE SIGMA2(N,IND,X,Y,SUM)
DIMENSION X(1),Y(1),SUM(1)
IS = 1
SUM(1) = 0.
DO 40 I=2,N
ISP = IS+IND
AREA = (Y(I)+Y(I-1))*(X(I)-X(I-1))/2.0
SUM(ISP) = SUM(IS)+AREA
IS = ISP
RETURN
END

```

40

```

C*****VOLUME CALCULATION PROCEDURE (PHASE II CONTRACT)
COMMON/ALLQ/C(8,16),NCQ,A(100,3,4)
COMMON /ONE/X1
DIMENSION ZX(25),P(25),Q(25),R(25),S(25),T(25),SG(25),ZXP(25)
DIMENSION NO(14),AAA(500),YYY(500)
DATA NO/3,20,2,8,3,40,40,3,8,25,5,25,3,3,3/
IPRINT=0
NY=1
DELTAY=0.
REWIND 3
REWIND 2
READ(3,500) NCQ
DO 5 J=1,NCQ
  READ(3,201) IC,(C(I,J),I=1,2)
  READ(3,201) IC,(C(I,J),I=3,8)
5 CONTINUE
500 FORMAT(14I5)
  YMAXL=-100.
  YMAX=-100.
10 WRITE(6,600)
600 FORMAT(' INPUT Y1,Y2,NY,BTMBLN')
  READ(5,*) Y1,Y2,NY,SSS
  XNY=NY-1
  DELTAY=(Y2-Y1)/XNY
  DO 50 LL=1,NY
    XLL=LL-1
    Y=Y1+DELTAY*XLL
    DO 2 I=1,50
      IF((Y.LE.YMAX).AND.(Y.GE.YMAXL)) GO TO 3
      IF(Y.LT.YMAXL) REWIND 2
      YMAXL=YMAX
    READ(2,200) YMAX,N,MOD,RATIO
    IF(MOD.NE.0) MOOD=MOD
    DO 2 K=1,N
      READ(2,201) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
2 CONTINUE
      C**** MOOD=1 FUSELAGE ONLY
      C**** MOOD=2 FUSELAGE WITH CANOPY
      C**** MOOD=3 FUSELAGE WITH WING
      C**** MOOD=4 FUSELAGE WITH WING & CANOPY
3 IF(MOOD.EQ.1) M=7
  IF(MOOD.EQ.2) M=13
  IF(MOOD.GT.2) M=21
00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
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00000180
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00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000290
00000300
00000310
00000320
00000330
00000340
00000350
00000360
00000370
00000380
00000390
00000400
00000410
00000420
00000430

```



```

200 FORMAT(F10.5,2I5,F10.5)
201 FORMAT(I2,5E15.8,F2.0)
DO 4 I=1,M
  IF((MOOD.EQ.3).AND.(I.GT.7).AND.(I.LT.14)) GO TO 4
  IF((RATIO.GT.0.).AND.((I.EQ.19).OR.(I.EQ.20))) GO TO 4
  CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),ZXP(I))
4 CONTINUE
  IF(MOOD.LT.3)GO TO 6
  IF(RATIO.GT.0.) CALL XSUBG(ZX,ZXP,RATIO)
  CALL CONPIC(C,NCQ,Y,ZX(22),ZXP(22),INQ)
  ZX(23)=ZX(15)-SSS
  ZXP(23)=ZXP(15)
6 CONTINUE
  IF(MOOD.GT.2) M=23
  CALL AREAC(Y,ZX,ZXP,MOOD,NO,AAA(LL))
  YYY(LL)=Y
50 CONTINUE
  CALL SIGMA2(NY,0,YYY,AAA,AREAT)
  WRITE(6,601) AREAT
601 FORMAT(' VOLUME=',G15.7)
502 FORMAT(F20.0)
700 FORMAT(8G15.7)
701 FORMAT('Y,MOOD/ZX,.....',2G15.7)
  GO TO 10
END

```

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00000680

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00000690
 00000700
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 00000770

```

SUBROUTINE CONICF(P,Q,R,S,T,SG,X,Y,YP)
  ROOT=SG*SQRT((R*X+S)*X+T)
  Y=P*X+Q+ROOT
  IF((SG.NE.0.).AND.(ROOT.NE.0.)) GO TO 10
  YP=P
  GO TO 20
10 YP=P+(R*X+S/2.0)/ROOT
20 RETURN
  END
  
```

00000780
00000790
00000800
00000810
00000820
00000830
00000840

```

FUNCTION XELIPS(Z1,Z2,X,Z)
C=1.0-((Z-Z1)/(Z2-Z1))**2
IF (C.LT.0.) C=0.
XELIPS=X*SQRT(C)
XELIPS=ABS(XELIPS)
RETURN
END

```

00000850
00000860
00000870
00000880

FUNCTION XELIPP(Z1,Z2,X1,X,Z)
XELIPP=-X1/(Z-Z1)*((Z2-Z1)/X)**2
RETURN
END

00000890
 00000900
 00000910
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```

FUNCTION PELIPS(X1,Z1,X2,Z2,Z2P,X)
S=SIGN(1.0,Z2-Z1)
C=X1-X2
DZ=Z2-Z1
A=C*(C+DZ/Z2P)/(2.*C+DZ/Z2P)
B2=DZ*DZ-(A-C)*DZ*Z2P
X0=X1-A
U=(X-X0)/A
ROOT=B2*(1.0-((X-X0)/A)**2)
IF (ROOT.LT.0.) ROOT=0.
PELIPS=S*SQRT(ROOT)*Z1
RETURN
END
  
```

```

SUBROUTINE AREAC(Y,ZX,ZXP,MOOD,N0,AA)
COMMON/MESH/K1,K2,K3,K4,K5,K6,K7,K8,AL(4)
COMMON/OK/X0U,Z0U,X0L,Z0L,R0U,R0L,SU,SL
COMMON /ONE/X1
DIMENSION XP(200),ZP(200),N0(1),ZX(1),ZXP(1)
IF(MOOD.LT.3) GO TO 10
CALL PCRCL(ZX,ZXP,-2.,Y,Z,14,16,19,1,4,2,5,22,0,0,0,0,D,
& X2U,Z2U,X0U,Z0U)
X1U=X1
CALL PCRCL(ZX,ZXP,-2.,Y,Z,15,17,20,3,6,7,5,23,0,0,0,0,D,
& X2L,Z2L,X0L,Z0L)
X1L=X1
R0U=SQRT((Z2U-Z0U)**2+(X2U-X0U)**2)
R0L=SQRT((Z2L-Z0L)**2+(X2L-X0L)**2)
SU=0
SL=0
IF(ZX(5).NE.ZX(20)) SU=(ZX(16)-ZX(14))/(ZX(19)-ZX(5))
IF(ZX(19).NE.ZX(5)) SL=(ZX(17)-ZX(15))/(ZX(20)-ZX(5))
10 L=0
IF(ZX(6).EQ.0.) GO TO 20
CALL STEP(L,0,ZX(6),N0,1,1,XP,ZP,ZX)
20 IF(MOOD.GT.2) Z2=AMIN1(ZX(7),ZX(23))
IF(MOOD.LT.3) Z2=ZX(7)
III=0
IF(ZX(6).EQ.0.) III=1
CALL STEP(L,ZX(3),Z2,N0,2,III,ZP,XP,ZX)
IF(MOOD.GT.2) GO TO 30
IF(ZX(2).LE.ZX(7)) GO TO 70
CALL STEP(L,ZX(7),ZX(2),N0,3,0,ZP,XP,ZX)
GO TO 70
30 IF(ZX(23).LE.ZX(7)) GO TO 35
CALL STEP(L,ZX(7),ZX(23),N0,3,0,ZP,XP,ZX)
35 CALL STEP(L,X1L,X2L,N0,4,0,XP,ZP,ZX)
IF(ZX(20).LE.X2L) GO TO 40
CALL STEP(L,X2L,ZX(20),N0,5,0,XP,ZP,ZX)
40 CALL STEP(L,ZX(20),ZX(21),N0,6,0,XP,ZP,ZX)
CALL STEP(L,ZX(21),ZX(19),N0,7,0,XP,ZP,ZX)
IF(ZX(19).LE.X2U) GO TO 50
CALL STEP(L,ZX(19),X2U,N0,8,0,XP,ZP,ZX)
50 CALL STEP(L,X2U,X1U,N0,9,0,XP,ZP,ZX)
IF(ZX(22).GE.ZX(2)) GO TO 60
CALL STEP(L,ZX(22),ZX(2),N0,3,0,ZP,XP,ZX)
60 IF(MOOD.GT.2) Z1=AMAX1(ZX(2),ZX(22))

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```

70 IF (MOOD.LT.3) Z1=ZX(2)
   IF ((MOOD.EQ.2).OR.(MOOD.EQ.4)) Z2=ZX(9)
   IF ((MOOD.EQ.1).OR.(MOOD.EQ.3)) Z2=ZX(1)
   CALL STEP(L,Z1,Z2,NO,10,0,ZP,XP,ZX)
   IF ((ZX(4).EQ.0.).OR.((MOOD.EQ.2).OR.(MOOD.EQ.4))) GO TO 80
   CALL STEP(L,ZX(4),0.,NO,14,0,XP,ZP,ZX)
   GO TO 90
80 IF ((MOOD.EQ.1).OR.(MOOD.EQ.3)) GO TO 90
   CALL STEP(L,ZX(9),ZX(8),NO,11,0,ZP,XP,ZX)
   CALL STEP(L,ZX(8),ZX(10),NO,12,0,ZP,XP,ZX)
   IF (ZX(13).EQ.0) GO TO 90
   CALL STEP(L,ZX(13),0.,NO,13,0,XP,ZP,ZX)
90 IF (MOOD.GT.2) ZM=ZX(18)
   IF (MOOD.LT.3) ZM=ZX(2)
   XMAX=XP(1)
   IC=1
   DO 100 I=2,L
   IF (XMAX.GT.XP(I)) GO TO 100
   XMAX=XP(I)
   IC=I
100 CONTINUE
   DO 120 I=1,IC
120 ZP(I)=ZM-ZP(I)
   DO 130 I=IC,L
130 ZP(I)=ZP(I)-ZM
   ZP(IC)=0.
   CALL SIGMA2(IC,0,XP,ZP,A1)
   N2=L-IC+1
   CALL SIGMA2(N2,0,XP(IC),ZP(IC),A2)
   AA=A1-A2
   RETURN
   END

```

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```

SUBROUTINE STEP(L,X1,X2,N0,IN,I0,XP,YP,ZX)
COMMON /OK/X0U,Z0U,X0L,Z0L,R0U,R0L,SU,SL
COMMON /ONE/X11
DIMENSION XP(1),YP(1),ZX(1),NO(1)
N=NO(IN)+I0
XN=N-I0
DX=(X2-X1)/XN
DO 100 I=1,N
  L=L+1
  XI=I-I0
  XP(L)=X1+DX*XI
  GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14),IN
1 YP(L)=ZX(3)
  GO TO 100
2 YP(L)=XELIPS(ZX(7),ZX(3),ZX(5)-ZX(6),XP(L))+ZX(6)
  GO TO 100
3 YP(L)=ZX(5)
  GO TO 100
4 ROOT=R0L**2-(XP(L)-X0L)**2
  IF (ROOT.LE.0.) ROOT=0.
  YP(L)=Z0L+SQRT(ROOT)
  GO TO 100
5 YP(L)=SL*(XP(L)-ZX(5))+ZX(15)
  GO TO 100
6 YP(L)=PELIPS(ZX(21),ZX(18),ZX(20),ZX(17),SL,XP(L))
  GO TO 100
7 YP(L)=PELIPS(ZX(21),ZX(18),ZX(19),ZX(16),SU,XP(L))
  GO TO 100
8 YP(L)=SU*(XP(L)-ZX(19))+ZX(16)
  GO TO 100
9 ROOT=R0U**2-(XP(L)-X0U)**2
  IF (ROOT.LE.0.) ROOT=0.
  YP(L)=Z0U-SQRT(ROOT)
  GO TO 100
10 YP(L)=XELIPS(ZX(2),ZX(1),ZX(5)-ZX(4),XP(L))+ZX(4)
  GO TO 100
11 QX1=XELIPS(ZX(11),ZX(10),ZX(12)-ZX(13),ZX(8))+ZX(13)
  QX2=XELIPS(ZX(2),ZX(1),ZX(5)-ZX(4),ZX(9))+ZX(4)
  Z1P=XELIPP(ZX(11),ZX(10),QX1,ZX(12)-ZX(13),ZX(8))
  Z2P=XELIPP(ZX(2),ZX(1),QX2,ZX(5)-ZX(4),ZX(9))
  DZ1=XP(L)-ZX(8)
  DZ2=ZX(9)-ZX(8)
  A=3.*DZ21-(Z2P+2.*Z1P)*(QX2-QX1)

```



```

      B=-2.*DZ21*(Z2P+Z1P)*(QX2-QX1)
      IF((Z1P.LT.-4.).OR.(Z2P.LT.-4.).OR.(Z1P.GE.0.)) GO TO 22
      GO TO 18
22  TX=1
      IF(XP(L).EQ.ZX(8)) YP(L)=QX1
      IF(XP(L).EQ.ZX(9)) YP(L)=QX2
      IF((XP(L).EQ.ZX(8)).OR.(XP(L).EQ.ZX(9))) GO TO 100
      XI=QX1
      DO 19 KKK=1,2
      DO 17 J=1,6
      DXR=(XI-QX1)/(QX2-QX1)
      ZI=ZX(8)+Z1P*(XI-QX1)+A*DXR**2+B*DXR**3
      Z1P=Z1P+(2.0*A*DXR+3.0*B*DXR**2)/(QX2-QX1)
      IF(ZIP.NE.0.) GO TO 16
      YP(L)=XI+(QX2-QX1)/100.
      GO TO 17
16  YP(L)=XI-(ZI-XP(L))/ZIP
      IF(ABS(YP(L)-XI).LE.1.E-5) GO TO 100
17  XI=YP(L)
      XI=QX2
19  CONTINUE
      GO TO 100
18  QX21=QX2-QX1
      QX1P=1.0/ZIP
      QX2P=1.0/Z2P
      A=3.0*DQX21-(QX2P+2.0*QX1P)*DZ21
      B=-2.0*DQX21+(QX2P+QX1P)*DZ21
      DZR=(XP(L)-ZX(8))/DZ21
      YP(L)=QX1+QX1P*DZ1+A*DZR**2+B*DZR**3
      GO TO 100
12  YP(L)=XELIPS(ZX(11),ZX(10),ZX(12)-ZX(13)+XP(L))+ZX(13)
      GO TO 100
13  YP(L)=ZX(10)
      GO TO 100
14  YP(L)=ZX(1)
100 CONTINUE
      RETURN
      END

```

```

SUBROUTINE PCRCL(ZX,ZXP,X,Y1,Z,IZE,IZG,IXG,IZU,IXU,IZM,IXM,
6 IZ1,FX,FY,FZ,F,X2,Z2,X0,Z0)
COMMON /ONE/X1
DIMENSION ZX(1),ZXP(1)
IT=0
IF((ZX(IZ1).LT.ZX(2)).AND.(ZX(IZ1).GT.ZX(7))) IT=1
IF((Y.EQ.Y1).AND.(ITT.EQ.IT).AND.(IZEP.EQ.IZE)) GO TO 1000
Y=Y1
ITT=IT
IZEP=IZE
XM4=(ZX(IZG)-ZX(IZE))/(ZX(IXG)-ZX(IXM))
IF(IZG.EQ.16) SS=-SIGN(1.0,XM4)
IF(IZG.EQ.17) SS=SIGN(1.0,XM4)
ZUM=ZX(IZU)-ZX(IZM)
XMU=ZX(IXM)-ZX(IXU)
IF(ITT.NE.1) GO TO 10
X1=ZX(IXM)
X1Y=ZXP(IXM)
XM1=0.
XM1Y=0.
XM3P=0.
XM3PY=0.
GO TO 20
10 Z1M=ZX(IZ1)-ZX(IZM)
Z1MZUM=Z1M/ZUM
T1=SQRT(1.0-Z1MZUM**2)
X1U=X1-ZX(IXU)
X1U=X1-ZX(IXU)
T2=2.0*Z1MZUM*((ZXP(IZ1)-ZXP(IZM))/ZUM
6 -Z1M*(ZXP(IZU)-ZXP(IZM))/ZUM**2)
X1Y=-XMU**2/X1U*T2/2.0+T1*(ZXP(IXM)-ZXP(IXU))
6 +ZXP(IXU)
XMUZUM=XMU/ZUM
T1=Z1M/X1U
XM1=XMUZUM**2*T1
T2=((ZXP(IXM)-ZXP(IXU))/ZUM-XMU*(ZXP(IZU)-ZXP(IZM))
6 /ZUM**2)*T1
T3=(ZXP(IZ1)-ZXP(IZM))/X1U-Z1M*(X1Y-ZXP(IXU))/X1U**2
XM1Y=(2.0*T2+XMUZUM*T3)*XMUZUM
XM3=-1.0/XM1
XM3P=-1.0/XM3
XM3Y=XM1Y/XM1**2
XM3PY=XM3Y/XM3**2
00002560
00002570
00002580
00002590
00002600
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```

20 XM4P=-1.0/XM4
   XGE=ZX(IXG)-ZX(IXM)
   ZGE=ZX(IZG)-ZX(IZE)
   XM4Y=(ZXP(IZG)-ZXP(IZE))/XGE-(ZXP(IXG)-ZXP(IXM))*ZGE/XGE**2
   XM4PY=XM4Y/XM4**2
   DTH=(ATAN(XM3P)+SS*ATAN(XM4P))/2.0
   XM5=TAN(DTH)
   T1=(1.0/COS(DTH))**2
   T2=XM3PY/(1.0+XM3P**2)+XM4PY/(1.0+XM4P**2)
   XM5Y=T1*T2/2.0
   IF(IT.NE.1) GO TO 30
   XP=ZX(IXM)
   ZP=ZX(IZE)
   XPY=ZXP(IXM)
   ZPY=ZXP(IZE)
   GO TO 40
30 ZE1=ZX(IZE)-ZX(IZ1)
   XM34=XM3-XM4
   T1=(XM4*ZX(IXM)-XM3*X1)
   XP=(ZE1-T1)/XM34
   T2=ZXP(IZE)-ZXP(IZ1)-XM4*ZXP(IXM)-XM4Y*ZX(IXM)+XM3*X1Y+XM3Y*X1
   XPY=(XM34*T2-(ZE1-T1)*(XM3Y-XM4Y))/XM34**2
   ZP=ZX(IZE)+XM4*(XP-ZX(IXM))
   ZPY=ZXP(IZE)+XM4*(XPY-ZXP(IXM))+*(XP-ZX(IXM))*XM4Y
40 XM15=XM1-XM5
   T1=(ZP-ZX(IZ1))-(XM5*XP-XM1*X1)
   T2=ZPY-ZXP(IZ1)-XM5*XPY-XM5Y*XP+XM1*X1Y+XM1Y*X1
   X0=T1/XM15
   X0Y=(XM15*T2-T1*(XM1Y-XM5Y))/XM15**2
   Z0=ZX(IZ1)+XM1*(X0-X1)
   Z0Y=ZXP(IZ1)+XM1*(X0Y-X1Y)+XM1Y*(X0-X1)
   Z0Z1=Z0-ZX(IZ1)
   X0X1=X0-X1
   X0YX1=X0Y-X1Y
   X0X1X1=X0X1**2
   R2=Z0Z1**2+X0X1**2
   H=SQRT(R2)
1000 IF(X.LT.-1.) GO TO 2000
   HY=(Z0Z1*(Z0Y-ZXP(IZ1))+X0X1*(X0Y-X1Y))/R
   X0=X-X0
   Z0=Z-Z0
   F=R2-Z0**2-X0**2
   FX=-2.0*X0
   FY=2.0*(R*RY+X0*X0Y+Z0*Z0Y)
   FZ=-2.0*ZZ0

```

00003420
 00003430
 00003440
 00003450
 00003460
 00003470
 00003480
 00003490

GO TO 50
 2000 CONTINUE
 D=SQRT((X1-XP)**2+(ZX(IZ1)-ZP)**2)
 ANG=ATAN(XM4)
 X2=XP+D*COS(ANG)
 Z2=ZP+XM4*(X2-XP)
 50 RETURN
 END


```

SUBROUTINE CONPIC(C,NC,XP,YP,DYP,IND)
DIMENSION C(B,4)
IND=0
DO 10 I=1,NC
IF((XP,GE,C(1,I)).AND.(XP,LE,C(2,I))) GO TO 20
10 CONTINUE
IND=1
20 CALL CONICF(C(3,I),C(4,I),C(5,I),C(6,I),C(7,I),C(8,I),XP,YP,DYP)
RETURN
END

```

```

00003500
00003510
00003520
00003530
00003540
00003550
00003560
00003570
00003580
00003590

```

00003600
00003610
00003620
00003630
00003640
00003650
00003660
00003670
00003680
00003690
00003700
00003710

```

SUBROUTINE XSUBG(ZX,ZXP,R)
DIMENSION ZX(1),ZXP(1)
T1=ZX(21)-ZX(5)
T2=ZX(16)-ZX(18)
T3=ZX(14)-ZX(18)
ZX(19)=ZX(21)-T1*T2/(R*T3)
ZXP(19)=ZXP(21)-(T3*(T2*(ZXP(21)-ZXP(5))+T1*(ZXP(16)-ZXP(18)
& ))-T1*T2*(ZXP(14)-ZXP(18)))/(R*T3*T3)
ZX(20)=ZX(19)
ZXP(20)=ZXP(19)
RETURN
END

```

```

SUBROUTINE SECOND (X,Y,N,XP,YP,DYP,IT)
DIMENSION X(1),Y(1)
M = N-1
ARROW = XP-X(1)
NI = N/2+1
IF ((X(NI)-X(1))*ARROW) 2,2,5
2  IP = 2
   GO TO 20
5  DO 10 I=2,M
   IP = I
   IF ((XP-X(I))*ARROW) 20,20,10
10  CONTINUE
20  A = XP-X(IP-1)
   B = XP-X(IP)
   C = XP-X(IP+1)
   D = X(IP-1)-X(IP)
   E = X(IP-1)-X(IP+1)
   G = X(IP)-X(IP+1)
   T1 = Y(IP-1)/(D+E)
   T2 = -Y(IP)/(D*G)
   T3 = Y(IP+1)/(E*G)
   YP = T1*B*C+T2*A*C+T3*A*B
   IF (IT.GT.0) DYP=T1*(B+C)+T2*(A+C)+T3*(A+B)
RETURN
END

```

```

00003720
00003730
00003740
00003750
00003760
00003770
00003780
00003790
00003800
00003810
00003820
00003830
00003840
00003850
00003860
00003870
00003880
00003890
00003900
00003910
00003920
00003930
00003940
00003950
00003960

```

00003970
00003980
00003990
00004000
00004010
00004020
00004030
00004040
00004050
00004060
00004070

```

SUBROUTINE SIGMA2(N,IND,X,Y,SUM)
DIMENSION X(1),Y(1),SUM(1)
IS = 1
SUM(1) = 0.
DO 40 I=2,N
  ISP = IS+IND
  AREA = (Y(I)+Y(I-1))*(X(I)-X(I-1))/2.0
  SUM(ISP) = SUM(IS)+AREA
  IS = ISP
RETURN
END

```

40

SECTION V

LOGICAL STRUCTURE

1. INTERDEPENDENCE OF SUBROUTINES

The Calling-Called matrix for the program is shown in Figure 28.

2. LISTINGS

Two complete listings of the Surface Fit and Minimum Search Program are given below, following Figure 28. The first listing is for the computer program developed in Phase I using a 6 x 6 Latin Square. The second listing is for the computer program developed in Phase II using a 4 x 4 Latin Square.

| Calling \ Called | XXGEN | CROUT | SEARCH | VALUE | XFORM | SIGMA2 | CNSTN | BASEA | VOLMD | AREA | KONIC | KONICA | TABLE | READ | CONICF | LINEAR | XELIPL |
|------------------|-------|-------|--------|-------|-------|--------|-------|-------|-------|------|-------|--------|-------|------|--------|--------|--------|
| LATIN1 | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • |
| SEARCH | | | | • | | • | | | | | | | | | | | |
| CNSTN | | | | • | | • | • | | • | | | • | | | | | |
| AREA | | | | | | | | | | | • | | | | | | |
| TABLE | | | | | | | | | | | • | | | | | • | • |
| READ | | | | | | | | | | | | | | • | | | |

(a) LATIN1 Program

| Calling \ Called | XXGEN | CROUT | SEARCH | VALUE |
|------------------|-------|-------|--------|-------|
| LATIN2 | • | • | • | • |
| SEARCH | | | | • |

(b) LATIN2 Program

FIGURE 28. CALLING-CALLED MATRIX FOR SURFACE FIT AND MINIMUM SEARCH PROGRAMS

```

PROGRAM LATIN1(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE2,TAPE3) 5X500010
C=====5X500020
C**LATIN SQUARE MINIMUM VALUE SEARCH PROGRAM (5X5 - 6 VARIABLES) 1975 5X500030
C=====5X500040
COMMON /XXX/XX(36,29)
COMMON/CHECK/FS(20),ZB(8,20),CV(28),VOLB,KIND(20),NS
COMMON/CHK1/RATIO(20),ZFS(20,20),XFS(20,20),LUM,NFS(20),ISO,
& ISN,ISNP
DIMENSION Y(28),C(28),YF(28),B(28,29),SUM(28,29)
DIMENSION O(6),E(6),XMIN(6),XMAX(6),NP(6),IY(36)
DIMENSION ZZ(8),DEV(36),IJK(3,11),V(6),SYM(6),TYPE(4)
DATA TYPE/4HAREA,8H LOCAL-X,6H RADOME,6H VOLUME/
DATA FSNOS,INU,NY/50,3,32/
DATA IJK/18,2,2,19,7,7,20,2,5,21,3,7,22,2,3,23,5,7/
M=6
412 FORMAT(3F10.0,10I5)
610 FORMAT(110,16H POINTS REJECTED/110,16H POINTS ACCEPTED/
& T12,8H AVERAGE=G12.5)
611 FORMAT(19H KIND,FS,ABASE,AMIN,I5,3G12.5)
WRITE(6,410)
410 FORMAT(1H1,T20,*LATIN SQUARE MINIMUM VALUE SEARCH PROGRAM*)
READ(5,400) SYM
WRITE(6,411) SYM
411 FORMAT(* VARIABLES ARE LISTED AS. . *.6A5)
400 FORMAT(6(3X,A2))
READ(5,401) IOR,IPRINT
401 FORMAT(14I5)
IF((IOR.LT.17).OR.(IOR.GT.28)) IOR=17
WRITE(6,402) IOR
402 FORMAT(* ORDER OF FIT. . . *.I2)
403 FORMAT(8G9.2)
IORS=IOR+1
999 FORMAT(14,25F4.0)
KASE=0
NS=1
C-----
11 READ(5,401) KIND(NS)
IF(KIND(NS).EQ.4) KASE=1
IF((KIND(NS).EQ.0).OR.(KIND(NS).GT.4)) GO TO 12
IT=KIND(NS)
WRITE(6,404) KIND(NS),TYPE(IT)
404 FORMAT(13H CONSTRAINT =,I2,1H-,A8)
GO TO (201,201,202,203),IT
5X500040
5X500050
5X500060
5X500070
5X500080
5X500090
5X500100
5X500110
5X500120
5X500130
5X500140
5X500150
5X500160
5X500170
5X500180
5X500190
5X500200
5X500210
5X500220
5X500230
5X500240
5X500250
5X500260
5X500270
5X500280
5X500290
5X500300
5X500310
5X500320
5X500330
5X500340
5X500350
5X500360
5X500370
5X500380
5X500390
5X500400
5X500410
5X500420
5X500430

```

```

201 READ(5,403) FS(NS),RATIO(NS)
   IF((RATIO(NS).NE.0.).OR.(KIND(NS).EQ.1)) GO TO 21
   READ(5,401) NPFS
   READ(5,403)(ZFS(K,NS),XFS(K,NS),K=1,NPFS)
   NFS(NS)=NPFS
   WRITE(6,405)FS(NS),(K,ZFS(K,NS),XFS(K,NS),K=1,NPFS)
405 FORMAT(* INPUT CROSS SECTION TABLE,F.S.,G12.5/
   & T10,1HZ,T22,1HX/(13,2G12.5))
21 CALL READ(INU,FS(NS),ZB(1,NS))
   GO TO 35
202 READ(5,403) FS(NS),RC,RD
   CALL READ(INU,FS(NS),ZB(1,NS))
   ZB(7,NS)=RC
   ZB(8,NS)=RD
   GO TO 35
203 READ(5,412) FS1,FS2,ANY,NFSI,LOVE
   FS(NS)=FS1
   RATIO(NS)=ANY
   IF(ANY.GT.2.0) VOLB=ANY
   IF(FS1.LT.FSNOSE) LUM=1
   IF(FS1.GE.FSNOSE) LIM=2
   IF(FS1.LE.FSNOSE) FS(NS)=FSNOSE
   IF((FS2.LE.FSNOSE).OR.(NFSI.LT.2)) LUM=0
   IS0=NS
   IS1=NS+1
   ISN=IS0+NFSI
   IS2=ISN-1
   IF(ISN.NE.IS0) FS(ISN)=FS2
   ISNP=NFSI+1
   IC=NFSI-1
   NS=ISN
   IF((LUM.EQ.0).OR.(IS0.EQ.ISN)) GO TO 33
   IF(LOVE.EQ.0) GO TO 31
   READ(5,403)(FS(K),K=IS1,IS2)
   GO TO 33
31 XI=NFSI
   DY=(FS(ISN)-FS(IS0))/XI
   DO 32 K=IS1,IS2
     XI=K-IS1+1
32 FS(K)=FS(IS0)+DY*XI
33 DO 34 K=IS0,ISN
     CALL READ(INU,FS(K),ZB(1,K))
     KIND(K)=4

```

```

5X500440
5X500450
5X500460
5X500470
5X500480
5X500490
5X500500
5X500510
5X500520
5X500530
5X500540
5X500550
5X500560
5X500570
5X500580
5X500590
5X500600
5X500610
5X500620
5X500630
5X500640
5X500650
5X500660
5X500670
5X500680
5X500690
5X500700
5X500710
5X500720
5X500730
5X500740
5X500750
5X500760
5X500770
5X500780
5X500790
5X500800
5X500810
5X500820
5X500830
5X500840
5X500850
5X500860

```



```

34 CONTINUE
35 NS=NS+1
   GO TO 11
12 NS=NS-1
C-----
6 CALL XGEN(IJK,M)
  IF (IPRINT.EQ.0) GO TO 8
  WRITE(6,886)
886 FORMAT(/* ADDITIONAL TERMS ARE. . . *)
   DO 7 I=1,M
     I1=IJK(2,I)-1
     I2=IJK(3,I)-1
7 WRITE(6,887) IJK(1,I),SYM(I1),SYM(I2)
887 FORMAT(2H (*I2,3H) ,2A5)
8 KU=KASE+1
   DO 1000 KKK=1,KU
     DO 10 I=1,28
       DO 10 J=1,29
         10 SUM(I,J)=0.0
         N=0
         DO 20 JY=1,36
           READ(5,500) J,ANY,V
           500 FORMAT(I2,7F10.0)
           IF ((J.LE.25).OR. (KKK.EQ.2)) GO TO 19
           DO 15 I=2,7
             15 XX(J,I)=V(I-1)
             DO 16 I=8,11
               16 XX(J,I)=XX(J,I-5)**2
               DO 17 I=12,14
                 17 XX(J,I)=XX(J,3)*XX(J,I-8)
                 DO 18 I=15,16
                   18 XX(J,I)=XX(J,4)*XX(J,I-10)
                   XX(J,17)=XX(J,5)*XX(J,6)
                   DO 1 I=1,M
                     10=IJK(1,I)
                     11=IJK(2,I)
                     12=IJK(3,I)
                     1 XX(J,I0)=XX(J,I1)*XX(J,I2)
                     19 IF (J.EQ.0) GO TO 25
                     N=N+1
                     XX(J,I0KS)=ANY
                     IY(N)=J
                     DO 20 K=1,10R

```

```

5X500870
5X500880
5X500890
5X500900
5X500910
5X500920
5X500930
5X500940
5X500950
5X500960
5X500970
5X500980
5X500990
5X501000
5X501010
5X501020
5X501030
5X501040
5X501050
5X501060
5X501070
5X501080
5X501090
5X501100
5X501110
5X501120
5X501130
5X501140
5X501150
5X501160
5X501170
5X501180
5X501190
5X501200
5X501210
5X501220
5X501230
5X501240
5X501250
5X501260
5X501270
5X501280
5X501290

```

```

00 20 L=1,IORS
20 SUM(K,L)=SUM(K,L)+XX(J,K)*XX(J,L)
25 IF(N,LT,IOR) GO TO 60
WRITE(6,607)
IF(KKK.EQ.1) WRITE(6,801)
IF(KKK.EQ.2) WRITE(6,802)
801 FORMAT(1H+,T17,11H*WAVE DRAG*)
802 FORMAT(1H+,T17,8H*VOLUME*)
607 FORMAT(15H0INPUT DATA....)
DO 55 I=1,N
NN=IY(I)
IF(IPRINT.GT.0) WRITE(6,609) NN,XX(NN,IORS)
55 CONTINUE
609 FORMAT(110,G15.7)
602 FORMAT(10G12.4)
IF(KKK.EQ.1) CALL CROUT(SUM,B,C,IOR)
IF(KKK.EQ.2) CALL CROUT(SUM,B,CV,IOR)
IF(IPRINT.GT.0).AND.(KKK.EQ.1))WRITE(6,803)
803 FORMAT(120,*COEFFICIENTS OF WAVE DRAG EQUATION*)
IF(IPRINT.GT.0).AND.(KKK.EQ.1)) WRITE(6,601) (I,C(I),I=1,IOR)
IF(IPRINT.GT.0).AND.(KKK.EQ.2)) WRITE(6,601) (I,CV(I),I=1,IOR)
DO 30 J=1,N
30 YF(J)=0.0
DO 40 I=1,N
DO 40 K=1,IOR
IF(KKK.EQ.1) YF(I)=YF(I)+XX(I,K)*C(K)
IF(KKK.EQ.2) YF(I)=YF(I)+XX(I,K)*CV(K)
40 CONTINUE
C-----15X501580
SUMS=0.
SUMSUM=0.
DO 45 K=1,N
NN=IY(K)
DEV(NN)=YF(NN)-XX(NN,IORS)
SUMSUM=SUMSUM+XX(NN,IORS)
45 SUMS=SUMS+(DEV(NN))**2
XNY=N
STD=SQRT(SUMS/XNY)
AVG=SUMSUM/XNY
IF(IPRINT.EQ.0) GO TO 1000
WRITE(6,699) STD
699 FORMAT(9H STD DEV=G12.5)
IF(IPRINT.GT.0).AND.(KKK.EQ.1)) WRITE(6,804)

```

```

804 FORMAT(T20,*FITTED WAVE DRAG*)
   WRITE(6,601) (I,YF(I),I=1,N)
   WRITE(6,710)
   WRITE(6,805)
805 FORMAT(T20,*ERROR OF FIT*)
   WRITE(6,601)(I,DEV(I),I=1,N)
1000 CONTINUE
C-----L
   IF((KASE.EQ.1).AND.(RATIO(ISO).LE.2.0)) VOLB=XX(26,IORS)
601 FORMAT(5(1X,1H(,12,1H),G15.7,1X))
50 WRITE(6,603)
603 FORMAT(* INPUT NO. OF PTS.*)
604 FORMAT(* INPUT LOWER LIMITS*)
   READ(5,401) NP
   IF(EOF(5)) 1122,59
59 WRITE(6,401) NP
   WRITE(6,604)
   READ(5,403) O
   WRITE(6,403) O
   WRITE(6,605)
605 FORMAT(* INPUT UPPER LIMITS*)
   READ(5,403) E
   WRITE(6,403) E
C-----)XJK,MSX501970
   CALL SEARCH(O,E,NP,C,IC,NO,YSUM,XMIN,XMAX,YMIN,YMAX,YAVG,IOR,IJK,MSX501970
& )
C-----)X501990
711 FORMAT(/T7,2HCD,T22,6(A2,13X))
   WRITE(6,610) NO,IC,YAVG
   WRITE(6,806)
806 FORMAT(1H0,T10,*MINIMUM DRAG CONFIGURATION*)
   WRITE(6,711) SYM
   WRITE(6,606) YMIN,XMIN
   IF(NS.EQ.0) GO TO 50
   DO 76 K=1,NS
   CALL XFORM(XMIN,ZZB(1,K),ZZ)
   CALL BASEA(XX1,IX2,IX3,IX4,IX5,ABASE,K,VMIN)
   CALL AREA(ZZ,AMIND,XMIN)
   WRITE(6,710)
710 FORMAT(1H )
   WRITE(6,611) KIND(K),FS(K),ABASE,AMIND
76 CONTINUE
77 IF(KASE.NE.1) GO TO 50

```

5X502170
 5X502180
 5X502190
 5X502200
 5X502210
 5X502215
 5X502220
 5X502230
 5X502240
 5X502250
 5X502260
 5X502270

```

CALL CNSTN(XMIN,INDEX,IOR,IJK,M,XX1,IX2,XX3)
CALL VOLMD(XX1,IX2,IX3,IX4,IX5,XX6,IX7,VMIN)
VNOSE=VALUE(XMIN,CV,IOR,IJK,M)
WRITE(6,710)
WRITE(6,620) VOLB,VMIN,VNOSE
620 FORMAT(*OVOLUME - BASELINE,MIN. CONF.,NOSE...,3G15.7)
GO TO 50
60 WRITE(6,608) N
608 FORMAT(* INSUFFICIENT NO. OF INPUT DATA/* N=*,I2)
606 FORMAT(8G15.7)
1122 STOP
      END

```



```

C*****XXGEN5X502280
SUBROUTINE XXGEN(IJK,M)
COMMON /XXX/XX(36,29)
DIMENSION JS(5),XB(5,5),XL(28),IJK(3,11)
EQUIVALENCE (XB(1,1),XX(1,2))
EQUIVALENCE (XB(1,1),XL(1,1))
DATA JS/3,4,0,1,2/
DO 5 I=1,36
5 XX(I,1)=1.0
DO 10 J=1,5
DO 10 I=1,5
XI=I-1
XB(I,J)=-2.0XI
10 CONTINUE
DO 20 J=1,5
I1=1+(J-1)*5
I2=I1+4
DO 20 I=I1,I2
XX(I,J)=XB(J,1)
20 CONTINUE
DO 30 J=1,5
I1=1+(J-1)*5
I2=I1+4
JUMP=JS(J)
DO 30 K=3,6
XK=K-2
L1=JUMP+XK
IC=0
DO 30 I=I1,I2
IC=IC+1
XX(I,K)=XL(L1+IC)
30 CONTINUE
DO 50 K=8,11
DO 50 I=1,25
XX(I,K)=XX(I,K-5)**2
50 CONTINUE
DO 60 K=12,14
DO 60 I=1,25
60 XX(I,K)=XX(I,3)*XX(I,K-8)
DO 70 K=15,16
DO 70 I=1,25
70 XX(I,K)=XX(I,4)*XX(I,K-10)
DO 80 I=1,25

```

5X502710
5X502720
5X502730
5X502740
5X502750
5X502760
5X502770
5X502780
5X502790
5X502800
5X502810

```

      80 XX(I,17)=XX(I,5)*XX(I,6)
      IF(M.EQ.0) RETURN
      DO 40 I=1,25
      DO 40 J=1,M
      I0=IJK(1,J)
      I1=IJK(2,J)
      I2=IJK(3,J)
      XX(I,I0)=XX(I,I1)*XX(I,I2)
      40 CONTINUE
      RETURN
      END

```

```
C*****CROUT(A,AUX,B,N)
SUBROUTINE CROUT(A,AUX,B,N)
DIMENSION A(28,29),AUX(28,29),B(1)
A IS GIVEN MATRIX, AUX IS AUXILARY MATRIX, B IS SOLUTION VECTOR
NN = N+1
DO 1 J=1,N
DO 1 K=1,NN
AUX(J,K) = A(J,K)
DO 2 J=2,NN
AUX(1,J) = A(1,J)/AUX(1,1)
DO 5 J=2,N
K = J-1
DO 5 JJ=J,N
JJ1 = JJ+1
DO 4 L=1,K
AUX(JJ,J) = AUX(L,J)*AUX(JJ,L)
AUX(J,JJ1) = AUX(J,JJ1) - AUX(L,JJ1)*AUX(J,L)
AUX(J,JJ1) = AUX(J,JJ1)/AUX(J,J)
DO 6 J=1,N
B(J) = AUX(J,NN)
DO 7 J=2,N
K = NN-J
M = J-1
DO 7 L=1,M
NNL = NN-L
B(K) = B(K) - AUX(K,NNL)*B(NNL)
RETURN
END
```

```

C*****SEARCH*****SEARCH*****SEARCH*****SEARCH*****SEARCH*****
SUBROUTINE SEARCH(O,E,NP,C,IC,NO,SUM,XMIN,XMAX,YMIN,YMAX,YAVG,IOR,
& IJK,M)
  DIMENSION O(6),E(6),NP(6),D(6),X(6),C(1),XMAX(6),XMIN(6),IJK(3,11),
DO 10 I=1,6
  IF((NP(I).LE.0))NP(I)=1
  XN=NP(I)-1
  D(I)=0.
  IF(XN.NE.0.) D(I)=(E(I)-O(I))/XN
10 CONTINUE
  SUM=0.
  NO=0
  IC=0
  YMAX=-1.0E50
  YMIN=1.0E50
  N1=NP(1)
  DO 1000 I1=1,N1
    X11=I1-1
    X(1)=O(1)+X11*D(1)
    N2=NP(2)
    DO 1000 I2=1,N2
      X12=I2-1
      X(2)=O(2)+X12*D(2)
      N3=NP(3)
      DO 1000 I3=1,N3
        X13=I3-1
        X(3)=O(3)+X13*D(3)
        N4=NP(4)
        DO 1000 I4=1,N4
          X14=I4-1
          X(4)=O(4)+X14*D(4)
          N5=NP(5)
          DO 1000 I5=1,N5
            X15=I5-1
            X(5)=O(5)+X15*D(5)
            N6=NP(6)
            DO 1000 I6=1,N6
              X16=I6-1
              X(6)=O(6)+X16*D(6)
            CALL CNSTN(X,INDEX,IOR,IJK,M,XX1,IX2,XX3)
            IF (INDEX.EQ.0) GO TO 50
            NO=NO+1
            GO TO 1000
          
```


5X503530
5X503540
5X503550
5X503560
5X503570
5X503580
5X503590
5X503600
5X503610
5X503620
5X503630
5X503640
5X503650
5X503660
5X503670
5X503680

```

50  Y=VALUE(X,C,IOR,IJK,M)
   IC=IC+1
   SUM=SUM+Y
   IF (Y.LT.YMAX) GO TO 200
   DO 100 I=1,6
     100 XMAX(I)=X(I)
     YMAX=Y
   200 IF (Y.GT.YMIN) GO TO 1000
     DO 300 I=1,6
       300 XMIN(I)=X(I)
       YMIN=Y
   1000 CONTINUE
      XIC=IC
      YAVG=SUM/XIC
      RETURN
      END

```

```

C*****
FUNCTION VALUE(X,C,IOR,IJK,M)
DIMENSION X(1),C(1),Y(36),IJK(3,11)
VALUE=C(1)
DO 10 I=2,7
  10 Y(I)=X(I-1)
DO 20 I=8,11
  20 Y(I)=X(I-6)**2
DO 30 I=12,14
  30 Y(I)=X(2)*X(I-9)
DO 40 I=15,16
  40 Y(I)=X(3)*X(I-11)
  Y(17)=X(4)*X(5)
  IF(M.EQ.0) GO TO 60
DO 50 I=1,M
  50 Y(I0)=Y(I1)*Y(I2)
  60 DO 70 I=2,IOR
  70 VALUE=VALUE+C(I)*Y(I)
RETURN
END

```

```

*****VALUE5X503690
5X503700
5X503710
5X503720
5X503730
5X503740
5X503750
5X503760
5X503770
5X503780
5X503790
5X503800
5X503810
5X503820
5X503830
5X503840
5X503850
5X503860
5X503870
5X503880
5X503890
5X503900
5X503910

```

```

C*****XFORM5X503920
SUBROUTINE XFORM(X,ZZH,ZZ)
  DIMENSION X(6),ZZB(8),ZZ(6)
  DATA COS45/.707106781/
  ZZ(1)=(.0625*(X(6)+2.)+.9)*ZZB(1)
  ZZ(2)=(.15*(X(5)+2.)+.6)*ZZB(2)
  ZZ(3)=(.375*(X(3)+2.)*ZZB(3)
  ZZ(4)=-3.75*(X(4)+2.)+5.0*ZZB(4)
  C1M=ZZB(2)-ZZB(1)
  C1L=ZZB(4)-ZZB(3)
  C2B=(ZZB(4)-ZZB(1))*COS45
  C1B=AMIN1(C1M,C1L)*COS45
  DC21B=C2B-C1B
  XBB=(-ZZB(5)-C1B)/DC21B
  C1M=ZZ(2)-ZZ(1)
  C1L=ZZ(4)-ZZ(3)
  C2=(ZZ(4)-ZZ(1))*COS45
  C1=AMIN1(C1M,C1L)*COS45
  DC21=C2-C1
  REF=C1+DC21*XRR
  IF(X(2).EQ.0.) ZZ(5)=REF
  IF(X(2).LT.0.) ZZ(5)=REF+(REF-C1)/3.*X(2)
  IF(X(2).GT.0.) ZZ(5)=REF+(C2-REF)/3.*X(2)
  ZZ(5)=-ZZ(5)
  ZZ(6)=ZZB(6)
  ZZ(7)=ZZB(7)
  ZZ(8)=ZZB(8)
  RETURN
END
5X503930
5X503940
5X503950
5X503960
5X503970
5X503980
5X503990
5X504000
5X504010
5X504020
5X504030
5X504040
5X504050
5X504060
5X504070
5X504080
5X504090
5X504100
5X504110
5X504120
5X504130
5X504140
5X504150
5X504160
5X504170
5X504180
5X504190
5X504200

```

```

C*****
SUBROUTINE SIGMA2(N,IND,X,Y,SUM)
DIMENSION X(1),Y(1),SUM(1)
IS = 1
SUM(1) = 0.
DO 40 I=2,N
  IF (I-N) 20,10,10
10  X1=X(I-1)
   X2=X(I)
   GO TO 30
20  X1=X(I-1)
   X2=X(I)
   X3=X(I+1)
   D=X1-X2
   E=X1-X3
   G=X2-X3
   T1=Y(I-1)/(D*E)
   T2=-Y(I)/(D*G)
   T3=Y(I+1)/(E*G)
   A=(T1+T2+T3)/3.0
   B=-(T1*(X2+X3)+T2*(X1+X3)+T3*(X1+X2))/2.0
   C=T1*X2*X3+T2*X1*X3+T3*X1*X2
30  ISP=IS+IND
   AREA=((A*X2)+B)*X2+C)*X2-(((A*X1)+B)*X1+C)*X1
   SUM(ISP) = SUM(IS)+AREA
40  IS = ISP
   RETURN
END

```

```

*****SIGMA2
5X504210
5X504220
5X504230
5X504240
5X504250
5X504260
5X504270
5X504280
5X504290
5X504300
5X504310
5X504320
5X504330
5X504340
5X504350
5X504360
5X504370
5X504380
5X504390
5X504400
5X504410
5X504420
5X504430
5X504440
5X504450
5X504460
5X504470
5X504480

```



```

C*****CNSIN5X504490
SUBROUTINE CNSTN(X,INDEX,IOR,IJK,M,ARASE,K,VMIN)
COMMON/CHECK/FS(20),ZB(8,20),CV(28),VOLB,KIND(20),NS
COMMON/CHK1/RATIO(20),ZFS(20,20),XFS(20,20),LUM,NFS(20),
& ISO,ISN,ISNP
DIMENSION X(6),ZZ(8),AB(20),AA(20),LIGHT(20),IJK(3,11)
DATA NP,LIGHT/20,20*0/
INDEX=0
IF(NS.EQ.0) GO TO 2000
DO 100 I=1,NS
CALL XFORM(X,ZB(1,I),ZZ)
IT=KIND(I)
GO TO (10,20,20,30),IT
C***AREA CONSTRAINT
10 IF(LIGHT(I).EQ.1) GO TO 15
CALL AREA(ZB(1,I),AB(I),X)
IF(RATIO(I).LE.2.0) AB(I)=AB(I)*RATIO(I)
IF(RATIO(I).GT.2.0) AB(I)=RATIO(I)
15 CALL AREA(ZZ,A,X)
IF(A-AB(I)) 1000,100,100
C***LOCAL FUSELAGE WIDTH OR CIRCULAR RADOM
20 CALL TABLE(ZB(1,I),ZZ,NP,INDEX,X,KIND(I),ZFS(1,I),XFS(1,I),
* NFS(I))
IF(INDEX.EQ.1) GO TO 2000
C***VOLUME CONSTRAINT
30 IF((I.NE.ISO).OR.(LUM.GT.2)) GO TO 40
VOLUME=VALUE(X,CV,IOR,IJK,M)
40 IF(LUM.LT.1) GO TO 60
CALL AREA(ZZ,AA(I),X)
IF(LIGHT(I).EQ.0) CALL AREA(ZB(1,I),AB(I),X)
50 IF(I.NE.ISN) GO TO 100
CALL SIGMA2(ISNP,0,FS(IS0),AA(IS0),VOLADD)
VOLUME=VOLUME+VOLADD
IF(LIGHT(I).EQ.1) GO TO 60
LIGHT(I)=1
CALL SIGMA2(ISNP,0,FS(IS0),AB(IS0),VOLADD)
VOLB=VOLB+VOLADD
IF(RATIO(IS0).LE.2.0) VOLB=VOLB*RATIO(IS0)
60 IF(VOLUME-VOLB) 1000,100,100
100 CONTINUE
GO TO 2000
1000 INDEX=1
2000 RETURN

```

```

C-----BASEA5X504940
  ENTRY BASEA
  ABASE=AB(K)
  RETURN
C-----VOLMD5X504980
  ENTRY VOLMD
  VMIN=VOLUME
  RETURN
  END
5X504950
5X504960
5X504970
5X504990
5X505000
5X505010
5X505020

```

```

C*****
SUBROUTINE AREA(ZZ,A,X)
  DIMENSION ZZ(1),X(1)
  DATA PI/3.14159265358979/
  X1=ZZ(1)-ZZ(7)
  X2=ZZ(6)-ZZ(2)
  IF (ZZ(8).NE.0.) GO TO 10
  AE=(PI*X1/4.0+ZZ(7))*X2
  GO TO 20
10 T=(ZZ(8)-ZZ(2))/X2
   ASINT=ASIN(T)
   ROOT=SQRT(1.0-T*T)
   AE=X1*X2/2.0*(T*ROOT+ASINT)+(ZZ(8)-ZZ(2))*ZZ(7)
20 CALL KONICA(ZZ(3),ZZ(4),ZZ(1),ZZ(2),ZZ(5),X,X1,X2,AK,ZZ,X)
  A=AE+AK
  RETURN
END

```

```

*****AREA*****
5X505030
5X505040
5X505050
5X505060
5X505070
5X505080
5X505090
5X505100
5X505110
5X505120
5X505130
5X505140
5X505150
5X505160
5X505170
5X505180
5X505190

```

```

C*****KONIC5X505200
SUBROUTINE KONIC(XL,ZL,XM,ZM,B,Z,X,ARE,ZZX,XX)
DIMENSION SUM(2),ZZX(8),XX(6)
ID=1
GO TO 10
ENTRY KONICA
ID=2
10 SIG=SIGN(1.0,ZL-ZM)
H=SIG*(1.414213562*B-XM)-ZM
Z1=ZL-ZM
X1=XL-XM
CK=(H-Z1)**2/(4.*H*X1*Z1*(H-SIG*X1-Z1))
IF(ID.EQ.2) GO TO 20
ZZ=Z-ZM
A=2.*X1*Z1*7Z*CK+Z1-ZZ
X=XM*(A-SIG*SQRT((2.*A-Z1+ZZ)*(Z1-ZZ)))/(2.*Z1*Z1*CK)
RETURN
20 Z=ZL-ZM
C=4.0*X1*Z1*CK-1.
DO 30 I=1,2
Z1PCZ=Z1+C*Z
Z1MZ=Z1-Z
IF(C)24,22,22
22 ARG=(C*Z1MZ)/Z1PCZ
IF(ARG.LT.0.) GO TO 35
E=2./SQRT(C)*ATAN(SQRT(ARG))
GO TO 26
24 ARG1=C*Z1PCZ
ARG2=-Z1MZ
IF((ARG1.LT.0.).OR.(ARG2.LT.0.)) GO TO 35
E=2./SQRT(-C)*ALOG(SQRT(ARG1)-C*SQRT(ARG2))
26 ARG3=Z1PCZ*Z1MZ
IF(ARG3.LT.0.) GO TO 35
E=((C+1.)*Z1-2.*C*Z1MZ)*SQRT(ARG3)+
& (C+1.)*2*Z1*2*E/2.)/(4.*C)
SUM(1)=XM*Z*((Z1+(C-1.)*Z/4.)*Z-SIG*E)/(2.*Z1*Z1*CK)
30 Z=0.
ARE=SUM(2)-SUM(1)
GO TO 50
35 WRITE(6,600) XX
ARE=0.
600 FORMAT(* NEGATIVE SQRT ENCOUNTERED IN KONIC*/ * X=*,6G12.5)
50 CONTINUE

```


PAGE 19

5X505630
5X505640

RETURN
END

```

C*****
SUBROUTINE TABLE(ZZB,ZZ,NP,INDEX,XX,KIND,ZFS,XFS,NFS)
DIMENSION ZZB(6),ZZ(6),ZFS(1),XFS(1)
XB=0.
IF (KIND.EQ.3) GO TO 20
Z1=AMAX1(ZFS(1),ZZ(4))
Z2=AMIN1(ZFS(NFS),ZZ(6))
GO TO 30
20 Z1=AMAX1((ZZB(7)-ZZB(8)),ZZ(4))
Z2=AMIN1((ZZB(7)-ZZB(8)),ZZ(6))
30 ZNP=NP-1
DZ=(Z2-Z1)/ZNP
DO 100 I=1,NP
XI=I-1
Z=Z1+XI*DZ
IF (KIND.EQ.3) GO TO 32
XB=LINER(ZFS,XFS,NFS,Z)
32 IF (Z.GE.ZZ(2)) X=XELIPS(ZZ(2),ZZ(6),ZZ(1),Z)
34 IF (Z.LT.ZZ(2)) CALL KONIC(ZZ(3),ZZ(4),ZZ(1),ZZ(2),ZZ(5),Z,X
*,XX1,XX2,XX3)
IF (KIND.NE.3) GO TO 50
40 ROOT=ZZB(8)**2-(Z-ZZB(7))**2
IF (ROOT.LE.0.) GO TO 50
XB=SQRT(ROOT)
50 IF (X.LT.XB) GO TO 200
100 CONTINUE
GO TO 300
200 INDEX=1
300 RETURN
END

```

```

C*****XELIPS 5X506070
5X506080
5X506090
5X506100
5X506110
5X506120

FUNCTION XELIPS(Z1,Z2,X,Z)
XELIPS=X*SQRT(1.-((Z-Z1)/(Z2-Z1))**2)
XELIPS=ABS(XELIPS)
RETURN
END

```

```

C*****READ
SUBROUTINE READ(INU,Y,ZZ)
  DIMENSION ZX(13),P(13),Q(13),R(13),S(13),T(13),SG(13),ZZ(8)
  DATA YMAXL,YMAX/-100.,-100./
  DO 2 I=1,50
    IF((Y.LE.YMAX).AND.(Y.GE.YMAXL)) GO TO 3
    IF(Y.LT.YMAXL) REWIND INU
    YMAXL=YMAX
  READ(INU,200) YMAX,N
  M=7
  DO 2 K=1,N
    READ(INU,201) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
    IF(L.GT.7) M=13
  2 CONTINUE
  200 FORMAT(F10.5,I5)
  201 FORMAT(I2,5E15.8,F2.0)
  3 DO 4 I=1,7
    CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),D)
  4 CONTINUE
    IF(M.EQ.7) GO TO 6
    DO 5 I=8,13
      CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),D)
  5 CONTINUE
  6 ZZ(1)=ZX(5)
    ZZ(2)=ZX(2)
    ZZ(3)=ZX(6)
    ZZ(4)=ZX(3)
    ZZ(5)=ZX(7)
    ZZ(6)=ZX(1)
    ZZ(7)=ZX(4)
    ZZ(8)=ZX(8)
    IF(M.EQ.7) ZZ(8)=0.0
  RETURN
END

```



```

C*****CONICF*****
SUBROUTINE CONICF (P,Q,R,S,T,SG,X,Y,YP)
  ROOT=SG*SQRT ((R*X+S)*X+T)
  Y=P+X*Q*ROOT
  IF (SG.NE.0.) GO TO 10
  YP=P
  GO TO 20
10 YP=P+(R*X+S/2.0)/ROOT
20 RETURN
  END

```

SX506460
 SX506470
 SX506480
 SX506490
 SX506500
 SX506510
 SX506520
 SX506530
 SX506540
 SX506550

5X506560

```
FUNCTION LINEAR(X,Y,N,XP)
  DIMENSION X(100),Y(100)
  DO 30 I=2,N
    IP=I
    IF((XP-X(I)).LE.0.) GO TO 40
  30 CONTINUE
  40 LINEAR=Y(IP-1)+(Y(IP)-Y(IP-1))*(XP-X(IP-1))/(X(IP)-X(IP-1))
  RETURN
END
```

```

PROGRAM LATIN2(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
C=====
C**LATIN SQUARE MINIMUM VALUE SEARCH PROGRAM (3X3 - 4 VARIABLES)
C=====
COMMON /XXX/XX(36,29)
COMMON/CHECK/FS(20),ZZB(8,25),CV(28),VOLB,KIND(20),NS
COMMON/CHK1/RATIO(20),ZFS(20,20),XFS(20,20),LUM,NFS(20),ISO,
& ISN,ISNP
DIMENSION Y(28),C(28),YF(28),B(28,29),SUM(28,29)
DIMENSION O(4),E(4),XMIN(4),XMAX(4),NP(4),IY(36)
DIMENSION ZZ(8),DEV(36),IJK(3,11),V(4),SYM(4)
DATA FSNOSE,INU,XY/430.,3,32/
DATA IJK/10,3,3/
M=1
READ(5,400) (SYM(I),I=2,4),SYM(1)
400 FORMAT(4(3X,A2))
DO 1010 I=1,36
DO 1010 J=1,29
1010 XX(I,J)=0.
WRITE(6,888)
888 FORMAT(* INPUT ORDER OF FIT - 8 THRU 14*)
READ(5,401) IOR,IPRINT
WRITE(6,466) IOR,IPRINT
466 FORMAT(* IOR,IPRINT*,2I10)
401 FORMAT(14I5)
IF((IOR.LT.8).OR.(IOR.GT.14)) IOR=8
IORS=IOR+1
999 FORMAT(I4,25F4.0)
KASE=0
NS=1
ISO =1
C-----
11 READ(5,490) KINDT,VOLBIN
490 FORMAT(I5,F10.0)
VOLB=VOLBIN
IF(KINDT.NE.0) WRITE(6,722) VOLB
722 FORMAT(*0VOLUME CONSTRAINT, VOLUME*,G16.7,*GREATER THAN BASELINE*
+ )
IF(KINDT.EQ.0) WRITE(6,721)
721 FORMAT(*0NO CONSTRAINT*)
1113 IF(KINDT.EQ.0) KIND(NS)=4
IF(KINDT.NE.0) KIND(NS)=3
IF(KIND(NS).EQ.3) KASE=1
3X300010
3X300020
3X300030
3X300040
3X300050
3X300060
3X300070
3X300080
3X300090
3X300100
3X300110
3X300120
3X300130
3X300140
3X300150
3X300160
3X300170
3X300180
3X300190
3X300200
3X300210
3X300220
3X300230
3X300240
3X300250
3X300260
3X300270
3X300280
3X300290
3X300300
3X300310
3X300320
3X300330
3X300340
3X300350
3X300360
3X300370
3X300380
3X300390
3X300400
3X300410
3X300420
3X300430

```

```

412 FORMAT(3F10.0,10I5)
-----
6 CALL XXGEN(IJK,M)
  IF(IIPRINT.EQ.0) GO TO 8
  WRITE(6,886)
886 FORMAT(/* ADDITIONAL TERMS ARE. . . *)
  IF(M.EQ.0) GO TO 8
  DO 7 I=1,M
    I1=IJK(2,I)-1
    I2=IJK(3,I)-1
  7 WRITE(6,887) IJK(1,I),SYM(I1),SYM(I2)
887 FORMAT(2H (.I2,3H) ,2A2)
8 KU=KASE+1
  DO 1000 KKK=1,KU
    DO 10 I=1,28
      DO 10 J=1,29
        10 SUM(I,J)=0.0
        N=0
        DO 20 JY=1,36
          READ(5,500) J,ANY,V
          500 FORMAT(I2,7F10.0)
          IF((J.LE.9).OR.(KKK.EQ.2)) GO TO 19
          DO 15 I=2,5
            15 XX(J,I)=V(I-1)
          DO 16 I=6,7
            16 XX(J,I)=XX(J,I-2)**2
          XX(J,8)=XX(J,4)*XX(J,5)
          DO 18 I=9,10
            18 XX(J,I)=XX(J,I-7)**2
          DO 101 I=11,12
            101 XX(J,I)=XX(J,2)*XX(J,I-7)
          DO 102 I=13,14
            102 XX(J,I)=XX(J,3)*XX(J,I-9)
          IF(M.EQ.0) GO TO 19
          DO 1 I=1,M
            10=IJK(1,I)
            I1=IJK(2,I)
            I2=IJK(3,I)
            1 XX(J,I0)=XX(J,I1)*XX(J,I2)
          19 IF(J.EQ.0) GO TO 25
            N=N+1
            XX(J,IORS)=ANY
            IV(N)=J

```

```

3X300440
3X300450
3X300460
3X300470
3X300480
3X300490
3X300500
3X300510
3X300520
3X300530
3X300540
3X300550
3X300560
3X300570
3X300580
3X300590
3X300600
3X300610
3X300620
3X300630
3X300640
3X300650
3X300660
3X300670
3X300680
3X300690
3X300700
3X300710
3X300720
3X300730
3X300740
3X300750
3X300760
3X300770
3X300780
3X300790
3X300800
3X300810
3X300820
3X300830
3X300840
3X300850
3X300860

```



```

DO 20 K=1,IOR
DO 20 L=1,IORS
20 SUM(K,L)=SUM(K,L)+XX(J,K)*XX(J,L)
25 IF(IPRINT.NE.2) GO TO 26
DO 1239 JK=1,N
1239 WRITE(6,789)(XX(JK,I),I=1,14),XX(JK,IORS)
789 FORMAT(14F4.0,G13.6)
26 IF(N.LT.IOR) GO TO 60
WRITE(6,607)
IF(KKK.EQ.1) WRITE(6,801)
IF(KKK.EQ.2) WRITE(6,802)
801 FORMAT(1H+,T17,11H*WAVE DRAG*)
802 FORMAT(1H+,T17,8H*VOLUME*)
607 FORMAT(15H0INPUT DATA....)
DO 55 I=1,N
NN=IY(I)
IF(IPRINT.GT.0) WRITE(6,609) NN,XX(NN,IORS)
55 CONTINUE
609 FORMAT(1I0,G15.7)
602 FORMAT(10G12.4)
IF(KKK.EQ.1) CALL CROUT(SUM,B,C,IOR)
IF(KKK.EQ.2) CALL CROUT(SUM,B,CV,IOR)
IF(IPRINT.GT.0).AND.(KKK.EQ.1))WRITE(6,803)
803 FORMAT(T20,*COEFFICIENTS OF WAVE DRAG EQUATION*)
IF(IPRINT.GT.0).AND.(KKK.EQ.1)) WRITE(6,601)(I,C(I),I=1,IOR)
IF(IPRINT.GT.0).AND.(KKK.EQ.2)) WRITE(6,601)(I,CV(I),I=1,IOR)
DO 30 J=1,N
30 YF(J)=0.0
DO 40 I=1,N
DO 40 K=1,IOR
IF(KKK.EQ.1) YF(I)=YF(I)+XX(I,K)*C(K)
IF(KKK.EQ.2) YF(I)=YF(I)+XX(I,K)*CV(K)
40 CONTINUE
C-----1
SUMS=0.
SUMSUM=0.
DO 45 K=1,N
NN=IY(K)
DEV(NN)=YF(NN)-XX(NN,IORS)
SUMSUM=SUMSUM+XX(NN,IORS)
45 SUMS=SUMS+(DEV(NN))**2
XNY=N
STD= SQRT(SUMS/XNY)

```

```

AVG=SUMSUM/XNY
IF (IPRINT.EQ.0) GO TO 1000
WRITE(6,699) STD
699 FORMAT(9H STD DEV=,G12.5)
IF ((IPRINT.GT.0).AND.(KKK.EQ.1)) WRITE(6,804)
804 FORMAT(T20,*FITTED WAVE DRAG*)
WRITE(6,601) (I,YF(I),I=1,N)
WRITE(6,710)
WRITE(6,805)
805 FORMAT(T20,*ERROR OF FIT*)
WRITE(6,601) (I,DEV(I),I=1,N)
WRITE(6,1234)
1234 FORMAT(* ++++++*****+*****+*****+*****+*****+*)
1000 CONTINUE
C-----L
WRITE(6,1234)
601 FORMAT(5(1X,1H(I,12,1H),G15.7,1X))
50 WRITE(6,603)
603 FORMAT(* INPUT NO. OF PTS.*)
READ(5,401) (NP(I),I=2,4),NP(1)
IF (EOF(5)) 1122,59
59 WRITE(6,401) (NP(I),I=2,4),NP(1)
WRITE(6,604)
604 FORMAT(* INPUT LOWER LIMITS*)
READ(5,403) (O(I),I=2,4),O(1)
403 FORMAT(8G9.2)
WRITE(6,403) (O(I),I=2,4),O(1)
WRITE(6,605)
605 FORMAT(* INPUT UPPER LIMITS*)
READ(5,403) (E(I),I=2,4),E(1)
WRITE(6,403) (E(I),I=2,4),E(1)
C-----
CALL SEARCH(O,E,NP,C,IC,NO,YSUM,XMIN,XMAX,YMIN,YMAX,YAVG,IOR,IJK,M3X301620
& )
C-----
711 FORMAT(/T7,2HCD,T22,6(A2,13X))
WRITE(6,610) NO,IC,YAVG
610 FORMAT(110,16H POINTS REJECTED/110,16H POINTS ACCEPTED/
* T12,8HAVERAGE=,G12.5)
WRITE(6,806)
806 FORMAT(1H0,T10,*MINIMUM DRAG CONFIGURATION*)
WRITE(6,711) (SYM(I),I=2,4),SYM(1)
WRITE(6,606) YMIN,(XMIN(I),I=2,4),XMIN(1)
3X301300
3X301310
3X301320
3X301330
3X301340
3X301350
3X301360
3X301370
3X301380
3X301390
3X301400
3X301410
3X301420
3X301430
3X301440
3X301450
3X301460
3X301470
3X301480
3X301490
3X301500
3X301510
3X301520
3X301530
3X301540
3X301550
3X301560
3X301570
3X301580
3X301590
3X301600
3X301610
3X301620
3X301630
3X301640
3X301650
3X301660
3X301670
3X301680
3X301690
3X301700
3X301710
3X301720

```

3X301730
3X301740
3X301750
3X301760
3X301770
3X301780
3X301790
3X301800
3X301810
3X301820
3X301830

```

710 FORMAT(1H )
77 IF (KASE.NE.1) GO TO 50
   VMIN=VALUE(XMIN,CV,IOR,IJK,M)
   WRITE(6,710)
   WRITE(6,606) VOLB,VMIN
   GO TO 50
60 WRITE(6,608) N
608 FORMAT(* INSUFFICIENT NO. OF INPUT DATA*/* N=*,I2)
606 FORMAT(8G15.7)
1122 STOP
      END

```



```

C*****CROUT3X302230
SUBROUTINE CROUT(A,AUX,B,N)
DIMENSION A(28,29),AUX(28,29),B(1)
C A IS GIVEN MATRIX, AUX IS AUXILIARY MATRIX, B IS SOLUTION VECTOR
NN = N+1
DO 1 J=1,N
DO 1 K=1,NN
1 AUX(J,K) = A(J,K)
DO 2 J=2,NN
2 AUX(1,J) = A(1,J)/AUX(1,1)
DO 5 J=2,N
K = J-1
DO 5 JJ=J,N
JJ1 = JJ+1
DO 4 L=1,K
4 AUX(JJ,J) = AUX(JJ,J) - AUX(L,J)*AUX(JJ,L)
5 AUX(J,JJ1) = AUX(J,JJ1) - AUX(L,JJ1)*AUX(J,L)
DO 6 J=1,N
6 B(J) = AUX(J,NN)
DO 7 J=2,N
K = NN-J
M = J-1
DO 7 L=1,M
NNL = NN-L
7 B(K) = B(K) - AUX(K,NNL)*B(NNL)
RETURN
END
3X302240
3X302250
3X302260
3X302270
3X302280
3X302290
3X302300
3X302310
3X302320
3X302330
3X302340
3X302350
3X302360
3X302370
3X302380
3X302390
3X302400
3X302410
3X302420
3X302430
3X302440
3X302450
3X302460
3X302470
3X302480
3X302490
3X302500

```

```

C*****SEARCH(O,E,NP,C,IC,NO,SUM,XMIN,XMAX,YMIN,YMAX,YAVG,IOR,
& IJK,M)
SUBROUTINE SEARCH(O,E,NP,C,IC,NO,SUM,XMIN,XMAX,YMIN,YMAX,YAVG,IOR,
COMMON/CHECK/FS(20),ZB(8,25),CV(28),VOLB,KIND(20),NS
DIMENSION O(4),E(4),NP(4),D(4),X(4),C(1),XMAX(4),XMIN(4),IJK(3,11)
DO 10 I=1,4
IF((NP(I).LE.0))NP(I)=1
XN=NP(I)-1
D(I)=0.
IF(XN.NE.0.) D(I)=(E(I)-O(I))/XN
10 CONTINUE
SUM=0.
NO=0
IC=0
YMAX=-1.0E50
YMIN=1.0E50
N1=NP(1)
DO 1000 I1=1,N1
X11=I1-1
X(1)=O(1)+X11*D(1)
N2=NP(2)
DO 1000 I2=1,N2
X12=I2-1
X(2)=O(2)+X12*D(2)
N3=NP(3)
DO 1000 I3=1,N3
X13=I3-1
X(3)=O(3)+X13*D(3)
N4=NP(4)
DO 1000 I4=1,N4
X14=I4-1
X(4)=O(4)+X14*D(4)
N5=NP(5)
VOL=VALUE(X,CV,IOR,IJK,M)
IF(VOL.GE.VOLB) GO TO 50
NO=NO+1
GO TO 1000
50 Y=VALUE(X,C,IOR,IJK,M)
IC=IC+1
SUM=SUM+Y
IF(Y.LT.YMAX) GO TO 200
DO 100 I=1,4
100 XMAX(I)=X(I)

```

```

YMAX=Y
200 IF (Y.GT.YMIN) GO TO 1000
DO 300 I=1,4
300 XMIN(I)=X(I)
YMIN=Y
1000 CONTINUE
XIC=IC
YAVG=SUM/XIC
RETURN
END

```

```

3X302940
3X302950
3X302960
3X302970
3X302980
3X302990
3X303000
3X303010
3X303020
3X303030

```

```

C*****
FUNCTION VALUE(X,C,IOR,IJK,M)
DIMENSION X(1),C(1),Y(36),IJK(3,11)
VALUE=C(1)
DO 10 I=2,5
  10 Y(I)=X(I-1)
DO 20 I=6,7
  20 Y(I)=X(I-3)**2
DO 30 I=8,8
  30 Y(I)=X(3)*X(4)
DO 40 I=9,10
  40 Y(I)=X(I-8)**2
IF(M.EQ.0) GO TO 60
DO 50 I=1,M
  I0=IJK(1,I)
  I1=IJK(2,I)
  I2=IJK(3,I)
  50 Y(I0)=Y(I1)*Y(I2)
DO 60 I=2,IOR
  60 Y(I)=Y(I-1)
  70 VALUE=VALUE+C(I)*Y(I)
RETURN
END

```

```

*****VALUE
3X303040
3X303050
3X303060
3X303070
3X303080
3X303090
3X303100
3X303110
3X303120
3X303130
3X303140
3X303150
3X303160
3X303170
3X303180
3X303190
3X303200
3X303210
3X303220
3X303230
3X303240
3X303250

```



```

C**FUSELAGE VOLUME CALCULATION PROCEDURE
  DIMENSION ZX(13),P(13),Q(13),R(13),S(13),T(13),SG(13),ZXP(13)
  DIMENSION AREA(101),YS(101)
  REWIND 2
  NY=101
  M78=10
  YMAXL=-100.
  YMAX=-100.
  10 WRITE(6,600)
  600 FORMAT(' INPUT KASE,Y1,Y2')
  READ(K,501) KASE,Y1,Y2
  501 FORMAT(I5,2F10.2)
  XN=NY-1
  DELTAY=(Y2-Y1)/XN
  DO 50 LL=1,NY
    XLL=LL-1
    Y=Y1+DELTAY*XLL
    YS(LL)=Y
    DO 2 I=1,50
      IF((Y.LE.YMAX).AND.(Y.GE.YMAXL)) GO TO 3
      IF(Y.LT.YMAXL) REWIND 2
      YMAXL=YMAX
      READ(2,200) YMAX,N
      M=7
      DO 2 K=1,N
        READ(2,201) L,P(L),Q(L),R(L),S(L),T(L),SG(L)
        IF(L.GT.7) M=13
        IF((L.EQ.9).OR.(L.EQ.8)) M78=8
        2 CONTINUE
        200 FORMAT(F10.5,I5)
        201 FORMAT(I2,5E15.8,F2.0)
        3 DO 4 I=1,7
          CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),ZXP(I))
          4 CONTINUE
          IF(M.EQ.7) GO TO 6
          DO 5 I=M78,13
            5 CALL CONICF(P(I),Q(I),R(I),S(I),T(I),SG(I),Y,ZX(I),ZXP(I))
            IF(M78.EQ.10) SG(8) = 99.
            6 CALL PLOT(Y,ZX,ZXP,M,SG,AREA(LL))
            MODE=1
          50 CONTINUE
          CALL SIGMA2(NY,0,YS,AREA,VOL)
          WRITE(6,700) KASE,VOL

```

00000430
00000440
00000450
00000460
00000470

700 FORMAT('IKASE =',I5,'VOLUME =',G14.6)
HEAD(5,500) DUMMY
500 FORMAT(F20.0)
GO TO 10
END

00000480
 00000490
 00000500
 00000510
 00000520
 00000530
 00000540
 00000550
 00000560

```

SUBROUTINE CONICF(P,Q,R,S,T,SG,X,Y,YP)
  ROOT=SG*SQRT((R*X+S)*X+T)
  Y=P*X+Q+ROOT
  IF (SG.NE.0.) GO TO 10
  YP=P
  GO TO 20
10 YP=P+(R*X+S/2.0)/ROOT
20 RETURN
  END
  
```

```

SUBROUTINE PLOT(Y,ZX,ZXP,M,SG,AREA)
COMMON PRINT,NMAX
DIMENSION XP(200),ZP(200)
DIMENSION ZX(1),ZXP(1),SG(1)
N=200
XN=N-1
NM1=N-1
IF(M.EQ.7) Z1=ZX(1)
IF(M.EQ.13) Z1=ZX(10)
Z2=ZX(3)
XP(1)=0.
XP(N)=0.
ZP(1)=Z1
ZP(N)=Z2
DZ=(Z1-Z2)/XN
DO 1000 I=2,NM1
X1=I-1
Z=Z1-DZ*X1
ZP(I)=-Z
IF(M.EQ.7).OR.(SG(8).EQ.99.)) GO TO 10
IF(Z.GT.ZX(8)) GO TO 100
IF(Z.GT.ZX(9)) GO TO 200
10 IF(Z.GT.ZX(2)) GO TO 300
IF(Z.GT.ZX(3)) GO TO 400
C***LOWER FLAT
INDEX=5
X=ZX(6)
GO TO 500
C***CANOPY
100 INDEX=1
X=XELIPS(ZX(1),ZX(10),ZX(12),ZX(13),Z)+ZX(13)
GO TO 500
C***CUBIC
200 INDEX=2
IF(SG(8).NE.99.) GO TO 15
IF(Z.GE.ZX(1)) GO TO 300
GO TO 400
15 X1=XELIPS(ZX(11),ZX(10),ZX(12),ZX(13),ZX(8))+ZX(13)
X2=XELIPS(ZX(2),ZX(1),ZX(5),ZX(4),ZX(9))+ZX(4)
Z1P=XELIPP(ZX(11),ZX(10),X1,ZX(12),ZX(8))
Z2P=XELIPP(ZX(2),ZX(1),X2,ZX(5),ZX(4),ZX(9))
DZ1=Z-ZX(8)
DZ21=ZX(9)-ZX(8)

```

```

00000570
00000580
00000590
00000600
00000610
00000620
00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000900
00000910
00000920
00000930
00000940
00000950
00000960
00000970
00000980
00000990

```



```

A=3.*DZ21-(Z2P+2.*Z1P)*(X2-X1)
B=-2.*DZ21+(Z2P+Z1P)*(X2-X1)
IF((Z1P.LT.-4.).OR.(Z2P.LT.-4.).OR.(Z1P.GE.0.)) GO TO 22
GO TO 18
22 TX=1
IF(Z.EQ.ZX(8)) X=X1
IF(Z.EQ.ZX(9)) X=X2
IF((Z.EQ.ZX(8)).OR.(Z.EQ.ZX(9))) GO TO 500
XI=X1
DO 19 L=1,2
DO 17 J=1,6
DXR=(X1-X1)/(X2-X1)
ZI=ZX(8)+Z1P*(XI-X1)+A*DXR**2+B*DXR**3
Z1P=Z1P+(2.0*A*DXR+3.0*B*DXR**2)/(X2-X1)
IF(ZIP.NE.0.) GO TO 16
X=X1+(X2-X1)/100.
GO TO 17
16 X=X1-(Z1-Z)/ZIP
IF(ABS(X-XI).LE.1.E-5) GO TO 500
17 XI=X
XI=X2
19 CONTINUE
GO TO 500
18 DX21=X2-X1
X1P=1.0/Z1P
X2P=1.0/Z2P
A=3.0*DX21-(X2P+2.0*X1P)*DZ21
B=-2.0*DX21+(X2P+X1P)*DZ21
DZR=(Z-ZX(8))/DZ21
X=X1+X1P*DZ1+A*DZR**2+B*DZR**3
GO TO 500
C**UPPER ELLIPSE
300 INDEX=3
X=XELIPS(ZX(2),ZX(1),ZX(5)-ZX(4),Z) + ZX(4)
GO TO 500
C**LOWER CONIC
400 INDEX=4
CALL CONICS(ZX,ZXP,6,3,5,2,7,Z,X)
500 XP(I)=X
1000 CONTINUE
CALL SIGMA2(N,0,ZP,XP,AREA)
RETURN
END
00001000
00001010
00001020
00001030
00001040
00001050
00001060
00001070
00001080
00001090
00001100
00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210
00001220
00001230
00001240
00001250
00001260
00001270
00001280
00001290
00001300
00001310
00001320
00001330
00001340
00001350
00001360
00001370
00001380
00001390
00001400
00001410
00001420

```

00001430
00001440
00001450
00001460
00001470

FUNCTION XELIPS(Z1,Z2,X,Z)
XELIPS=X*SQRT(1.0-((Z-Z1)/(Z2-Z1))**2)
XELIPS=ABS(XELIPS)
RETURN
END

00001480
00001490
00001500
00001510

FUNCTION XELIPP(Z1,Z2,X1,X,Z)
XELIPP=-X1/(Z-Z1)*((Z2-Z1)/X)**2
RETURN
END

```

SUBROUTINE CONICS(ZX,ZXP,ICX,ICZ,ISX,ISZ,IB,Z,X)
  DIMENSION ZX(1),ZXP(1)
  SIG = SIGN(1.,ZX(ICZ))-ZX(ISZ))
  H = SIG*(1.414213562*ZX(IB)-ZX(ISX))-ZX(ISZ)
  ZZ = Z-ZX(ISZ)
  Z1 = ZX(ICZ)-ZX(ISZ)
  X1 = ZX(ICX)-ZX(ISX)
  CK = (H-Z1)**2/(4.*H*X1*Z1*(H-SIG*X1-Z1))
  A = 2.*X1*Z1*ZZ*CK*Z1-ZZ
  X = ZX(ISX)+(A-SIG*SQR((2.*A-Z1*ZZ)*(Z1-ZZ)))/(2.*Z1*Z1*CK)
  RETURN
END
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630

```


00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740

```

SUBROUTINE SIGMA2(N,IND,X,Y,SUM)
DIMENSION X(1),Y(1),SUM(1)
IS = 1
SUM(1) = 0.
DO 40 I=2,N
  ISP = IS+IND
  AREA = (Y(I)+Y(I-1))*(X(I)-X(I-1))/2.0
  SUM(ISP) = SUM(IS)+AREA
  IS = ISP
40 RETURN
END

```

SECTION VI

FUNCTIONAL DESCRIPTION OF SUBROUTINES

| | | |
|--------|---|---|
| XYGEN | - | Generates the Latin Square Coordinate Matrix. |
| CROUT | - | Uses Crout method to solve simultaneous linear equations. |
| SEARCH | - | Searches for the minimum value. |
| VALUE | - | Uses the Latin Square Surface Fit Wave Drag Coefficients. |
| XFORM | - | Transforms reduced variables to physical variables for forward fuselage. |
| SIGMA2 | - | Performs integration using the second order Lagrange formula. |
| CNSTN | - | Imposes constraints according to input parameter. |
| BASEA | - | A second entry of CNSTN to transfer the value of the baseline cross-sectional area. |
| VOLMD | - | A third entry of CNSTN to transfer the value of the fuselage volume. |
| AREA | - | Computes the cross-sectional area of fuselage excluding the canopy. |
| KONIC | - | Computes fuselage widths at given fuselage stations. |
| KONICA | - | A second entry of KNOIC to compute the cross-sectional area of the lower fuselage. |
| TABLE | - | Compares the fuselage width distribution with given local tabulation of width or with random contour. |
| READ | - | Reads baseline body description data. |
| CONICF | - | Computes Y and Y' from given conic coefficients. |
| LINEAR | - | Linear interpolation routine. |

Appendix

SAMPLE DECK SET-UP

Samples of deck set-up are given below. The IVS and 3DMoC programs, because of their lengths, are stored on tapes in an updatable binary form. Permanent files of these programs are created for computation. The Surface Fit and Minimum Search Programs are read in the computer to create permanent files for computation. The samples were selected to illustrate various calculations for wave drag reduction of an F-4 type baseline configuration.

(1) LOAD IVS AND 3DMOC PROGRAMS ON TAPE, CREATE PF TO RUN FUSELAGE-WINGS
FOR 100 SURFACES, AND STORE OUTPUT DATA ON DATA TAPE.

```

JOB1,CB100000,T500,NT2.
*ACCOUNT CARD*
RESOURC(NT=2)
REQUEST(A,D=HD,VSN=4379),NT,PO=W)
UPDATE(N,W)
REWIND(NEWPL)
COPYBF(NEWPL,A)
FTN(I=COMPILE)
SAVE(LGO=IVSPF)
UPDATE(N=NUPL,C=COMT,W)
REWIND(NUPL)
COPYBF(NUPL,A)
FTN(I=COMT,B=BIN)
SAVE(BIN=MOC PF2)
SETCORE(0)
LOAD(LGO)
BLUNT.
XPAUSE. **** IF TAPE 4380 REACH END, USE TAPE 4381 AS NEXT OUTPUT TAPE ****
VSN(TAPE1=4380/4381)
REQUEST(TAPE1,D=HD,VSN=4380,NT,PO=W)
SETCORE(0)
REDUCE.
BIN.
7/8/9
*IVS PROGRAM
7/8/9
*3DMOC2 PROGRAM
7/8/9

```

```

$$$$$$$$$$$ F-4 BASELINE WITH WINGS $$$$$$$$$$$$$$$$$$$$
2.5 1.4 0. 35.70 5. 1.05
1. .001 4. 0. 90. 6.
.1

```

```

1/8/9
$$$$$$$$$$$ F-4 BASELINE WITH WINGS $$$$$$$$$$$$$$$$$$$$
.1 .1 .1 .01 0. 430. 3. 110.
100 5 11 14 1 0 20
45. 11 0
65. 17 15 17
85. 21 13 21
110. 22 13 19 5 9

```


| | | | | | | | | | | |
|---------|--------|----|-----|---|------|----|----|----|-----|---|
| 115. | 22 | 15 | 19 | 4 | 6 | 6 | 6 | 6 | 8 | 1 |
| 120. | 24 | 17 | 21 | 4 | 6 | 6 | 6 | 6 | 9 | 2 |
| 140. | 26 | 19 | 23 | 4 | 6 | 6 | 6 | 6 | 10 | 3 |
| 165. | 36 | 29 | 33 | 4 | 5 | 10 | 10 | 10 | 15 | 4 |
| 185. | 38 | 31 | 35 | 4 | 6 | 10 | 10 | 11 | 15 | 3 |
| 205. | 43 | 36 | 40 | 4 | 6 | 11 | 11 | 13 | 18 | 4 |
| 250. | 44 | 40 | 44 | 3 | 5 | 13 | 13 | 16 | 20 | 3 |
| 290. | 46 | 42 | 46 | 3 | 5 | 13 | 13 | 17 | 21 | 3 |
| 330. | 48 | 44 | 48 | 3 | 5 | 13 | 13 | 18 | 22 | 3 |
| 370. | 50 | 46 | 50 | 3 | 5 | 13 | 13 | 19 | 23 | 3 |
| 2.5 | 1.4 | | 0.0 | | | | | | | |
| -26.105 | 11.015 | | 1. | | 530. | | | | 0.5 | |

* FUSELAGE + WINGS BODY DESCRIPTION DATA *

6/7/8/9

(2) LOAD PHASE-2 3DMOC PROGRAM ON TAPE AND CREATE PF.

JOB2•CB100000•T500.

* ACCOUNT CARD *

UPDATE(N•W)

FTN(I=COMPILE)

SAVE(LG0=MOC PF1)

7/8/9

*3DMOC1 PROGRAM

6/7/8/9

(3) LOAD LATEINI PROGRAM TO CREATE PF AND RUN RADOME CONSTRAINT OPTION.

J083*CR600000*TS00.

* ACCOUNT CARD *

FTN.

SAVE (LGO=5X5)

COPYBR(INPUT,TAPE3)

REWIND(TAPE3)

LGO.

7/8/9

*LATINI LATIN SQUARE MINIMUM VALUE SEARCH PROGRAM *

7/8/9

FUSELAGE BODY DESCRIPTION DATA

7/8/9

L B F H A' A

23 1

3

50. 19.

18.5

* BLANK CARD *

1 8.72259

2 5.97017

3 5.72492

4 5.88469

5 5.95256

6 7.62580

7 7.25404

8 7.10510

9 5.43938

10 5.76062

11 6.52684

12 6.67305

13 6.59154

14 6.86143

15 7.61059

16 8.21773

17 8.68830

18 6.43817

19 6.61810

20 5.93960

21 7.63046

22 8.22275

23 8.62522

24 7.24846

00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000290
00000300
00000310

| | | | | | | | |
|------------|-------|-------|----------|-----------|----------|-------|----------|
| 25 5.87617 | -1.38 | 0. | .6666667 | -.6666667 | .6666667 | -.4 | 00000330 |
| 26 6.69437 | -1.38 | 1.5 | 2.0 | -.6666667 | 2.0 | -2.0 | 00000340 |
| 27 6.57260 | -1.38 | 2.0 | 2.0 | -2.0 | 2.0 | -2.0 | 00000350 |
| 28 6.09569 | -1.38 | 0. | 2.0 | -2.0 | 2.0 | -2.0 | 00000360 |
| 29 5.95529 | -1.38 | -1.71 | -2.0 | -2.0 | .84 | -2.0 | 00000370 |
| 30 5.86343 | -1.38 | 2.0 | 2.0 | -2.0 | 1.91 | .5325 | 00000380 |
| 31 6.81449 | -1.38 | 2.0 | 2.0 | -2.0 | 1.8 | -2.0 | 00000390 |
| 32 6.11884 | -0.38 | 2.0 | 2.0 | -2.0 | | -.418 | 00000400 |

* BLANK CARD *

| | | | | | | | |
|----|---|---|---|---|-----|-----|----|
| 1 | 5 | 5 | 5 | 5 | -2. | -2. | -2 |
| 0. | 5 | 5 | 5 | 5 | -2. | 2. | 2. |
| 0. | 5 | 5 | 5 | 5 | -2. | 2. | 2. |

6/7/8/9

(4) RESTART FUSELAGE-WING PROGRAM TO CONTINUE FOR 10 MORE SURFACES.

```

DER1,CB60000,I500,TP1.
* ACCOUNT CARD *
VSN(TAPE1=4380/4381)
XPAUSE. *** IF TAPE 4380 REACH END. USE TAPE 4381 AS NEXT OUTPUT TAPE ***
REQUEST(A,D=HD,VSN=4379),NT,PO=W)
SKIPF(TAPE1,99,17,B)
GET(BIN=MOC PF2)
SETCORE(0)
REDUCE.
BIN.
7/8/9

```

```

$$$$$$$$$$$ F-4 BASELINE WITH WING $$$$$$ $$$$$$ $$$$$$
110. 5 11 14 1 100 20 .01 0. 430. 3. 110.
45. 11 0 0
65. 17 15 17
85. 21 13 21
110. 22 13 19 5 9
115. 22 15 19 4 6 6 6 8 1
120. 24 17 21 4 6 6 6 9 2
140. 26 19 23 4 6 6 6 10 3
165. 36 29 33 4 5 10 10 15 4
185. 38 31 35 4 6 10 11 15 3
205. 43 36 40 4 6 11 13 18 4
250. 44 40 44 3 5 13 16 20 3
290. 46 42 46 3 5 13 17 21 3
330. 48 44 48 3 5 13 18 22 3
370. 50 46 50 3 5 13 19 23 3
2.5 1.4 0.0
-26.105 11.015 1. 530. 0.5
* FUSELAGE + WINGS BODY DESCRIPTION DATA *
6/7/8/9

```

(5) USE PF TO CALCULATE FUSELAGE FLOW FIELD.

VER2,CB100000,T500.

* ACCOUNT CARD *

GET(BIN=IVSPF)

SETCORE(0)

LOAD(BIN)

BLUNT.

GET(LGO=MOCPL)

SETCORE(0)

REDUCE.

LGO.

7/8/9

\$\$\$\$\$\$\$\$\$ F-4 BASELINE FUSELAGE ONLY \$\$\$\$\$\$\$\$\$\$

1.05
6.

35.70
0.
90.

0.
4.

1.4
0.001
.1

1

7/8/9

\$\$\$\$\$\$\$\$\$ F-4 BASELINE FUSELAGE ONLY \$\$\$\$\$\$\$\$\$\$

230.

0.

.01

5

.01

1

7

11

5

10

45.

65.

85.

95.

145.

190.

240.

2.5

-26.105

11.015

1.

530.

FUSELAGE BODY DESCRIPTION DATA

6/7/8/9

(6) USE LATINI PF TO RUN EQUIPMENT CONSTRAINT OPTION

DER3.CB60000.1500.
 * ACCOUNT CARD *
 COPYBR(INPUT,TAPE3)
 REWIND(TAPE3)
 GET(LGO=5X5)
 LGO.

7/8/9
 FUSELAGE BODY DESCRIPTION DATA
 7/8/9

| L | B | F | H | A* | A |
|----|---|---|---|----|---|
| 23 | 1 | | | | |
| 2 | | | | | |

50. 0.
 * BLANK CARD *

| | |
|----|---------|
| 1 | 8.72259 |
| 2 | 5.97017 |
| 3 | 5.72492 |
| 4 | 5.88469 |
| 5 | 5.95256 |
| 6 | 7.62580 |
| 7 | 7.25404 |
| 8 | 7.10510 |
| 9 | 5.43938 |
| 10 | 5.76062 |
| 11 | 6.52684 |
| 12 | 6.67305 |
| 13 | 6.59154 |
| 14 | 6.86143 |
| 15 | 7.61059 |
| 16 | 8.21773 |
| 17 | 8.68830 |
| 18 | 6.43817 |
| 19 | 6.61810 |
| 20 | 5.93960 |
| 21 | 7.63046 |
| 22 | 8.22275 |
| 23 | 8.62522 |
| 24 | 7.24846 |
| 25 | 5.87617 |
| 26 | 6.69437 |
| 27 | 6.57260 |

| | |
|-------|-----|
| -1.38 | 0. |
| -1.38 | 1.5 |

| | | |
|----------|------------|----------|
| .6666667 | - .6666667 | .6666667 |
| 2.0 | - .6666667 | 2.0 |

| |
|------|
| - .4 |
| -2.0 |

00000080
 00000090
 00000100
 00000110
 00000120
 00000130
 00000140
 00000150
 00000160
 00000170
 00000180
 00000190
 00000200
 00000210
 00000220
 00000230
 00000240
 00000250
 00000260
 00000270
 00000280
 00000290
 00000300
 00000310
 00000330
 00000340
 00000350

| | | | | | | | | |
|----------------|---------|-------|-------|------|------|------|-------|----------|
| 28 | 6.09569 | -1.38 | 2.0 | 2.0 | -2.0 | 2.0 | -2.0 | 00000360 |
| 29 | 5.95529 | -1.38 | 0. | 2.0 | -2.0 | 2.0 | -2.0 | 00000370 |
| 30 | 5.86343 | -1.38 | -1.71 | -2.0 | -2.0 | .84 | -2.0 | 00000380 |
| 31 | 6.81449 | -1.38 | 2.0 | 2.0 | -2.0 | 1.91 | .5325 | 00000390 |
| 32 | 6.11884 | -0.38 | 2.0 | 2.0 | -2.0 | 1.8 | -.418 | 00000400 |
| * BLANK CARD * | | | | | | | | |
| 1 | 5 | 5 | 5 | 5 | -2. | -2. | -2 | |
| 0. | 5 | -2. | -2. | -2. | 2. | 2. | 2. | |
| 0. | | 2. | | | | | | |
| 6/7/8/9 | | | | | | | | |

(7) USE LATINI PROGRAM TO RUN CROSS-SECTIONAL AREA CONSTRAINT.

CHUI,CB60000,T500.

* ACCOUNT CARD *

COPY8R(INPUT,TAPE3)

REWIND(TAPE3)

GET(LGO=5X5)

LGO.

7/8/9

FUSELAGE BODY DESCRIPTION DATA

7/8/9

L R F H A' A

23 1

1

50. 0.95

* BLANK CARD *

1 8.72259

2 5.97017

3 5.72492

4 5.88469

5 5.95256

6 7.62580

7 7.25404

8 7.10510

9 5.43938

10 5.76062

11 6.52684

12 6.67305

13 6.59154

14 6.86143

15 7.61059

16 8.21773

17 8.68830

18 6.43817

19 6.61810

20 5.93960

21 7.63046

22 8.22275

23 8.62522

24 7.24846

25 5.87617

26 6.69437

27 6.57260

0.

1.5

-1.38

-1.38

.6666667

2.0

-.6666667

2.0

.6666667

2.0

-.4

-2.0

00000340

00000350

| | | | | | | | |
|----------------|-------|-------|------|------|------|-------|----------|
| 28 6.09569 | -1.38 | 2.0 | 2.0 | -2.0 | 2.0 | -2.0 | 00000360 |
| 29 5.95529 | -1.38 | 0. | 2.0 | -2.0 | 2.0 | -2.0 | 00000370 |
| 30 5.86343 | -1.38 | -1.71 | -2.0 | -2.0 | .84 | -2.0 | 00000380 |
| 31 6.81449 | -1.38 | 2.0 | 2.0 | -2.0 | 1.91 | .5325 | 00000390 |
| 32 6.11884 | -0.38 | 2.0 | 2.0 | -2.0 | 1.8 | -.418 | 00000400 |
| * BLANK CARD * | | | | | | | |
| 1 | 5 | 5 | 5 | -2. | -2. | -2 | |
| 0. | -2. | -2. | -2. | -2. | 2. | 2. | |
| 0. | 2. | 2. | 2. | 2. | 2. | 2. | |
| 6/7/8/9 | | | | | | | |

(8) USE LATINI PROGRAM TO RUN VOLUME CONSTRAINT OPTION.

CHU2*CB60000*1500.
 * ACCOUNT CARD *
 COPYBR(INPUT,TAPE3)
 REWIND(TAPE3)
 GET(LG0=5X5)
 LG0.

7/8/9

FUSELAGE BODY DESCRIPTION DATA

7/8/9

| L | B | F | H | A' | A |
|------|---|------|---|------|------|
| 23 | 1 | | | | |
| 4 | | | | | |
| 0. | | 230. | | 1. | |
| 90. | | 150. | | 190. | |
| 225. | | | | | |
| | | | | | 1 |
| | | | | | 205. |
| | | | | | 200. |
| | | | | | 210. |
| | | | | | 215. |
| | | | | | 220. |

* BLANK CARD *

| | |
|----|---------|
| 1 | 8.72259 |
| 2 | 5.97017 |
| 3 | 5.72492 |
| 4 | 5.88469 |
| 5 | 5.95256 |
| 6 | 7.62580 |
| 7 | 7.25404 |
| 8 | 7.10510 |
| 9 | 5.43938 |
| 10 | 5.76062 |
| 11 | 6.52684 |
| 12 | 6.67305 |
| 13 | 6.59154 |
| 14 | 6.86143 |
| 15 | 7.61059 |
| 16 | 8.21773 |
| 17 | 8.68830 |
| 18 | 6.43817 |
| 19 | 6.61810 |
| 20 | 5.93960 |
| 21 | 7.63046 |
| 22 | 8.22275 |
| 23 | 8.62522 |
| 24 | 7.24846 |
| 25 | 5.87617 |

| |
|----------|
| 00000080 |
| 00000090 |
| 00000100 |
| 00000110 |
| 00000120 |
| 00000130 |
| 00000140 |
| 00000150 |
| 00000160 |
| 00000170 |
| 00000180 |
| 00000190 |
| 00000200 |
| 00000210 |
| 00000220 |
| 00000230 |
| 00000240 |
| 00000250 |
| 00000260 |
| 00000270 |
| 00000280 |
| 00000290 |
| 00000300 |
| 00000310 |
| 00000330 |

| | | | | | | | |
|--------------|-------|-------|----------|-----------|----------|-------|----------|
| 26 6.69437 | -1.38 | 0. | .6666667 | -.6666667 | .6666667 | -.4 | 00000340 |
| 27 6.57260 | -1.38 | 1.5 | 2.0 | -.6666667 | 2.0 | -2.0 | 00000350 |
| 28 6.09569 | -1.38 | 2.0 | 2.0 | -2.0 | 2.0 | -2.0 | 00000360 |
| 29 5.95529 | -1.38 | 0. | 2.0 | -2.0 | 2.0 | -2.0 | 00000370 |
| 30 5.86343 | -1.38 | -1.71 | -2.0 | -2.0 | .84 | -2.0 | 00000380 |
| 31 6.81449 | -1.38 | 2.0 | 2.0 | -2.0 | 1.91 | .5325 | 00000390 |
| 32 6.11884 | -0.38 | 2.0 | 2.0 | -2.0 | 1.8 | -.418 | 00000400 |
| * BLANK CARD | | | | | | | |
| 1 27969. | | | | | | | 00000420 |
| 2 24190. | | | | | | | 00000430 |
| 3 22492. | | | | | | | 00000440 |
| 4 27633. | | | | | | | 00000450 |
| 5 31198. | | | | | | | 00000460 |
| 6 25953. | | | | | | | 00000470 |
| 7 26918. | | | | | | | 00000480 |
| 8 31499. | | | | | | | 00000490 |
| 9 25273. | | | | | | | 00000500 |
| 10 30202. | | | | | | | 00000510 |
| 11 22460. | | | | | | | 00000520 |
| 12 26212. | | | | | | | 00000530 |
| 13 29430. | | | | | | | 00000540 |
| 14 34228. | | | | | | | 00000550 |
| 15 37811. | | | | | | | 00000560 |
| 16 28259. | | | | | | | 00000570 |
| 17 33819. | | | | | | | 00000580 |
| 18 29035. | | | | | | | 00000590 |
| 19 32614. | | | | | | | 00000600 |
| 20 30919. | | | | | | | 00000610 |
| 21 26603. | | | | | | | 00000620 |
| 22 31917. | | | | | | | 00000630 |
| 23 35621. | | | | | | | 00000640 |
| 24 36351. | | | | | | | 00000650 |
| 25 31103. | | | | | | | 00000660 |
| 26 25076. | | | | | | | |
| 27 25055. | | | | | | | |
| 28 23565. | | | | | | | |
| 29 21192. | | | | | | | |
| 30 20452. | | | | | | | |
| 31 27049. | | | | | | | |
| 32 27194. | | | | | | | |
| * BLANK CARD | | | | | | | |
| 1 | 5 | 5 | 5 | 5 | 5 | 5 | |
| 0. | -2. | -2. | -2. | -2. | -2. | -2. | |

0.
6/7/8/9 2. 2. 2. 2.

(9) LOAD LATINT2 PROGRAM TO CREATE PF AND RUN VOLUME CONSTRAINT OPTION.

CHU3,CR60000,T500.

* ACCOUNT CARD *

FTN.

SAVE (LGO=3X3)

LGO.

7/8/9

* LATIN2 LATIN SQUARE AND MINIMUM VALUE SEARCH PROGRAM *

7/8/9

H A R1 R2

10 1

1 116486.8

1 .0104602

4 .0094555

7 .0116629

2 .0116525

5 .0104013

8 .0114297

3 .0107868

6 .0128320

9 .0114309

10.00979359 -.333333 -.2

* BLANK CARD

1 -70402.3

4 -48181.6

7 32094.0

2 1265.5

5 36291.1

8 83446.1

3 47920.1

6 137459.1

9 154575.0

10 0.0

* BLANK CARD

21 21

-1. -1.

1. 1.

6/7/8/9

-1.

1.

-1.

1.

-1.0

-1.0

FUSELAGE BODY DESCRIPTION DATA

```

-26.511737
7
1 5.49149075E-01 5.73367672E+01 3.22022279E-01 6.24456002E+00 8.89238536E+02-1
2 0.0 E+00 1.10150000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
3 0.0 E+00 1.10150000E+01-1.0 E+00-5.22100000E+01-6.80471025E+02-1
4 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
5 8.14509253E-01 3.20504355E+01 3.09440900E-01 1.81910169E+01 3.55338926E+02-1
6 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
7 3.36009329E+00 1.58223695E+02 1.09128778E+01 9.80325854E+02 2.40943954E+04-1
-26.105
1
3-2.49023891E-01-4.04856541E+01 3.26127292E-01 3.22161029E-02 1.70631329E+03 1
0.
1
2 9.41050000E-02 1.34716110E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
35.
1
5 2.37961562E-01 1.97192947E+01 4.59075164E-02-1.22612844E+00 4.25012054E+01-1
50.
1
3 4.69618114E-02-6.35703498E+00 8.76793612E-03-7.465044489E-01 1.73845541E+01 1
60.
12
1 3.25001860E-01 2.12498820E+01 4.56257987E-02-5.58759941E+00 1.71565599E+02 1
2 9.41050000E-02 1.34716110E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
3 6.17342129E-02-6.76706983E+00 6.00394077E-03-5.32392375E-01 1.27723780E+01 1
5 2.43645384E-01 1.97395403E+01 4.84059774E-02-1.25659158E+00 4.38354577E+01-1
6 5.61007015E-01-1.87201403E+01-3.62840714E-01 4.67526985E+01-1.34348031E+03-1
7 6.65006015E-02 8.65811699E+00 2.55118541E-03-3.82669717E-01 1.95318964E+01-1
8 3.25001860E-01 2.12498820E+01 4.56257987E-02-5.58759941E+00 1.71565599E+02 1
9 1.03303975E+00-2.69645401E+02 1.48693730E+00-6.81728634E+02 9.69296900E+04 1
10 3.25001860E-01 2.12498820E+01 4.56257987E-02-5.58759941E+00 1.71565599E+02 1
11 4.60000000E-01-3.00000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
12 9.25000000E-02 7.75000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
13 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
65.
5
1 2.50000000E-01 2.65000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
3 2.20660324E-01-8.51318827E+00 5.04189058E-02-4.82042026E+00 1.46485599E+02-1
8 2.50000000E-01 2.65000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
10 3.30800117E-01 2.13816842E+01 2.10071510E-02-2.56454008E+00 7.83197281E+01 1
13 1.69428355E-01-7.61103902E+00 3.62521514E-02-5.18344403E+00 1.87025196E+02-1
1 4.49999988E-01 1.12031262E+01 1.83749962E-01-2.48062449E+01 8.41337958E+02 1
6 7.62467575E-01-5.13706401E+01-6.28039714E-02 5.64312348E+00-5.50767734E+01 1
10 4.65789000E-01 1.32237330E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
77.
3
1 3.194669309E-01 2.20894279E+01-3.44198713E-02 5.18085882E+00-1.93702750E+02 1
5 7.249999081E-02 1.70083294E+01 1.12293182E-03-2.02127204E-01 9.31348979E+00 1

```

8 1.81818203E-01 3.21818144E+01 1.03305539E-02-1.57024414E+00 6.01238176E+01-1
 80.
 3
 1 2.63562000E-01 2.74657260E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
 6 5.37634000E-03 9.58602200E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
 10 4.65789000E-01 1.32237330E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
 85.
 2
 2 5.36480156E-02 1.54704910E+01-2.71605902E-03 5.34714063E-01-2.38625259E+01 1
 10 4.65789000E-01 1.32237330E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
 100.
 2
 8 1.29323524E-01 3.31659571E+01 8.33241401E-03-1.55383488E+00 7.73570984E+01 1
 13-4.61624110E-01 5.15383731E+01 2.62234164E-01-5.23353921E+01 2.62443194E+03-1
 103.
 1
 11 2.94177736E-01 2.02578527E+01 5.59112031E-02-1.33961752E+01 8.25069479E+02-1
 110.
 2
 10 3.72282544E-01 2.47202489E+01 1.23135674E-02-2.88544023E+00 1.70045253E+02-1
 13 0.0 E+00 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
 120.
 2
 5 4.22221093E-02 2.08296406E+01-7.26924572E-04 1.97586566E-01-1.28325043E+01 1
 12 3.11818358E-02 1.37379328E+01-2.04450978E-03 5.45701343E-01-3.46769581E+01 1
 122.
 2
 2 0.0 E+00 2.30000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
 10 3.72282544E-01 2.47202489E+01 1.23135674E-02-2.88544023E+00 1.70045253E+02-1
 130.
 1
 10 1.44921931E-01 4.55285164E+01-3.31860250E-02 1.01251470E+01-7.07791365E+02 1
 140.
 2
 8 2.05479000E-01 2.72877300E+01 0.0 F+00 0.0 E+00 1.0 E+00 0
 9 2.26027000E-01 1.81164900E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
 150.
 1
 11 1.26667000E-01 3.69666200E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
 160.
 2
 1 3.58105141E-01 2.40204689E+01 5.91180929E-02-1.57053527E+01 1.14091266E+03-1
 12-4.35421248E-02 2.43167648E+01-1.46009950E-03 5.87340493E-01-5.23091400E+01 1
 170.
 2
 5 0.0 E+00 2.80000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
 10 1.44921931E-01 4.55285164E+01-3.31860250E-02 1.01251470E+01-7.07791365E+02 1
 180.
 2
 6 3.03462490E-02 4.93794747E+00 3.98463449E-03-1.37491097E+00 1.18741491E+02 1
 11 2.35939575E-02 4.64431781E+01-6.09878510E-02 2.23944900E+01-1.97977872E+03 1
 190.
 3
 3 0.0 E+00 1.00000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
 6 8.00000000E-02-3.40000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
 10-2.48597019E-02 8.23034310E+01-1.04050162E-04 4.10035098E-02-4.00432153E+00 1
 203.
 2

| | | | | | | |
|------|----------------|----------------|-----------------|-----------------|-----------------|--------|
| 1 | 8.00000602E-02 | 6.23787330E+01 | 1.65039699E-02 | -6.68410750E+00 | 6.80837034E+02 | -1 |
| 10-2 | 48597019E-02 | 8.23034310E+01 | -1.04050162E-04 | 4.10035098E-02 | -4.00432153E+00 | 1 |
| 215. | | | | | | |
| 8 | 4.84836491E-01 | 3.20811892E+01 | 2.37474528E-01 | -9.79004947E+01 | 1.00947849E+04 | 1 |
| 9 | 1.76756712E+01 | 3.94110534E+03 | 3.17849965E+02 | -1.43598138E+05 | 1.62259851E+07 | 1 |
| 218. | | | | | | |
| 1-7 | .00000000E-02 | 9.20500000E+01 | 0.0 | E+00 0.0 | 1.0 | E+00 0 |
| 8-7 | .00000000E-02 | 9.20500000E+01 | 0.0 | E+00 0.0 | 1.0 | E+00 0 |
| 10-7 | .00000000E-02 | 9.20500000E+01 | 0.0 | E+00 0.0 | 1.0 | E+00 0 |
| 290. | | | | | | |
| 1-7 | .00000000E-02 | 9.20500000E+01 | 0.0 | E+00 0.0 | 1.0 | E+00 0 |

* FUSELAGE * WINGS BODY DESCRIPTION DATA *

```

4
1 1.1000000E+02 1.90000000E+02
22 4.33296327E-02 1.80002653E+01 -1.08547881E-02 3.26821039E+00 -1.25005203E+02 -1
2 1.90000000E+02 2.10000000E+02
22 8.53087902E-02 -1.78558350E-01 0.0 E 0.0 E 1.00000000E+00 0
3 2.10000000E+02 2.85000000E+02
22 8.95633362E-02 8.8149228E+00 1.60979977E-02 -6.67703379E+00 7.89998489E+02 -1
4 2.85000000E+02 4.30000000E+02
22 -3.69162194E-02 5.93919575E-01 -1.95519518E-02 1.33830055E+01 -1.30691653E+03 1
-26.678576 7 1
1 4.67350412E-01 4.26126281E+01 1.77600524E-01 2.88372638E-01 2.16548185E+02 -1
2 0.0 E+00 1.10150000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
3 0.0 E+00 1.10150000E+01 -1.0 E+00 -5.22100000E+01 -6.80471025E+02 -1
4 0.0 E+00 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
5 0.0 E+00 0.0 E+00 -1.0 E+00 -5.22100000E+01 -6.80471025E+02 1
6 0.0 E+00 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
7 0.0 E+00 1.10150000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
-26.511737 1
5 6.44442767E-01 2.44436641E+01 1.46386781E-01 7.09346363E+00 1.26419987E+02 -1
-6.105 1
3 -2.48647190E-01 -3.99438475E+01 3.22172520E-01 -1.52592977E-03 1.66169704E+03 1
0. 2
2 1.27651029E-01 1.17943095E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
7 1.27651029E-01 1.17943095E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
35. 1
5 2.25972698E-01 1.88438923E+01 3.82148943E-02 -1.16294999E+00 3.18535228E+01 -1
50. 1
3 3.26131567E-02 -5.61306675E+00 7.12285310E-03 -5.75019262E-01 1.27728399E+01 1
60. 12 2
1 3.25001860E-01 2.12498820E+01 4.56257987E-02 -5.58759941E+00 1.71565599E+02 1
2 9.41050000E-02 1.34716110E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
3 3.26131567E-02 -5.61306675E+00 7.12285310E-03 -5.75019262E-01 1.27728399E+01 1
5 2.43645384E-01 1.97395403E+01 4.84059774E-02 -1.25659158E+00 4.38354577E+01 -1
6 5.61007015E-01 -1.87201403E+01 -3.62840714E-01 4.67526985E+01 -1.34348031E+03 -1
7 9.41050000E-02 1.34716110E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
8 3.25001860E-01 2.12498820E+01 4.56257987E-02 -5.58759941E+00 1.71565599E+02 1
9 1.03303975E+00 -2.69645401E+02 1.4869730E+00 -6.81728634E+02 9.69296900E+04 1
10 3.25001860E-01 2.12498820E+01 4.56257987E-02 -5.58759941E+00 1.71565599E+02 1
11 4.60000000E-01 -3.00000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
12 9.25000000E-02 7.77500000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
13 0.0 E+00 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0

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65. 4
1 2.5000000E-01 2.65000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
8 2.5000000E-01 2.65000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
10 3.30800117E-01 2.13816842E+01 2.10071510E-02-2.56454008E+00 7.83197281E+01 1
13 1.69428355E-01-7.61103902E+00 3.62521514E-02-5.18344403E+00 1.87025196E+02-1
70. 4
1 4.49999988E-01 1.12031262E+01 1.83749962E-01-2.48062449E+01 8.41337958E+02 1
3 7.47301953E-02-4.28907043E+00 5.79379569E-03-8.65816229E-01 3.47521388E+01-1
6 7.62467575E-01-5.13706401E+01-6.28039714E-02 5.64312348E+00-5.50767734E+01 1
10 4.65789000E-01 1.32237330E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
77. 3
1 3.19469309E-01 2.20894279E+01-3.44198713E-02 5.18085882E+00-1.93702750E+02 1
5 7.24999081E-02 1.70083294E+01 1.12293182E-03-2.02127204E-01 9.31348979E+00 1
8 1.81818203E-01 3.21818144E+01 1.03305539E-02-1.57024414E+00 6.01238176E+01-1
80. 2
1 2.63562000E-01 2.74657260E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
6 5.37634000E-03 9.58602200E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
85. 2
2 5.36480156E-02 1.54704910E+01-2.71605902E-03 5.34714063E-01-2.38625259E+01 1
7-4.02667000E-01 5.32133600E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
95.36 2
8 1.293323524E-01 3.31659571E+01 8.33241401E-03-1.55383488E+00 7.73570984E+01 1
13-4.61624110E-01 5.15383731E+01 2.62234164E-01-5.23353921E+01 2.62443194E+03-1
100. 1
7-4.02667000E-01 5.32133600E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
103. 1
11 2.94177736E-01 2.02578527E+01 5.59112031E-02-1.33961752E+01 8.25069479E+02-1
110. 2
10 3.72282544E-01 2.47202489E+01 1.23135674E-02-2.88544023E+00 1.70045253E+02-1
13 0.0 E+00 0.0 E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
120. 9 4 1.9
5 4.22221093E-02 2.08296406E+01-7.26924572E-04 1.97586566E-01-1.28325043E+01 1
7 0.0 E+00 8.92000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
12 3.11818358E-02 1.37379328E+01-2.04450978E-03 5.45701343E-01-3.46769581E+01 1
14 5.54759061E-02 2.52983153E+00 3.46164047E-03-1.20290707E+00 1.06256968E+02 1
15-5.54759235E-02 1.96901731E+01 3.46164330E-03-1.20290821E+00 1.06257085E+02-1
16 4.28614138E-02 4.31462046E+00 2.06422324E-03-7.18208885E-01 6.35161184E+01 1
17-4.28614040E-02 1.79053759E+01 2.06422148E-03-7.18208281E-01 6.35160620E+01-1
18 0.0 E+00 1.11100000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
21 2.51831244E-01-9.54562517E+00 2.33959273E-02-7.46835782E+00 5.96862302E+02 1
122. 1 1.9
2 0.0 E+00 2.30000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
130. 1 1.9

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10 1.44921931E-01 4.55285164E+01-3.31860250E-02 1.01251470E+01-7.07791365E+02 1
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8 2.05479000E-01 2.72877300E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
9 2.26027000E-01 1.81164900E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
150. 1.9
11 1.26667000E-01 3.69666200E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
160. 1.9
1 3.58105141E-01 2.40204689E+01 5.91180929E-02-1.57053527E+01 1.14091266E+03-1
12-4.35421248E-02 2.43167648E+01-1.46009505E-03 5.87340493E-01-5.23091400E+01 1
170. 1.9
5 0.0 E+00 2.80000000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
180. 1.9
6 3.03462490E-02 4.93794747E+00 3.98463449E-03-1.37491097E+00 1.18741491E+02 1
7-5.54759235E-02 1.96901731E+01 3.46164330E-03-1.20290821E+00 1.06257085E+02-1
11 2.35939575E-02 4.64431781E+01-6.09878510E-02 2.23944900E+01-1.97977872E+03 1
190. 1.9
2 5.01194177E-02 1.30713767E+01 4.53565465E-03-1.72376514E+00 1.64145395E+02 1
3 0.0 E+00 1.00000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
6 0.00000000E-02-3.40000000E+00 0.0 E+00 0.0 E+00 1.0 E+00 0
10-2.48597019E-02 8.23034310E+01-1.04050162E-04 4.10035098E-02-4.00432153E+00 1
200. 1.9
1 8.00000002E-02 6.23787330E+01 1.65039699E-02-6.68410750E+00 6.80837034E+02-1
203. 1.9
2-6.76794001E-02 2.26207604E+01-1.01106588E-02 9.05011740E+00-1.18313633E+03 1
7 6.77003943E-02 7.93805583E+00-1.01105037E-02 9.05169351E+00-1.18336783E+03-1
14-6.76859833E-02 1.42810702E+01-1.01106792E-02 9.05065979E+00-1.18321397E+03 1
15 6.77003943E-02 7.93805583E+00-1.01105037E-02 9.05169351E+00-1.18336783E+03-1
16 9.27609874E-01-8.52069135E+01 9.09851308E-01-2.17906746E+02 1.45601058E+04-1
17-3.12060699E-01 4.33002563E+01 1.12311500E-01-3.22998628E+01 2.69014825E+03 1
212. 1.9
8 9.63279045E-01-1.26160629E+02-5.64020269E-02 2.34827545E+01-2.44257980E+03-1
9 1.76756712E+01-3.94110534E+03 3.17849965E+02-1.43598138E+05 1.62259851E+07 1
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218. 1.9
1-7.00000000E-02 9.20500000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
8-7.00000000E-02 9.20500000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
10-7.00000000E-02 9.20500000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
220. 1.9
1-7.00000000E-02 9.20500000E+01 0.0 E+00 0.0 E+00 1.0 E+00 0
230. 3
19 3.36342972E-01-3.08786588E+01 7.70106182E-03-3.64537091E+00 4.31450575E+02 1
20 3.36342972E-01-3.08786588E+01 7.70106182E-03-3.64537091E+00 4.31450575E+02 1

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21 4.04026000E-01-3.37448100E+01 0.0      E+00 0.0      E+00 1.0      E+00 0
240.
2
1-3.31343384E-01 1.54469238E+02 7.63460300E-02-3.63267175E+01 4.32177736E+03-1
6 3.78260866E-02 5.83620332E+04 2.33422784E+02-1.12296658E+05 3.41887176E+09-1
250.
3
1-3.02083331E-01 1.44458333E+02 1.32920989E-01-6.46102344E+01 7.85437568E+03 1
19 4.04026000E-01-4.67448100E+01 0.0      E+00 0.0      E+00 1.0      E+00 0
20 4.04026000E-01-4.67448100E+01 0.0      E+00 0.0      E+00 1.0      E+00 0
286.41
2
1 0.0      E+00 7.20000000E+01 0.0      E+00 0.0      E+00 1.0      E+00 0
6 0.0      E+00 1.58000000E+01 0.0      E+00 0.0      E+00 1.0      E+00 0
289.96
4
2 0.0      E+00 2.73100000E+01 0.0      E+00 0.0      E+00 1.0      E+00 0
7-4.15609201E+00-7.56278893E+03 2.35265344E+01 5.93082172E+04 5.77579183E+07 1
14 4.14592346E+00 7.56669858E+03 2.34269558E+01 5.90112026E+04 5.74799363E+07-1
15-4.15609201E+00-7.56278893E+03 2.35265344E+01 5.93082172E+04 5.77579183E+07 1
480.
2
16-9.55760562E-02 1.87374283E+02 5.77347121E-02-6.07877908E+01 3.31783010E+04-1
17 4.61274458E-02-4.67336905E+01 1.47273267E-02-1.21181837E+01 3.77934000E+03 1

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